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RESEARCH MEMORANDUM

FORCE AND PRESSURE-DISTRIBUTION INVESTIGATION TO HIGH ANGLES OF ATTACK ON ALL-MOVABLE TRIANGULAR AND RECTANGULAR WINGS IN COMBINATION WITH A BODY AT SUPERSONIC SPEEDS

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By authority of NACA. *CHL 62*Date *6/2/62*Time *8-14-67*RESEARCH MEMORANDUM

FORCE AND PRESSURE-DISTRIBUTION INVESTIGATION TO HIGH
ANGLES OF ATTACK ON ALL-MOVABLE TRIANGULAR AND
RECTANGULAR WINGS IN COMBINATION WITH A
BODY AT SUPERSONIC SPEEDS

By William A. Hill, Jr., and George E. Kaattari

SUMMARY

In order to provide high-incidence data for all-movable triangular and rectangular wings and a body in combination, forces, moments, and load distributions were measured to combined body angles of attack and wing deflection of $\pm 45^\circ$ at a Mach number of 3.36. The ranges of aspect ratios were, for the triangular wings, $3/8$ to 4 , and, for the rectangular wings, 1 to 3. Additional measurements giving over-all combination aerodynamic coefficients were made on two smaller scale wing-body combinations at Mach numbers of 3.36, 2.44, and 1.98.

The investigation showed that the mutual interference effects of body and wing could be satisfactorily calculated in the body angle-of-attack range from at least 0° to 6° and in the wing deflection range from 0° to 10° . Nonlinear effects precluded the satisfactory application of theoretical methods of predicting force and moment coefficients at higher incidences. These effects were due to a decrease in the effect of body upwash on wing lift with an increase in angle of attack above 10° , and to an increasingly nonplanar geometrical relationship of the wing and body with increasing wing deflection angle, thus departing from the simplified planar model on which the theory was based.

INTRODUCTION

Adequate maneuverability at ever-increasing altitudes requires missiles and interceptor aircraft to operate through large ranges of angles of attack and control deflection. Since supersonic aircraft at high angles of attack can encounter highly nonlinear aerodynamic forces, experimental investigation of body-wing configurations at high incidence and at supersonic speeds is needed in order to provide useful design data and to aid in the development of applicable high-angle theories. Some high-incidence

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data on body-wing combinations at supersonic speeds are available (e.g., refs. 1 to 4), however, detailed data in the form of forces, moments, and load distributions are limited.

A program was undertaken at the Ames 1- by 3-foot wind tunnels to provide some experimental data on the aerodynamic characteristics of wings and of all-movable wing-body combinations at high angles of attack. References 5, 6, and 7 report results of force and pressure-distribution measurements on semispan wings of triangular and rectangular plan form, tested to high angles of attack in the Mach number range 1.45 to 3.36. The investigation reported herein gives the results of tests at a Mach number of 3.36 of configurations using a selection of these wings as all-movable controls in combination with a body. The tests extended over the combined angle-of-attack and wing-deflection range of 0° to $\pm 45^\circ$. The data obtained consisted of forces and moments on the body and on all of the wings. Load distributions were obtained on the body and on the wings previously employed in the investigation of reference 7. Smaller scale full-span models of two of the semispan configurations were tested to high incidences at Mach numbers of 1.98, 2.44, and 3.36 in order to indicate the effects of Mach number.

Limited comparisons of experimental force and moment coefficients with calculated values based on linear theory were made to establish the range of angles of attack and wing deflection wherein theoretical values are in satisfactory agreement with those of experiment. Factors contributing to nonlinear force and moment coefficients at higher incidences are indicated.

SYMBOLS

A aspect ratio of the exposed wing panels joined together

c local chord, in.

$$c_n \quad \text{local normal-force coefficient,} \quad \begin{cases} c_{nB}(W) = \frac{2}{D} \int_0^{\pi} P r \cos \theta \, d\theta \\ c_{nW(B)} = \int_0^1 (P_l - P_u) d(x/c) \end{cases}$$

c_r root chord at wing-body juncture, in.

\bar{c} mean aerodynamic chord of exposed wing panels, in.

$\frac{cc_n}{\bar{c}}$ span loading coefficient

| | |
|--------------|--|
| C_b | bending-moment coefficient about wing root chord, <u>bending moment</u> $\frac{q_{\infty} S_w s_w}{}$ |
| C_h | hinge-moment coefficient, <u>hinge moment</u> $\frac{q_{\infty} S_w \bar{c}}{}$ |
| C_m | pitching-moment coefficient about wing hinge line, <u>pitching moment</u> $\frac{q_{\infty} S_w \bar{c}}{}$ |
| C_D | drag coefficient, <u>drag</u> $\frac{q_{\infty} S_w}{}$ |
| C_L^* | component of normal-force coefficient normal to free-stream direction, $C_N \cos(\alpha_B + \delta_w)$ |
| C_N | normal-force coefficient, <u>normal force</u> $\frac{q_{\infty} S_w}{}, C_{N_W(B)}$ normal to wing chord; $\Delta C_{N_B(W)}$, $C_{N_{BW}}$, and C_{N_B} normal to body axis |
| D | body diameter, in. |
| $k_B(W)$ | ratio of interference lift of body in presence of wing to that of wing alone, δ_w variable, $\alpha_B = 0^\circ$ |
| $k_W(B)$ | ratio of lift of wing in presence of body to that of wing alone, δ_w variable, $\alpha_B = 0^\circ$ |
| $K_B(W)$ | ratio of interference lift of body in presence of wing to that of wing alone, α_B variable, $\delta_w = 0^\circ$ |
| $K_W(B)$ | ratio of lift of wing in presence of body to that of wing alone, α_B variable, $\delta_w = 0^\circ$ |
| M | Mach number |
| p | orifice pressure |
| p_{∞} | free-stream static pressure |
| P | pressure coefficient, $\frac{p - p_{\infty}}{q_{\infty}}$ |
| q_{∞} | free-stream dynamic pressure |
| r | body radius, in. |

| | |
|---------------------|---|
| R | Reynolds number |
| s | combination semispan, measured from axis of body, in. |
| s_w | wing semispan measured from wing-body juncture, in. |
| S_B | body frontal area, sq in. |
| S_W | area of exposed wing panel, sq in. |
| t | local thickness of wing section |
| x | chordwise distance from leading edge of wing at spanwise distance y or distance along body from nose tip, in. |
| \bar{x}_{cr} | linear-theory distance to center of pressure from leading edge of wing-body juncture, root chords |
| y | spanwise distance from wing-body juncture, in. |
| β | $\sqrt{M^2 - 1}$ |
| α_B | angle of attack of body with respect to free stream, deg |
| α_W | angle of attack of wing with respect to free stream, $\alpha_W = \alpha_B + \delta_W$, deg |
| δ_W | deflection angle of wing with respect to body, deg |
| θ | azimuthal location of body pressure orifices measured from meridional plane, deg |
| $\Delta(\)_{B(W)}$ | body interference coefficient, $(\)_{B(W)} - (\)_B$ |

Subscripts

| | |
|------|------------------------------------|
| h | hinge line |
| l | lower surface |
| u | upper surface |
| B | body alone |
| B(W) | body in the presence of a wing |
| BW | body-wing combination, B(W) + W(B) |

W wing alone

W(B) wing in the presence of the body

APPARATUS

Tunnel

The investigation was conducted in the Ames 1- by 3-foot supersonic wind tunnel No. 2. This nonreturn, intermittent-operation, variable-pressure wind tunnel has a Mach number range of 1.4 to 3.8. The Mach number can be changed by varying the contour of flexible steel plates which form the upper and lower walls of the nozzle.

Models

Semispan wings.- The semispan wings of the present investigation were selected from models previously employed in the wing-alone tests of references 5, 6, and 7. The geometry of these wings is summarized in figure 1(a). Three of the wings of this figure were fitted with pressure orifices. The wings, in vertical streamwise planes, had modified biconvex sections with trailing edges blunted to a height one-half the maximum thickness. The wings fitted with pressure orifices had maximum thickness ratios of 5 percent at the 50-percent-chord line and the remaining wings had maximum thickness ratios of 4 percent at the 59-percent-chord line. At the root, the wings were provided with an integral shaft, the axis of which was the hinge line. All of the wings, with the exception of the triangular wing of aspect ratio 3/8, had filleted root sections (see sketch in fig. 1(a)). The pressure orifices were made by drilling holes in one surface of the wings at the locations listed in table I. Tubing was soldered into milled grooves in the wing surface opposite the orifice holes, and led from each orifice out through a hole in the hinge shaft.

Half bodies.- Two half bodies of revolution identical in profile were employed. The bodies consisted of a pointed nose 6 inches long on a 2-inch-diameter cylindrical afterportion 20 inches long. The nose profile is defined by the Haack equation

$$r = 0.564 \sqrt{\cos^{-1}\left(1 - \frac{x}{3}\right) - \sin \frac{1}{2} \left[\cos^{-1}\left(1 - \frac{x}{3}\right) \right]}$$

r(6) = .126

Inorrect

The first body, designated model I, was tested in combination with the pressure-distribution wings, and the other body, designated model II, was tested in combination with the remaining wings. The pressure orifices were

$$r = \frac{1}{\sqrt{\pi}} \sqrt{\cos^{-1}\left(1 - \frac{x}{3}\right) - \frac{1}{2} \sin \left[2 \cos^{-1}\left(1 - \frac{x}{3}\right) \right]}$$

A. H. Jr.

made by sweating steel tubing in drilled holes and grinding the ends of the tubes flush with the body surface. The coordinate system by which the orifices are located is presented in the sketch accompanying table II(a). Pressure tubes from the orifices were led out around the wing hinge shaft.

Full-span models.- The full-span models consisted of a body to which was attached an aspect-ratio-1 rectangular wing or an aspect-ratio-2 triangular wing. These models were geometrically the same as two semispan model combinations having $r/s = 0.2$, as denoted in figure 1(a), but were reduced in size by the ratio of 7/16. The wing panels of the full-span models were integral to a common hinge shaft which, when set in place in the body, could be rotated to the desired wing deflection angle and then secured by a friction clamp.

Balance and Supports

The semispan wings were tested in the presence of a half body of revolution which was mounted on a boundary-layer plate. The boundary-layer plate served as a flow reflection plane and as a means of eliminating the effect of tunnel wall boundary layer in much the same way as the boundary-layer plate of reference 5; however, in the present tests the plate extended 11-1/2 inches farther upstream to accommodate the long body (see fig. 1(b)). Since the plate could not be rotated, angle of attack was varied by attaching the body to the plate at the desired angles. For pressure-distribution tests the hinge shafts of the wings were supported by bearings in the body and at the tunnel wall. For balance tests of the wings, the shaft passed through a hole in the body and was supported entirely by a strain-gage balance (see ref. 8). A fairing extended between the wall of the tunnel and the back side of the boundary-layer plate to shield the support shaft from air loads. A 0.005- to 0.010-inch gap was provided between the wing and body in order to prevent mechanical interference. In addition, the operation of the balance in the force tests required an annular gap of 0.10 inch around the wing hinge shaft.

The full-span models were supported from the rear by a 13° bent sting. This bent sting was used to increase the range of positive angles of attack. Lift and drag forces acting on these models were measured by a strain-gage balance which supported the sting. Pitching moment was measured by strain gages mounted on the sting between the model and the balance. The sting was shielded from aerodynamic forces by a shroud that extended to within 0.015 inch of the base of the model. The base pressure of the models was measured by static-pressure orifices in the sting adjacent to the base.

PROCEDURE

Test Conditions

Tests of the semispan models were conducted at a Mach number of 3.36 and a Reynolds number per inch of 0.85 million. The body was set at fixed angles of attack and the wing deflection angle was varied such that the maximum wing deflection angle or the sum of the body angle of attack and wing deflection did not exceed $\pm 45^\circ$. The body angle of attack was varied from 0° to 25° . Tests of the aspect ratio 2/3 and 3/8 triangular wings were limited to the cases of zero body angle of attack with varying wing deflection angle, and zero wing deflection angle with varying body angle of attack.

The full-span models were tested at Mach numbers of 1.98, 2.44, and 3.36 and at a Reynolds number per inch of 0.85 million. The body angle of attack was varied through a nominal range of -4° to $+30^\circ$ with the wing set at fixed deflection angles ranging from -35° to $+40^\circ$.

Reduction of Data

Semispan models. - Comparisons of tunnel stream surveys for the conditions of tunnel empty and with the boundary-layer plate present indicated a plate-induced spanwise Mach number variation in the region occupied by the semispan models. Therefore average Mach numbers were determined according to the spanwise extent of each model:

| Model | Average Mach number, \bar{M} |
|-------------------------------|--------------------------------|
| Body | 3.36 ± 0.02 |
| All models having $r/s = 0.4$ | 3.40 ± 0.02 |
| All models having $r/s = 0.2$ | 3.43 ± 0.02 |

As it was desirable to compare the data for the wing in the presence of the body with the corresponding data for the wing alone, it was necessary to correct the data from the average Mach number, \bar{M} , to the Mach number of the wing-alone data, $M = 3.36$. The following approximation was used:

$$(\text{Coefficient at } M = 3.36) \approx \frac{\sqrt{\bar{M}^2 - 1}}{\sqrt{(3.36)^2 - 1}} (\text{Coefficient at } \bar{M})$$

For the pressure-distribution wings tabular integration of the corrected values of measured pressure distribution along the wing chord provided local span loading coefficients and chordwise centers of pressure.

The spanwise load distributions were in turn integrated to obtain normal-force, hinge-moment, and root bending-moment coefficients. For the other wings, normal-force, hinge-moment, bending-moment, and drag coefficients were determined from balance measurements. The normal-force coefficient is presented for these wings in order to be consistent with the pressure-distribution-wing data since in the latter case the distribution of ori-fices and their limited number precluded an accurate measurement of chord force.

Pressure distributions around the circumference of the body were integrated to give local longitudinal loading coefficients. The difference between the local loading for the body in the presence of a wing and the body alone yielded the interference loading on the body which was then integrated to give interference normal-force and pitching-moment coefficients about the wing hinge-line reference. Reasons for presenting only interference loading on the body are discussed in more detail in a later section.

Full-span models.- Variations of Mach number from free-stream conditions were negligible at the full-span-model locations and required no corrections to the measured data. Normal-force and total drag coefficients were determined from balance measurements. The drag coefficients were corrected to a condition of free-stream pressure on the base of the body. Pitching-moment coefficients, determined from measured pitching moments, were referred to the wing hinge axis. The actual angles of attack of the body were determined by photographs because of small deflections of the sting due to aerodynamic loads on the model.

RELIABILITY OF DATA

Limits of Uncertainty

The uncertainty in the data was assessed on the basis of repeatability, estimated effects of tunnel stream asymmetry, and uncertainty in the average Mach number in the wind tunnel at the model location. The limits of uncertainty for the wings in the presence of the body were:

$$C_{NW}(B) \quad \pm 0.015 \text{ for all wings}$$

$$C_{hW}(B) \quad \begin{cases} \pm 0.010 \text{ for rectangular wings of } A = 3 \text{ and } A = 1, r/s = 0.4; \\ \pm 0.005 \text{ for all other wings} \end{cases}$$

$$C_{bW}(B) \quad \begin{cases} \pm 0.040 \text{ for rectangular wing of } A = 1, r/s = 0.4; \\ \pm 0.020 \text{ for all other wings} \end{cases}$$

| | |
|--------------|---|
| $C_{Dw}(B)$ | ± 0.010 for all wings |
| $P_{W(B)}$ | ± 0.010 |
| $c_{n_w}(B)$ | ± 0.010 } for pressure-distribution wings |

The limits of uncertainty for the body in the presence of the wings, which apply up to $\alpha_B = 20^\circ$ as discussed later, are given as follows:

| | | |
|---------------------|-----------------------|--|
| $\Delta C_{N_B(W)}$ | $\pm 0.13/S_W$ | (These quantities are inversely proportional to the wing reference area and chord and are approximately equal to two of the smallest grid-line divisions on the graphs.) |
| $\Delta C_m(B(W))$ | $\pm 0.34/\bar{c}S_W$ | |

$P_B(W)$ ± 0.010

$\Delta c_{n_B(W)}$ ± 0.010

The limits of uncertainty for the full-span models were:

$C_{N_{BW}}$ ± 0.015

C_m_{BW} ± 0.030

$C_{D_{BW}}$ ± 0.010

$\frac{S_W}{S_B} C_{N_B}$ ± 0.08

$\frac{\bar{c}S_W}{DS_B} C_{m_B}$ ± 0.50

$\frac{S_W}{S_B} C_{D_B}$ ± 0.05

The uncertainty in Reynolds number per inch was ± 0.05 million.

Effects of Wing-Body Gap on Semispan Data

The effect of the annular clearance gap around the supporting shaft of the force test wings was evaluated through limited measurements on the pressure-distribution wings with and without a gap. A comparison of the data showed that the effects of the gap were insignificant. The effect of the gap between the body and the undeflected wing was assumed to be negligible for the gap-span ratios and angles of attack of the present test on the basis of the findings of references 9 and 10.

Effects of Boundary-Layer Plate on Half-Body Data

Evidence of boundary-layer effects on the half-body data was revealed by preliminary comparisons of pressure-test results of the half body alone with those of force tests on the full body alone. This comparison is presented in figure 2(a) in the form of normal-force coefficients plotted against angle of attack. Figure 2(a) shows that good agreement between the test methods occurs up to $\alpha_B = 15^\circ$. Beyond 15° an increasing loss of the normal-force coefficient of the half model is evident with increasing angle of attack. The poor agreement above 15° appears to be coincident with the fact that above $\alpha_B = 17.3^\circ$ the crossflow Mach number exceeds unity and interaction effects of the resulting crossflow shock with the plate boundary layer might be expected. In figure 2(b), which presents longitudinal loading along the cylindrical portion of the half-body model, an additional effect is shown which might be attributed to the boundary-layer plate. This is observed as a high loading near the base of the body which increases with angle of attack.

It is believed that the foregoing effects of boundary-layer interference are, to a large extent, eliminated in the interference data presented herein for the body in the presence of a wing. The procedure for determining interference, as mentioned in the data-reduction section, consisted of subtracting from the load distribution on the body in the presence of a wing, the loading distribution of the body alone at the same angle of attack. The boundary-layer plate effects, being presumably little affected by the presence of a wing, were thus minimized in the resulting interference loading.

In view of the foregoing discussion, the limits of uncertainty presented earlier for the interference force and moment coefficients on the body in the presence of a wing should apply up to $\alpha_B = 20^\circ$. Because of the large boundary-layer effects encountered at higher angles of attack, the reliability limits at $\alpha_B = 25^\circ$ are uncertain but are not expected to be in excess of ± 10 percent of the interference force and moment coefficients presented in the basic data.

Comparison of Full-Span and Semispan Data

An additional means of assessing the reliability of measurements was provided by a comparison of the results from the two independent methods employed in the investigation for the $A = 1$ rectangular wing and body combination. The data from both test methods were compared on a basis common to both; that is, the sum of the lift of the wing in the presence of the body and the interference lift on the body due to the wing, obtained from the semispan model tests, was compared with the equivalent total combination lift minus the lift of the body alone, obtained from the

full-span-model tests. A similar comparison of moment about the wing hinge line was also made. These comparisons are presented in figures 3(a) and 3(b), respectively. Figure 3(a) shows that the maximum differences between the two test methods occur at high positive and negative values of the lift component where the deviation is generally no greater than about ± 0.02 from a mean curve. This scatter substantially verifies the individual estimations of data reliability for the two test methods. As previously indicated, the degree of precision in measuring moments on the semispan models was considerably greater than that for full-span models. Therefore, the curves of figure 3(b) were drawn to favor the semispan data. The comparison thus reflects primarily the limited reliability of the full-span-model moment measurements. Errors in this quantity are inherently large for the full-span model, due to the remote location of the moment gage from the wing hinge-line reference axis.

RESULTS

All pressure data presented are in tabular form. Because of the large number of individual pressure measurements obtained, it was impractical to present a complete tabulation of all the data obtained. Tabulation of pressure coefficients was therefore restricted to cases of α_B variable, $\delta_W = 0^\circ$, and δ_W variable, $\alpha_B = 0^\circ$. However, complete loading results in terms of wing span loading and loading induced on the body by the wing are tabulated for all conditions investigated. The following index indicates the specific pressure and loading data presented in each table.

| Model | | | Table number | |
|--------------------------|-----|-----|-----------------------|--|
| Plan form | A | r/s | Pressure coefficients | Span loading coefficients |
| Wing in presence of body | | | | |
| Triangular | 4 | 0.2 | I(a) | III(a) |
| Triangular | 2 | .2 | I(b) | III(b) |
| Rectangular | 2 | .2 | I(c) | III(c) |
| Body in presence of wing | | | Pressure coefficients | Longitudinal interference loading coefficients |
| Triangular | 4 | .2 | II(a) | IV(a) |
| | 2 | .2 | II(b) | IV(b) |
| | 1 | .2 | II(c) | IV(c) |
| | 1 | .4 | II(d) | IV(d) |
| | 2/3 | .4 | II(e) | ^a IV(e) |
| | 3/8 | .4 | II(f) | ^a IV(f) |
| Rectangular | 3 | .2 | II(g) | IV(g) |
| | 2 | .2 | II(h) | IV(h) |
| | 1 | .2 | II(i) | IV(i) |
| | 1 | .4 | II(j) | IV(j) |
| Body alone | | | V | --- |

^aOnly for cases of α_B variable, $\delta_W = 0^\circ$, and δ_W variable, $\alpha_B = 0^\circ$.

Force and moment data obtained from the pressure measurements and from the balance measurements are presented in graphical form. A plan view of the combination tested is shown on each basic data figure, and the shaded area indicates the component of the combination for which the data applies. The following index indicates the specific data presented in each figure.

| Mach number | Model | | | Figure number | | | | | |
|-------------|-------------|-----|-----|---------------|--------------|--------------|---------------------------|------------------------------------|---------------------------|
| | Plan form | A | r/s | $C_{N_W}(B)$ | $C_{h_W}(B)$ | $C_{b_W}(B)$ | $C_{D_W}(B)$ | $\Delta C_{N_B}(W)$ | $\Delta C_{m_B}(W)$ |
| 3.36 | Triangular | 4 | 0.2 | 4(a) | 5(a) | 6(a) | (1) | 8(a) | 9(a) |
| | | 2 | .2 | 4(b) | 5(b) | 6(b) | (1) | 8(b) | 9(b) |
| | | 1 | .2 | 4(c) | 5(c) | 6(c) | 7(a) | 8(c) | 9(c) |
| | | 1 | .4 | 4(d) | 5(d) | 6(d) | 7(b) | 8(d) | 9(d) |
| | | 2/3 | .4 | 4(e) | 5(e) | 6(e) | 7(c) | 8(e) | 9(e) |
| | Rectangular | 3/8 | .4 | 4(f) | 5(f) | 6(f) | 7(d) | 8(f) | 9(f) |
| | | 3 | .2 | 4(g) | 5(g) | (1) | 7(e) | 8(g) | 9(g) |
| | | 2 | .2 | 4(h) | 5(h) | 6(g) | (1) | 8(h) | 9(h) |
| | | 1 | .2 | 4(i) | 5(i) | 6(h) | 7(f) | 8(i) | 9(i) |
| | | 1 | .4 | 4(j) | 5(j) | 6(i) | 7(g) | 8(j) | 9(j) |
| Mach number | Plan form | A | r/s | $C_{N_{BW}}$ | $C_{m_{BW}}$ | $C_{D_{BW}}$ | $\frac{S_W}{S_B} C_{N_B}$ | $\frac{\bar{C}_S W}{DS_B} C_{m_B}$ | $\frac{S_W}{S_B} C_{D_B}$ |
| 1.98 | Triangular | 2 | .2 | 10(a) | 11(a) | 12(a) | | | |
| 1.98 | Rectangular | 1 | .2 | 10(b) | 11(b) | 12(b) | | | |
| 2.44 | Triangular | 2 | .2 | 10(c) | 11(c) | 12(c) | | | |
| 2.44 | Rectangular | 1 | .2 | 10(d) | 11(d) | 12(d) | | | |
| 3.36 | Triangular | 2 | .2 | 10(e) | 11(e) | 12(e) | | | |
| 3.36 | Rectangular | 1 | .2 | 10(f) | 11(f) | 12(f) | | | |
| 1.98 | Body alone | | | | | | 13 | 13 | 13 |
| 2.44 | Body alone | | | | | | 13 | 13 | 13 |
| 3.36 | Body alone | | | | | | 13 | 13 | 13 |

¹No data

DISCUSSION

In addition to the basic data figures, summary figures are presented to facilitate discussion of the principal effects of high angles of attack and wing deflection on force and moment coefficients. In order to separate the effects of angle of attack and wing deflection, plots were made of experimental data for the cases of variable angle of attack with zero wing deflection angle and variable wing deflection with zero angle of attack (hereinafter designated α_B variable and δ_W variable, respectively). These experimental data are also compared with corresponding values from available theory. The theoretical values were obtained by modifying the experimental wing-alone characteristics by the methods of references 11-14.

which involve the use of interference factors to account for the effects of body-wing interaction. The manner in which these interference factors were used in calculating lift and moment in the present report are developed in the appendix. Published experimental results for the wings alone can be found in references 5, 6, and 7. Small corrections to α_B and δ_W were applied, whenever necessary, to the experimental results presented in the summary figures to provide zero values of the force and moment coefficients at zero α_B and δ_W .

Component Characteristics at $M = 3.36$

In the wing-body interference theory utilized herein consideration is not given to the chordwise forces arising either from pressures or viscosity. Accordingly, calculations could only be made of the normal force or the lift component of normal force acting on the model components. Comparisons of theory with experiment for the wings and the body were more conveniently made on the basis of the lift component of normal force. These quantities are defined as follows:

$$C_{LW}^*(B) = C_{NW}(B) \cos \alpha_B; \quad \Delta C_{LB}^*(W) = \Delta C_{NB}(W) \cos \alpha_B \quad \alpha_B \text{ variable}$$

$$C_{LW}^*(B) = C_{NW}(B) \cos \delta_W; \quad \Delta C_{LB}^*(W) = \Delta C_{NB}(W) \quad \delta_W \text{ variable}$$

Lift of the wings in presence of the body.- Comparisons of theoretical with experimental lift are given in figure 14(a) for triangular wings and in figure 14(b) for rectangular wings. The theoretical values were computed by the following relationships:

$$C_{LW}^*(B) = K_W(B) C_{LW}^* \quad \alpha_B \text{ variable}$$

$$C_{LW}^*(B) = k_W(B) C_{LW}^* \quad \delta_W \text{ variable}$$

For triangular wings in the presence of the body, the theory is in good agreement with experiment in the range $\alpha_B = 0^\circ$ to 6° for the variable α_B case at all aspect ratios. For angles of attack greater than about 10° , a decrease of lift below the theoretical curve is indicated, particularly for the models having an r/s of 0.4. A similar result was found in references 3 and 4 for a rectangular wing tested in combination with a body at $M = 1.89$ and 2.93 . These decreases in lift result from a decrease in the effect of body upwash on the lift of the wing. The decreased effectiveness of body upwash above 10° angle of attack is believed to be due to the presence of body vortices since it is known that body vortices tend to reduce body upwash in the plane of the wing. An investigation at $M = 2.00$

of a body similar to that of the present tests, reported in reference 15, shows that such body vortices appear at about a body angle of attack of 10° . An approximate estimate was made of the effect of body vortices on the lift of the $A = 1$ triangular wing in presence of the body for an $r/s = 0.4$. The strengths and positions of the body vortices were assumed to be the same as those reported in reference 15 for the similar body alone at $M = 2.00$. The effective induced downwash field of the body vortices in the plane of the wing was evaluated by strip theory. As indicated in figure 14(a) the inclusion of the effects of vortex-induced downwash on the wing accounts for a large portion of the discrepancy between theory and experiment. It is evident that a method of defining the vortex field for a supersonic wing-body combination is needed for inclusion in a theory applicable at large angles of attack. Furthermore, such a method should consider possible effects of crossflow shock waves on the body flow field when the critical crossflow Mach number is exceeded.

In the variable δ_w case of figure 14(a), the theoretical values of lift are in good agreement with experimental in the range of δ_w from 0° to 20° for all aspect ratios except $A = 3/8$. At deflection angles above 20° the $A = 3/8$ wing provided greater lift than that of the wing alone at the same angles. This greater lift can be accounted for to a large extent by the following reasoning: For moderate wing deflections, the resulting breach between the deflected wing and the body is large compared to the wing semispan, due to large ratio of wing root chord to body radius. Under these conditions the wing panel behaves to some extent as an independent wing of reduced aspect ratio (for this case, $A = 3/16$). Wings of such slenderness partake of the characteristics of bodies and experience significant contributions of lift due to crossflow drag. This is apparent by the parabolic shape of the experimental lift curve (see ref. 16) indicated in figure 14(a) for the $A = 3/8$ wing in the presence of the body.

The rectangular wings in the presence of the body show about the same degree of agreement between theory and experiment over substantially the same range of c_B and δ_w as for the triangular wings.

Figure 4 shows that both plan forms exhibit no important adverse effects of combined angles of attack and deflection, and retain their normal-force effectiveness up to at least the maximum angle of the tests (approximately 45°).

Hinge moments of the wings in presence of the body. - Comparisons of theoretical with experimental hinge moments are given in figure 15(a) for triangular wings and in figure 15(b) for rectangular wings. The theoretical values were computed by the following relationships which are developed in the appendix:

Triangular wings

$$C_{hW(B)} = K_{W(B)} \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{N_W} \right\} \quad \alpha_B \text{ variable}$$

$$C_{hW(B)} = k_{W(B)} \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{N_W} \right\} \quad \delta_W \text{ variable}$$

Rectangular wings

$$C_{hW(B)} = K_{W(B)} C_{hW} \quad \alpha_B \text{ variable}$$

$$C_{hW(B)} = k_{W(B)} \left\{ C_{hW} + \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{N_W} \right\} \quad \delta_W \text{ variable}$$

For the triangular wings in the presence of the body, $r/s = 0.2$, the theoretical hinge moments are within ± 20 percent of the experimental in the range of α_B from 0° to 6° in the variable α_B case. This 20-percent hinge-moment margin represents an accuracy in prediction of the chordwise center-of-pressure positions to within $\pm 0.01 \bar{c}$. The shaded areas in figure 15 represent the contribution to $C_{hW(B)}$ by a $0.01 \bar{c}$

shift in wing center-of-pressure position. For the models having $r/s = 0.4$ in the range α_B from 0° to 6° , the agreement between theoretical and experimental wing hinge moments is not as good as for the models having $r/s = 0.2$. Above $\alpha_B = 6^\circ$, and for both values of r/s , a large discrepancy between theory and experiment occurs emphasizing the need for an accurate definition of the vortex field for wing-body combinations at high angles of attack. As in the case of lift, the effects of body vortices were approximately estimated for the $A = 1$ triangular wing, $r/s = 0.4$, and are indicated in figure 15(a).

In the variable δ_W case, the theoretical hinge moments are, in general, within ± 20 percent of the experimental, representing a maximum of $\pm 0.01 \bar{c}$ error in the chordwise center-of-pressure position in the deflection-angle range of δ_W from 0° to 25° .

For the rectangular wings the theoretical hinge moments are within ± 10 percent of the experimental throughout the angle-of-attack range for the $A = 2$ and 3 wings in the variable α_B case. The agreement between the theoretical and experimental hinge moments of the $A = 1$ wings, however, is poor. The experimental values indicate at least an $0.01 \bar{c}$ shift in the center-of-pressure position forward of that of the wing alone.

In the variable δ_W case, the agreement between theory and experiment for the rectangular plan forms of $A = 2$ and 3 over the wing deflection range of δ_W from 0° to 25° was the same as in the case of the triangular

wings. The wings of $A = 1$ gave similar agreement but over the more restricted range of δ_w from 0° to 15° .

The primary effects of wing plan form at large combined angles of δ_w and α_B can be seen by a comparison of hinge moments of triangular wings (figs. 5(a) to 5(f)) with those of the rectangular wings (figs. 5(g) to 5(j)). This comparison shows that the rectangular wing hinge moments in presence of the body are more linear with δ_w than those of the triangular wings in the higher range of α_B tested. At these high angles, an inboard loading loss occurs in the wing-body juncture due to the combined effects of body vortices and the wing-body breach resulting from wing deflection. The result is an outboard shift in wing loading approximately along the midchord line causing, in the case of triangular wings of swept-back midchord line, a corresponding rearward shift in center of pressure, as pointed out in reference 17. This rearward shift in center of loading on wings with sweptback midchord lines gives a more nonlinear hinge moment than that exhibited by wings with unswept midchord lines.

Bending moments of the wings in presence of the body. - Comparisons of theoretical with experimental bending moments are given in figure 16(a) for triangular wings and figure 16(b) for rectangular wings. The theoretical values were calculated on the assumption that the spanwise center of pressure of a wing in the presence of a body is the same as that of the wing alone. Therefore, the theoretical bending moments are given by:

$$C_{bW(B)} = K_{W(B)} C_{bW} \quad \alpha_B \text{ variable}$$

$$C_{bW(B)} = k_{W(B)} C_{bW} \quad \delta_w \text{ variable}$$

In general, the wing alone bending moments are in as good agreement with experiment as the theoretical for both plan forms. For the triangular wings, the agreement between theory and experiment is poor for the $A = 1$ wing, $r/s = 0.2$, and for the $A = 3/8$ wing, $r/s = 0.4$. The agreement for the latter is especially poor for low body and wing incidences. The poor agreement for both wings must be the result of an inboard movement of the spanwise center of pressure, inasmuch as the corresponding theoretical and experimental lifts (fig. 14(a)) are in good agreement for α_B from 0° to about 10° and for δ_w from 0° to 20° . The reasons for this inboard movement, however, are not clear. Nevertheless, for the $A = 3/8$ wing a part of the disagreement is probably due to the effect of wing-root geometry, since this wing had a nonfilleted root section and theoretical calculations were based on experimental data for a wing-alone model which had a filleted root section. For both plan forms the $A = 1$ wings, $r/s = 0.4$, show higher bending moments than could be accounted for by theory, particularly in the variable δ_w case. The reasons are not clear for the apparent large outward shift in spanwise center of loading (the outward shift is again obvious since the corresponding theoretical and experimental lifts are in good agreement).

Span load distributions of three wings in the presence of the body are presented in figure 17 and are compared with the corresponding wing-alone span load distributions. For the variable α_B case the expected increased inboard loading due to body upwash is demonstrated, particularly at $\alpha_B = 6^\circ$. For the variable δ_W case the effect of the wing-body breach is noticeable as a loss of inboard loading, particularly at $\delta_W = 20^\circ$ as compared to the wing-alone values.

Drag of the wings in the presence of the body.- In the low-incidence range the predicted drag rise $(C_D - C_{D\min})_{W(B)}$ is given by:

$$(C_D - C_{D\min})_{W(B)} = K_W(B) C_{N_W} \sin \alpha_B \quad \alpha_B \text{ variable}$$

$$(C_D - C_{D\min})_{W(B)} = k_W(B) C_{N_W} \sin \delta_W \quad \delta_W \text{ variable}$$

It was found that, for wings of both plan forms, the theoretical and experimental drag rise coefficients were in good agreement in the identical angle range of α_B from 0° to 6° , and δ_W from 0° to 20° , in which the corresponding lift coefficients were also in good agreement. Therefore, no summary figures for the drag rise coefficients are presented.

At large combined angles a small decrease of drag was effected by increasing r/s from 0.2 to 0.4 for both triangular and rectangular wings of $A = 1$ (figs. 7(a), (b), (f), and (g)). The minimum drag for all wings on which drag was measured showed little change with α_B in the range 0° to 10° ; above 10° , there was a slight increase in minimum drag with increasing α_B . This increased drag is not significant for a wing-body combination but it might be an indication that the nature of the boundary layer over the wing was affected by the body at angles greater than about $\alpha_B = 10^\circ$.

Interference lift on the body due to the wings.- Comparisons of theory and experiment are given in figure 18(a) for the body in the presence of the triangular wings and in figure 18(b) for the body in the presence of the rectangular wings. The theoretical interference lifts are given by the following expressions:

$$\Delta C_{L_B^*}(W) = K_B(W) C_{L_W^*} \quad \alpha_B \text{ variable}$$

$$\Delta C_{L_B^*}(W) = k_B(W) C_{L_W^*} \quad \delta_W \text{ variable}$$

The theoretical values of interference lift on the body in the presence of the triangular wings in the variable α_B case are in fair accord with the experimental over the range of α_B from 0° to 25° when $r/s = 0.2$. For $r/s = 0.4$, theory is in good accord with experiment in the range of

α_B from 0° to 10° ; beyond this angle range the interference lifts given by theory are too large. This discrepancy is believed to be a result of body vortices and crossflow shock waves as was pointed out in the discussion of lift on the wings. It should be noted that the lack of agreement between theoretical and experimental wing lift in the presence of the body above $\alpha_B = 10^\circ$ was, in general, also more pronounced for the configurations having an $r/s = 0.4$ than for those with an $r/s = 0.2$.

In the variable δ_W case for triangular wings, the theoretical interference lifts on the body are generally in fair accord with experimental in the range of wing deflection angles from 0° to 10° . The δ_W range wherein theory is in satisfactory agreement with experiment tends to increase with aspect ratio for both values of r/s . At larger wing deflections, the existence of a relatively large wing-body breach violates the geometrical considerations upon which the interference factor $k_{B(W)}$ is based and hence departure of theory from experiment is to be expected. Such a departure is indicated in figure 18(a) where, at large deflection angles, a decrease in interference lift occurs, resulting in negative values for some cases.

In the case of variable α_B for the body in the presence of the rectangular wings, good agreement results over the angle range between the theoretical and experimental interference lifts on the body for all aspect ratios and r/s investigated.

The comparison of the theoretical and experimental interference lift on the body due to the rectangular wings in the variable δ_W case gave essentially the same results as found for the case of the triangular wings. As indicated in figure 18, theoretical values based on a modified theory (see eq. (A1) in appendix) are generally in better agreement with experiment and the range of agreement is extended to higher deflection angles, particularly for the rectangular wings. This modified theory in effect extends slender-body interference factors to the case of a non-slender configuration.

Distributions of interference normal force on the body due to the presence of the wings are presented in figure 19. Three wing-body models are considered, among which are included combinations having the largest and smallest values of the ratio c_r/r . The theoretical loading distribution on the body computed for $\alpha_B = 6^\circ$ demonstrates a fair agreement of total loading and its distribution along the body for all three models. At $\alpha_B = 20^\circ$ the total loading was increased approximately in proportion to the angle-of-attack increase in each case; however, some change in the load distribution is indicated, particularly for the models having small c_r/r values (2.67 and 4).

For $\delta_W = 6^\circ$ the theoretical body load distribution for the long chord triangular wing model ($c_r/r = 16$) is uniformly higher than the experimental. This disagreement is due to the effect of the wing-body

breach evidenced by the small region of negative loading developed on the body near the wing leading edge. For the short chord wings the theoretical loading is in good agreement with the experimental for the triangular wing but is in poor agreement for the rectangular wing. It is notable that the use of the modified theory materially improves the agreement with the experimental load distribution for the rectangular wing case but does not alter the good agreement of slender-body theory with experiment for the triangular wing case. At $\delta_w = 30^\circ$ the distribution of load on the body for models of small c_r/r is not materially altered by the increase in wing deflection. For the model with large c_r/r , however, the large wing-body breach apparently allows a large negative loading to develop on the body forward of the wing hinge axis due to the bleeding of positive pressures on the bottom of the wing to the top of the body.

The effects of high combined angles on normal force are apparent from an examination of figure 8. The general nonlinearity of $\Delta C_{N_B}(W)$ with variation in δ_w is evident, and is only slightly affected by body angle of attack up to 25° .

Interference moment on the body due to the wings.- Comparisons of theory and experiment are given in figure 20(a) for the body in the presence of the triangular wings and in figure 20(b) for the body in the presence of the rectangular wings. The theoretical interference moments are given by the following expressions:

Triangular wings

$$\Delta C_{m_B}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{N_W} \quad \alpha_B \text{ variable}$$

$$\Delta C_{m_B}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{L_W^*} \quad \delta_w \text{ variable}$$

Rectangular wings

$$\Delta C_{m_B}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{N_W} \quad \alpha_B \text{ variable}$$

$$\Delta C_{m_B}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{L_W^*} \quad \delta_w \text{ variable}$$

In the variable α_B case, good agreement between theoretical and experimental interference moments on the body due to wings of both plan forms is found over the entire range of α_B , except for combinations having wings with the smallest ratio of root chord to body radius.

For both plan forms in the variable δ_w case, interference moments on the body given by theory are in good agreement with those of experiment in the range of wing deflection angles from 0° to 10° . Except for the two models having the smallest c_r/r , the modified theory again provided somewhat better agreement with experiment than did the slender-body theory. At large deflection angles, except for the models having large c_r/r , a decrease in the magnitude of interference moment on the body occurred due to a decrease of body loading. For the models having the largest c_r/r , however, a stabilizing couple, resulting from the large negative loading developed on the body ahead of the wing hinge line (see fig. 19(f)), compensated for the effect of the load loss on the moment. Thus, in the case of the two models of largest c_r/r , the agreement at large deflection angles between experiment and theory is good, though fortuitous.

Complete Configuration at $M = 1.98, 2.44$, and 3.36

Combined lifts of the wing-body configurations. - The configuration lift component of normal force less that of the body alone, $C_{L_{BW}}^* - C_{L_B}^*$, is compared with theory in figure 21. The equivalent theoretical values are given by the quantity $C_{L_W(B)}^* + \Delta C_{L_B(W)}^*$. The theoretical combined lifts are in good agreement with the experimental in the angle-of-attack range 0° to 6° with zero wing deflection for both plan forms.

In the case of variable wing deflection with zero body incidence, theory and experiment are in satisfactory agreement in the wing deflection range 0° to 10° for both plan forms at all test Mach numbers for which experimental data were available. At large deflection angles the effect of the resulting breach between the wing and body is to reduce the lift of the wing-body combination (excluding the body nose) to values below that of the wing alone.

No comparisons of experimental $C_{m_{BW}} - C_{m_B}$ with theoretical were made since it was found that the resulting small quantities would be of the same order as the accuracy of the experimental values.

Effects of Mach number. - The full-span models tested at the Mach numbers 1.98, 2.44, and 3.36 were not instrumented to give the division of force and moments on the body and wing. Therefore, direct comparisons of Mach number could not be made on the ranges of agreement of theoretical and experimental lifts of the wings in the presence of the body and the body in the presence of the wings. However, an examination of figure 21 shows that for the combined lifts, $C_{L_W(B)}^* + \Delta C_{L_B(W)}^*$, or the equivalent value, $C_{L_{BW}}^* - C_{L_B}^*$, there is no significant effect of Mach number on the ranges of angles of attack and wing deflection wherein theory and

experiment are in good agreement. Some effects of Mach number might be expected due to the fact that with decreasing Mach number, critical crossflow Mach numbers with their attendant effects on crossflow occur at increasing angles of attack. No direct information is available in regard to the effect of Mach number on the angles of attack at which body vortices become important. Figure 13 shows, however, that the normal-force curves for the body alone are approximately linear to about $\alpha_B = 6^\circ$ at the test Mach numbers. At higher angles, the normal-force curves become approximately parabolic in shape due to the contribution of crossflow drag (see ref. 16), implying the presence of body vortices.

CONCLUSIONS

The following conclusions are based on data from semispan triangular and rectangular wing and body combinations tested at a Mach number of 3.36.

1. The mutual interference effects of wing and body in combination can be estimated with good accuracy by means of theoretical interference factors applied to experimental wing-alone characteristics. The good agreement, however, was limited to ranges of body angles of attack α_B and wing deflections δ_W that varied with wing geometry. The minimum ranges of agreement are given as follows:

| Coefficient | α_B variable, $\delta_W = 0$ | δ_W variable, $\alpha_B = 0$ |
|-----------------------------------|-------------------------------------|-------------------------------------|
| Wings in the presence of the body | | |
| Lift coefficient | 0° to 6° | 0° to 20° |
| Hinge-moment coefficient | | |
| Triangular plan form | 0° to 6° | 0° to 25° |
| Rectangular plan form | 0° to 6° | 0° to 15° |
| Body in the presence of the wings | | |
| Interference lift coefficient | 0° to 10° | 0° to 10° |
| Interference moment coefficient | 0° to 15° | 0° to 15° |

2. A decrease of lift below the theoretical for the undeflected wings in the presence of the body occurred at body angles of attack greater than about 10° . This decrease of lift, particularly affecting the inboard wing sections, resulted from a decrease in the effect of body upwash which is believed to be due to the combined effects of body-nose vortices and transonic crossflow.

3. In combination with a body, the triangular wings of aspect ratios 2/3 and 3/8, which have large root chords compared to the body radius, showed approximately parabolic curves of lift as a function of wing deflection angle. This parabolic shape indicates significant contributions of lift due to crossflow drag of the wing at large deflection angles.

4. At large body angles of attack, the variation of hinge moments of the triangular wings in the presence of the body were more nonlinear with wing deflection than those for the rectangular wings. This was a consequence of a rearward movement of the center of pressure for the triangular wings which accompanied an outward shift occurring at high wing deflections.

5. For the triangular wing and body combinations having a large ratio of wing root chord to body radius, the opening of a relatively large wing-body gap due to wing deflection produced a large negative interference load distribution on the body forward of the wing hinge axis. This resulted in highly nonlinear interference force and moment coefficients.

On the basis of data measured at Mach numbers 1.98, 2.44, and 3.36 on two smaller scale full-span models of two of the semispan configurations, the following conclusion was evident:

1. The ranges of angles of attack and wing deflection wherein the theoretical and experimental values of the lift component of normal force of the configuration less that of the body alone were in good agreement, were insignificantly affected by Mach number.

Ames Aeronautical Laboratory
National Advisory Committee for Aeronautics
Moffett Field, Calif., Mar. 12, 1956

APPENDIX A

INTERFERENCE FACTORS

The interference factors used to compute the theoretical curves of force and moment coefficients presented in the summary figures were obtained either from slender-body theory or linear-theory solutions. In cases where both solutions were available, linear-theory factors were generally used, when applicable. The following table summarizes the particular references from which the interference factors were determined. (The superscripts S and L refer, respectively, to slender-body theory and linear theory.)

| Wing in the presence of the body | | | | Body in the presence of the wing | | | |
|---|--------------------|--|--------------------|---|--------------------|---|--------------------|
| | | | | α_B variable, $\delta_W = 0^\circ$ | | | |
| $K_W(B)$ | | | | $K_B(W)$ | | | |
| Linear | Slender-body | Linear | Slender-body | Linear | Slender-body | Linear | Slender-body |
| --- | Ref. 14, fig. 2 | --- | Ref. 14, fig. 2 | Ref. 11, fig. 4 or Ref. 12, fig. 4 Ref. 13, fig. 2 Ref. 14, fig. 5(a) | Ref. 14, fig. 2 | Ref. 11, fig. 4 or Ref. 12, fig. 4 Ref. 13, fig. 2 Ref. 14, fig. 5(a) for $BA \geq 2$ and $[K_B(W)]^S > [K_B(W)]^L$ | Ref. 14, fig. 2 |
| δ_W variable, $\alpha_B = 0^\circ$ | | | | | | | |
| $K_W(B)$ | | | | $K_B(W)$ | | | |
| --- | Ref. 14, fig. 2 | Ref. 13, fig. 3 for $BA \geq 2$ | Ref. 14, fig. 2 | Eq.(A1) present report | Ref. 14, fig. 2 | Eq.(A1) present report | Ref. 14, fig. 2 |

An estimate for a linear-theory value of $k_B(W)$ for both triangular and rectangular wings was made by the following:

$$[k_B(W)]^L = \frac{[k_B(W)]^L}{[k_B(W)]^S} [k_B(W)]^S \quad (A1)$$

In figures which involved the use of $k_B(W)$, both the slender-body value and the above modification were used.

HINGE MOMENTS OF THE WINGS IN THE PRESENCE OF THE BODY

The following general equations were used to calculate wing hinge moments:

$$C_{hW(B)} = k_W(B) \left\{ \frac{C_{hW}}{C_{NW}} + \frac{c_r}{c} \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] \right\} C_{NW} \quad \alpha_B \text{ variable} \quad (A2)$$

$$C_{hW(B)} = k_W(B) \left\{ \frac{C_{hW}}{C_{NW}} + \frac{c_r}{c} \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] \right\} C_{NW} \quad \delta_W \text{ variable} \quad (A3)$$

The term in the braces represents the center of pressure of the wing in the presence of the body obtained, as suggested in reference 13, by adding to the experimental wing-alone center of pressure, $\frac{C_{hW}}{C_{NW}}$, the theoretical shift in center of pressure, $\frac{c_r}{c} \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right]$. For triangular wings,

$\left(\frac{\bar{x}}{c_r} \right)_W = \frac{2}{3}$ and $\left(\frac{\bar{x}}{c_r} \right)_{W(B)}$ for both variable α_B and δ_W are determined from

figure 4 of reference 13. For rectangular wings, linear-theory values of $\left(\frac{\bar{x}}{c_r} \right)_W$ are given in figure 6 of reference 12; for variable α_B ,

$\left(\frac{\bar{x}}{c_r} \right)_{W(B)} = \left(\frac{\bar{x}}{c_r} \right)_W$ (see ref. 13), and for variable δ_W , values of $\left(\frac{\bar{x}}{c_r} \right)_{W(B)}$ based on linear theory for wings with $\beta A \geq 2$ are given in figure 6 of

reference 13. Rewriting equations (A2) and (A3) for specific cases:

Triangular wings

$$C_{hW}(B) = K_W(B) \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{NW} \right\} \quad \alpha_B \text{ variable} \quad (A4)$$

$$C_{hW}(B) = k_W(B) \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{NW} \right\} \quad \delta_W \text{ variable} \quad (A5)$$

Rectangular wings

$$C_{hW}(B) = K_W(B) C_{hW} \quad \alpha_B \text{ variable} \quad (A6)$$

$$C_{hW}(B) = k_W(B) \left\{ C_{hW} + \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{NW} \right\} \quad \delta_W \text{ variable} \quad (A7)$$

INTERFERENCE MOMENT ON BODY DUE TO WING

The body interference moment coefficients were calculated by the following equations:

$$\Delta C_{mB}(W) = \frac{c_r}{c} \left[\left(\frac{x}{c_r} \right)_h - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] K_B(W) C_{NW} \quad \alpha_B \text{ variable} \quad (A8)$$

$$\Delta C_{mB}(W) = \frac{c_r}{c} \left[\left(\frac{x}{c_r} \right)_h - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_B(W) C_{LW}^* \quad \delta_W \text{ variable} \quad (A9)$$

where for both variable α_B and δ_W , values of $\left(\frac{\bar{x}}{c_r} \right)_{B(W)}$ based on linear theory are given in figure 7 of reference 12 or figure 20 of reference 14. For specific cases equations (A8) and (A9) become:

Triangular wings

$$\Delta C_{mB}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] K_B(W) C_{NW} \quad \alpha_B \text{ variable} \quad (A10)$$

$$\Delta C_{mB}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{LW}^* \quad \delta_w \text{ variable} \quad (\text{Al1})$$

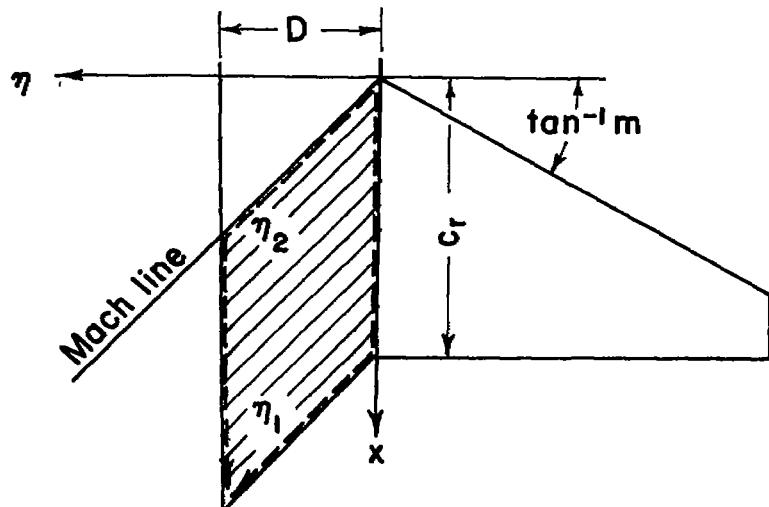
Rectangular wings

$$\Delta C_{mB}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] K_{B(W)} C_{NW} \quad \alpha_B \text{ variable} \quad (\text{Al2})$$

$$\Delta C_{mB}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{LW}^* \quad \delta_w \text{ variable} \quad (\text{Al3})$$

DISTRIBUTION OF INTERFERENCE NORMAL FORCE
ON THE BODY DUE TO THE WINGS

The theoretical body interference loading coefficient as a function of x , the distance along the body from the juncture of the body and the wing leading edge, calculated for variable α_B by the following integrals from reference 11. The variables of integration are defined in the accompanying sketch.



Supersonic-leading-edge wing

$$\Delta c_{nB}(W) = \frac{8\alpha_B}{\pi D \sqrt{\beta^2 m^2 - 1}} \int_{\eta_1}^{\eta_2} \cos^{-1} \frac{x/\beta - \beta m \eta}{\eta + mx} d\eta$$

$$= \frac{8\alpha_B}{\pi D \sqrt{\beta^2 m^2 - 1}} \left[\frac{\pi}{2} \eta - (\eta + mx) \sin^{-1} \left(\frac{x/\beta + \beta m \eta}{\eta + mx} \right) + \sqrt{\beta^2 m^2 - 1} \frac{x}{\beta} \sin^{-1} \frac{\eta}{x/\beta} \right]_{\eta_1}^{\eta_2}$$
(A14)

Subsonic-leading-edge wing

$$\Delta c_{nB}(W) = \frac{16(\beta m)^{3/2} \alpha_B}{\pi D \beta (\beta m + 1)} \int_{\eta_1}^{\eta_2} \frac{\sqrt{x/\beta - \eta}}{\sqrt{mx + \eta}} d\eta$$

$$= \frac{16(\beta m)^{3/2} \alpha_B}{\pi D \beta (\beta m + 1)} \left[\sqrt{(x/\beta - \eta)(mx + \eta)} + \frac{x/\beta(\beta m + 1)}{2} \tan^{-1} \sqrt{\frac{mx + \eta}{x/\beta - \eta}} \right]_{\eta_1}^{\eta_2}$$
(A15)

The loading for variable δ_W was then obtained by:

$$\left[\Delta c_{nB}(W) \right]_{\delta_W \text{ variable}} = \frac{\delta_W}{\alpha_B} \left[\frac{k_B(W)}{K_B(W)} \right] \left[\Delta c_{nB}(W) \right]_{\alpha_B \text{ variable}} \quad (A16)$$

wherein both the slender-body value of $k_B(W)$ and the linear-theory approximation (modified theory) given by equation (A1) were used.

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NACA RM A56C12

TABLE I.- PRESSURE COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY
 (a) $A = \frac{1}{4}$ triangular wing, $r/s = 0.2$

| y/s | x_0 | $\delta_w, \alpha_B = 0^\circ$ | | | | | | | | | | | | $\alpha_B, \delta_w = 0^\circ$ | | | | | | | | | | | |
|---------------|-------|--------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------------------------------|--------|--------|--------|--------|--------|--|--|--|--|--|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | | | | | | |
| Upper Surface | .025 | 103 | .085 | .076 | .085 | .078 | .070 | .059 | .047 | .014 | .180 | .105 | .070 | .022 | .037 | .066 | .074 | .081 | .078 | | | | | | |
| | .051 | - .081 | - .071 | - .079 | - .073 | - .059 | - .049 | - .034 | - .004 | - .131 | - .093 | - .063 | - .019 | - .016 | - .049 | - .074 | - .083 | - .083 | | | | | | | |
| | .078 | - .083 | - .071 | - .076 | - .074 | - .065 | - .054 | - .038 | - .009 | - .109 | - .076 | - .047 | - .009 | - .017 | - .054 | - .069 | - .079 | - .085 | | | | | | | |
| | .087 | - .080 | - .069 | - .075 | - .075 | - .067 | - .059 | - .045 | - .019 | - .081 | - .050 | - .028 | - .000 | - .021 | - .053 | - .065 | - .075 | - .085 | | | | | | | |
| | .079 | - .089 | - .085 | - .092 | - .091 | - .086 | - .080 | - .075 | - .071 | - .035 | - .051 | - .054 | - .051 | - .063 | - .071 | - .081 | - .098 | - .095 | | | | | | | |
| | .072 | - .081 | - .079 | - .087 | - .083 | - .082 | - .074 | - .069 | - .068 | - .026 | - .029 | - .034 | - .038 | - .049 | - .067 | - .071 | - .082 | - .091 | | | | | | | |
| | .075 | - .085 | - .068 | - .079 | - .090 | - .089 | - .080 | - .073 | - .061 | - .053 | - .013 | - .005 | - .083 | - .038 | - .042 | - .064 | - .075 | - .087 | | | | | | | |
| | .085 | - .087 | - .079 | - .089 | - .087 | - .078 | - .069 | - .062 | - .035 | - .175 | - .114 | - .066 | - .011 | - .039 | - .062 | - .074 | - .076 | - .076 | | | | | | | |
| | .060 | - .087 | - .076 | - .089 | - .085 | - .081 | - .071 | - .065 | - .044 | - .149 | - .091 | - .047 | - .000 | - .030 | - .064 | - .076 | - .079 | - .081 | | | | | | | |
| | .075 | - .085 | - .077 | - .090 | - .088 | - .088 | - .074 | - .068 | - .051 | - .125 | - .071 | - .032 | - .011 | - .044 | - .070 | - .078 | - .088 | - .087 | | | | | | | |
| | .050 | - .088 | - .088 | - .091 | - .089 | - .085 | - .076 | - .068 | - .056 | - .097 | - .049 | - .017 | - .028 | - .050 | - .068 | - .083 | - .087 | - .091 | | | | | | | |
| | .088 | - .090 | - .088 | - .093 | - .091 | - .086 | - .077 | - .074 | - .062 | - .081 | - .037 | - .009 | - .031 | - .054 | - .073 | - .083 | - .089 | - .095 | | | | | | | |
| | .075 | - .087 | - .088 | - .091 | - .089 | - .081 | - .073 | - .067 | - .061 | - .065 | - .026 | - .008 | - .030 | - .052 | - .067 | - .081 | - .087 | - .091 | | | | | | | |
| | .075 | - .080 | - .070 | - .088 | - .088 | - .078 | - .067 | - .064 | - .061 | - .053 | - .015 | - .004 | - .038 | - .054 | - .068 | - .074 | - .080 | - .088 | | | | | | | |
| | .066 | - .080 | - .071 | - .089 | - .087 | - .079 | - .070 | - .068 | - .058 | - .000 | - .037 | - .007 | - .057 | - .068 | - .076 | - .082 | - .088 | - .090 | | | | | | | |
| Lower Surface | .250 | 185 | - .068 | - .081 | - .090 | - .090 | - .079 | - .070 | - .065 | - .040 | - .180 | - .097 | - .055 | - .010 | - .080 | - .054 | - .067 | - .068 | - .069 | | | | | | |
| | .250 | - .082 | - .076 | - .089 | - .087 | - .078 | - .071 | - .068 | - .047 | - .141 | - .080 | - .043 | - .002 | - .027 | - .050 | - .068 | - .071 | - .075 | | | | | | | |
| | .088 | - .088 | - .077 | - .088 | - .087 | - .078 | - .068 | - .055 | - .058 | - .099 | - .046 | - .018 | - .041 | - .066 | - .078 | - .088 | - .092 | - .098 | | | | | | | |
| | .075 | - .080 | - .076 | - .088 | - .087 | - .078 | - .068 | - .056 | - .067 | - .081 | - .031 | - .004 | - .035 | - .051 | - .066 | - .077 | - .088 | - .090 | | | | | | | |
| | .078 | - .078 | - .071 | - .087 | - .085 | - .074 | - .068 | - .054 | - .066 | - .061 | - .010 | - .000 | - .035 | - .055 | - .061 | - .071 | - .078 | - .080 | | | | | | | |
| | .075 | - .076 | - .074 | - .086 | - .088 | - .075 | - .067 | - .061 | - .050 | - .099 | - .085 | - .000 | - .007 | - .085 | - .049 | - .065 | - .067 | - .066 | | | | | | | |
| | .065 | - .076 | - .071 | - .086 | - .083 | - .076 | - .068 | - .066 | - .063 | - .076 | - .041 | - .003 | - .008 | - .035 | - .050 | - .059 | - .070 | - .078 | | | | | | | |
| | .090 | - .076 | - .077 | - .086 | - .087 | - .076 | - .069 | - .063 | - .063 | - .041 | - .003 | - .003 | - .035 | - .051 | - .055 | - .068 | - .070 | - .066 | | | | | | | |
| | .085 | - .085 | - .087 | - .087 | - .086 | - .086 | - .081 | - .075 | - .068 | - .058 | - .004 | - .048 | - .030 | - .083 | - .000 | - .035 | - .078 | - .077 | - .077 | | | | | | |
| | .085 | - .075 | - .068 | - .087 | - .086 | - .080 | - .074 | - .065 | - .058 | - .045 | - .015 | - .045 | - .025 | - .070 | - .131 | - .018 | - .054 | - .066 | - .069 | | | | | | |
| | .071 | - .085 | - .071 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .043 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .078 | - .085 | - .087 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .078 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .078 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .078 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |
| | .075 | - .085 | - .077 | - .087 | - .084 | - .074 | - .065 | - .059 | - .053 | - .047 | - .019 | - .043 | - .027 | - .072 | - .112 | - .024 | - .050 | - .067 | - .072 | | | | | | |

TABLE I.- PRESSURE COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - Continued
 (b) A = 2 triangular wing, r/s = 0.2

| y_s | z/c | $\delta_w, \alpha_B = 0^\circ$ | | | | | | | | | | $\alpha_B, \delta_w = 0^\circ$ | | | | | | |
|-------|--------------------|---|-----|-----|-----|-----|-----|-----|-----|----|----|--------------------------------|----|----|-----|-----|-----|-----|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° |
| .025 | Upper surface .250 | 103 - .090 - .085 - .091 - .080 - .088 - .069 - .041 - .034 - .004 - .010 - .032 - .008 - .063 - .091 - .050 - .068 - .061 | | | | | | | | | | | | | | | | |
| | | 231 - .095 - .088 - .088 - .076 - .071 - .064 - .047 - .030 - .010 - .001 - .017 - .014 - .049 - .073 - .052 - .075 - .074 | | | | | | | | | | | | | | | | |
| | | 339 - .091 - .085 - .082 - .070 - .069 - .063 - .049 - .037 - .015 - .003 - .013 - .009 - .046 - .078 - .043 - .075 - .074 | | | | | | | | | | | | | | | | |
| | | 487 - .093 - .088 - .086 - .073 - .070 - .065 - .057 - .041 - .017 - .008 - .007 - .010 - .044 - .074 - .052 - .076 - .079 | | | | | | | | | | | | | | | | |
| | | 583 - .092 - .089 - .091 - .079 - .078 - .070 - .068 - .043 - .014 - .000 - .007 - .003 - .033 - .063 - .054 - .076 - .077 | | | | | | | | | | | | | | | | |
| | | 744 - .089 - .088 - .097 - .086 - .088 - .082 - .074 - .061 - .048 - .038 - .028 - .030 - .057 - .082 - .053 - .082 - .081 | | | | | | | | | | | | | | | | |
| | | 878 - .077 - .074 - .086 - .078 - .081 - .074 - .064 - .051 - .038 - .015 - .013 - .017 - .050 - .075 - .035 - .076 - .073 | | | | | | | | | | | | | | | | |
| | | 976 - .067 - .065 - .082 - .074 - .078 - .069 - .058 - .044 - .030 - .019 - .000 - .015 - .044 - .073 - .043 - .078 - .074 | | | | | | | | | | | | | | | | |
| | | 104 - .094 - .089 - .095 - .087 - .091 - .085 - .071 - .058 - .016 - .011 - .051 - .008 - .063 - .090 - .058 - .081 - .081 | | | | | | | | | | | | | | | | |
| | | 889 - .093 - .090 - .095 - .088 - .092 - .086 - .074 - .056 - .026 - .001 - .029 - .009 - .068 - .086 - .050 - .079 - .081 | | | | | | | | | | | | | | | | |
| .500 | Upper surface .500 | 354 - .076 - .078 - .082 - .078 - .080 - .076 - .064 - .051 - .025 - .006 - .014 - .017 - .067 - .075 - .050 - .074 - .074 | | | | | | | | | | | | | | | | |
| | | 500 - .086 - .081 - .100 - .093 - .094 - .090 - .076 - .062 - .037 - .025 - .011 - .014 - .068 - .087 - .064 - .080 - .087 | | | | | | | | | | | | | | | | |
| | | 685 - .092 - .091 - .098 - .094 - .093 - .089 - .076 - .061 - .040 - .029 - .010 - .032 - .066 - .085 - .061 - .083 - .085 | | | | | | | | | | | | | | | | |
| | | 750 - .076 - .075 - .089 - .082 - .086 - .088 - .073 - .058 - .037 - .023 - .011 - .016 - .055 - .081 - .058 - .082 - .082 | | | | | | | | | | | | | | | | |
| | | 878 - .077 - .078 - .098 - .091 - .093 - .089 - .076 - .055 - .039 - .029 - .015 - .017 - .062 - .085 - .051 - .083 - .083 | | | | | | | | | | | | | | | | |
| | | 969 - .068 - .066 - .086 - .088 - .091 - .087 - .076 - .056 - .040 - .029 - .017 - .011 - .061 - .087 - .057 - .087 - .088 | | | | | | | | | | | | | | | | |
| | | 125 - .089 - .090 - .097 - .089 - .091 - .088 - .076 - .056 - .020 - .006 - .067 - .008 - .057 - .082 - .054 - .077 - .081 | | | | | | | | | | | | | | | | |
| | | 250 - .089 - .088 - .097 - .089 - .092 - .089 - .078 - .063 - .030 - .003 - .038 - .004 - .068 - .086 - .057 - .080 - .080 | | | | | | | | | | | | | | | | |
| | | 378 - .087 - .086 - .097 - .090 - .093 - .090 - .080 - .067 - .038 - .013 - .028 - .014 - .068 - .087 - .058 - .083 - .083 | | | | | | | | | | | | | | | | |
| | | 800 - .086 - .087 - .097 - .090 - .093 - .091 - .083 - .069 - .048 - .019 - .013 - .017 - .068 - .085 - .054 - .081 - .081 | | | | | | | | | | | | | | | | |
| .750 | .750 | 625 - .085 - .088 - .098 - .092 - .095 - .093 - .087 - .075 - .047 - .027 - .001 - .025 - .071 - .086 - .056 - .083 - .083 | | | | | | | | | | | | | | | | |
| | | 750 - .081 - .087 - .098 - .098 - .095 - .095 - .086 - .075 - .051 - .032 - .010 - .033 - .069 - .080 - .057 - .086 - .086 | | | | | | | | | | | | | | | | |
| | | 878 - .073 - .073 - .086 - .076 - .088 - .068 - .074 - .061 - .037 - .008 - .006 - .004 - .057 - .069 - .047 - .066 - .065 | | | | | | | | | | | | | | | | |
| | | 985 - .076 - .076 - .087 - .087 - .089 - .088 - .081 - .069 - .054 - .034 - .016 - .034 - .069 - .074 - .043 - .080 - .075 | | | | | | | | | | | | | | | | |
| | | 156 - .080 - .081 - .095 - .089 - .092 - .089 - .078 - .058 - .018 - .010 - .057 - .014 - .044 - .075 - .063 - .078 - .078 | | | | | | | | | | | | | | | | |
| | | 250 - .081 - .083 - .098 - .094 - .097 - .095 - .085 - .065 - .029 - .003 - .044 - .002 - .044 - .077 - .065 - .087 - .087 | | | | | | | | | | | | | | | | |
| | | 375 - .079 - .081 - .094 - .091 - .093 - .090 - .080 - .064 - .034 - .011 - .031 - .005 - .056 - .075 - .049 - .078 - .077 | | | | | | | | | | | | | | | | |
| | | 500 - .078 - .080 - .093 - .089 - .093 - .089 - .080 - .067 - .041 - .019 - .024 - .014 - .057 - .075 - .050 - .079 - .079 | | | | | | | | | | | | | | | | |
| | | 750 - .078 - .078 - .098 - .090 - .091 - .089 - .083 - .073 - .051 - .031 - .008 - .003 - .044 - .064 - .077 - .050 - .077 - .077 | | | | | | | | | | | | | | | | |
| | | 969 - .070 - .075 - .090 - .087 - .090 - .088 - .081 - .070 - .057 - .037 - .003 - .027 - .046 - .066 - .073 - .047 - .080 - .077 | | | | | | | | | | | | | | | | |
| .875 | .875 | 500 - .070 - .076 - .089 - .088 - .092 - .090 - .081 - .066 - .037 - .014 - .025 - .007 - .054 - .074 - .049 - .080 - .079 | | | | | | | | | | | | | | | | |
| | | 688 - .070 - .075 - .090 - .090 - .091 - .090 - .088 - .070 - .046 - .025 - .010 - .018 - .059 - .077 - .053 - .082 - .079 | | | | | | | | | | | | | | | | |

TABLE I.- PRESSURE COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - Continued
 (b) A = 2 triangular wing, r/s = 0.2 - Concluded

| $\frac{V_w}{V_c}$ | $\frac{V_b}{V_c}$ | $\delta_w, \alpha_b = 0^\circ$ | | | | | | | | | | | | $\alpha_b, \delta_w = 0^\circ$ | | | | | | |
|-------------------|-------------------|--------------------------------|-------|------|------|------|------|------|-------|-------|-------|------|------|--------------------------------|------|------|------|------|--|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | |
| .025 | 1.03 | 1.836 | 1.074 | .897 | .785 | .545 | .408 | .384 | .152 | .095 | .059 | .038 | .063 | .138 | .209 | .311 | .494 | .695 | | |
| | 1.031 | 1.194 | 1.004 | .833 | .667 | .499 | .350 | .331 | .125 | .073 | .040 | .017 | .057 | .109 | .184 | .089 | .457 | .645 | | |
| | 1.039 | 1.182 | .948 | .776 | .619 | .461 | .356 | .239 | .100 | .056 | .032 | .013 | .048 | .083 | .147 | .240 | .391 | .561 | | |
| | 1.047 | 1.930 | .833 | .664 | .746 | .581 | .331 | .185 | .079 | .046 | .026 | .007 | .038 | .073 | .128 | .221 | .358 | .514 | | |
| | 1.053 | 1.190 | .951 | .736 | .513 | .348 | .284 | .139 | .063 | .034 | .018 | .007 | .086 | .059 | .111 | .197 | .386 | .476 | | |
| | 1.054 | .740 | .644 | .485 | .346 | .228 | .137 | .071 | .007 | - | .020 | - | .022 | - | .020 | - | .026 | .275 | | |
| | 1.078 | 1.206 | 1.049 | .688 | .457 | .269 | .141 | .061 | -.004 | -.013 | -.003 | .013 | .010 | .041 | .098 | .189 | .399 | .443 | | |
| | 1.076 | 1.260 | 1.090 | .761 | .461 | .245 | .118 | .039 | .011 | .006 | .017 | .000 | .026 | .057 | .110 | .189 | .383 | .470 | | |
| | 1.084 | 1.806 | 1.047 | .888 | .741 | .583 | .439 | .384 | .203 | .144 | .094 | .051 | .118 | .165 | .235 | .338 | .499 | .673 | | |
| | 1.089 | 1.408 | .987 | .836 | .661 | .511 | .373 | .263 | .168 | .105 | .064 | .029 | .076 | .119 | .184 | .281 | .433 | .609 | | |
| .250 | 1.136 | 1.169 | .934 | .636 | .488 | .391 | .248 | .187 | .058 | .044 | .017 | .041 | .080 | .152 | .244 | .368 | .553 | | | |
| | 1.180 | .868 | .717 | .578 | .436 | .319 | .201 | .090 | .047 | .017 | .011 | .086 | .163 | .222 | .308 | .444 | .508 | | | |
| | 1.195 | .837 | .688 | .581 | .405 | .274 | .148 | .070 | .034 | .008 | .010 | .015 | .051 | .103 | .186 | .349 | .476 | | | |
| | 1.250 | 1.030 | .774 | .601 | .467 | .346 | .235 | .160 | .061 | .027 | .007 | .081 | .165 | .245 | .376 | .511 | .579 | | | |
| | 1.275 | 1.058 | .866 | .660 | .461 | .331 | .215 | .138 | .049 | .019 | .001 | .015 | .011 | .048 | .102 | .179 | .305 | .444 | | |
| | 1.289 | 1.034 | .936 | .691 | .507 | .343 | .236 | .134 | .046 | .017 | .001 | .017 | .011 | .039 | .094 | .144 | .368 | .584 | | |
| | 1.295 | 1.083 | 1.093 | .836 | .661 | .573 | .449 | .338 | .228 | .164 | .110 | .057 | .189 | .162 | .256 | .349 | .491 | .661 | | |
| | 1.300 | 1.047 | .972 | .911 | .688 | .535 | .401 | .291 | .179 | .122 | .078 | .038 | .095 | .136 | .209 | .311 | .451 | .685 | | |
| | 1.375 | 1.070 | .874 | .805 | .488 | .548 | .398 | .280 | .156 | .102 | .059 | .026 | .069 | .113 | .188 | .274 | .419 | .584 | | |
| | 1.400 | 1.081 | .976 | .807 | .651 | .507 | .370 | .258 | .136 | .086 | .043 | .013 | .043 | .095 | .164 | .240 | .404 | .576 | | |
| .500 | 1.063 | .877 | .787 | .615 | .467 | .330 | .230 | .169 | .069 | .035 | .027 | .001 | .026 | .073 | .136 | .227 | .372 | .536 | | |
| | 1.121 | 1.860 | .740 | .568 | .440 | .309 | .199 | .093 | .047 | .017 | .010 | .019 | .068 | .132 | .213 | .359 | .586 | | | |
| | 1.100 | .926 | .709 | .561 | .417 | .292 | .185 | .066 | .031 | .017 | .006 | .010 | .040 | .101 | .174 | .316 | .501 | | | |
| | 1.118 | .875 | .686 | .548 | .400 | .269 | .171 | .065 | .037 | .003 | .016 | .007 | .042 | .103 | .189 | .334 | .510 | | | |
| | 1.186 | 1.073 | .970 | .834 | .786 | .640 | .503 | .395 | .269 | .199 | .128 | .057 | .143 | .218 | .304 | .404 | .540 | .680 | | |
| | 1.250 | 1.153 | 1.012 | .861 | .766 | .636 | .491 | .371 | .246 | .186 | .111 | .044 | .129 | .194 | .276 | .383 | .525 | .679 | | |
| | 1.278 | 1.166 | 1.046 | .897 | .742 | .606 | .467 | .336 | .201 | .139 | .087 | .031 | .103 | .160 | .237 | .340 | .489 | .655 | | |
| | 1.300 | 1.164 | 1.038 | .984 | .751 | .599 | .461 | .317 | .179 | .118 | .071 | .020 | .063 | .131 | .191 | .317 | .473 | .658 | | |
| | 1.378 | 1.107 | .959 | .808 | .684 | .541 | .407 | .286 | .147 | .098 | .041 | .008 | .050 | .104 | .178 | .279 | .438 | .588 | | |
| | 1.404 | .867 | .716 | .589 | .468 | .341 | .237 | .128 | .066 | .026 | -.003 | .008 | .075 | .143 | .239 | .388 | .551 | | | |
| .750 | 1.121 | 1.921 | .990 | .885 | .740 | .626 | .498 | .374 | .241 | .163 | .089 | .025 | .101 | .175 | .269 | .384 | .510 | .697 | | |
| | 1.139 | .986 | .837 | .709 | .574 | .449 | .331 | .198 | .134 | .070 | .010 | .052 | .149 | .239 | .348 | .501 | .660 | | | |
| .775 | 1.139 | 1.139 | .986 | .837 | .709 | .574 | .449 | .331 | .198 | .134 | .070 | .010 | .052 | .149 | .239 | .348 | .501 | .660 | | |
| | 1.168 | 1.168 | .986 | .837 | .709 | .574 | .449 | .331 | .198 | .134 | .070 | .010 | .052 | .149 | .239 | .348 | .501 | .660 | | |

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TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS
 (a) $A = 4$ triangular wing, $r/s = 0.2$

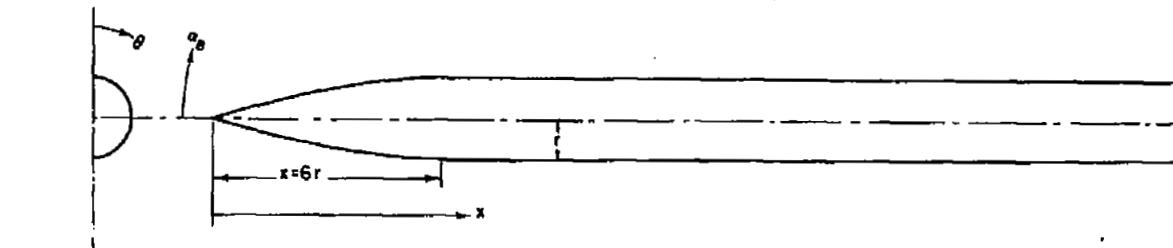


TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (a) $A = 4$ triangular wing, $r/s = 0.2$ - Concluded.

| θ | x/r | $\delta_w, \alpha_B = 0^\circ$ | | | | | | | | | | $\alpha_B, \delta_w = 0^\circ$ | | | | | | |
|----------|-------|--------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------------------------------|--------|--------|--------|-------|-------|--|
| | | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | |
| 120° | 11.34 | -0.019 | -0.018 | -0.020 | -0.020 | -0.019 | -0.019 | -0.018 | -0.019 | -0.019 | -0.019 | -0.020 | -0.018 | -0.005 | 0.000 | 1.16 | 1.16 | |
| | 12.59 | -0.010 | -0.007 | -0.010 | -0.008 | -0.008 | -0.009 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | -0.007 | 0.007 | 1.189 | 1.189 | |
| | 13.84 | -0.013 | -0.012 | -0.014 | -0.013 | -0.012 | -0.013 | -0.013 | -0.013 | -0.013 | -0.013 | -0.013 | -0.013 | -0.007 | 0.007 | 1.187 | 1.187 | |
| | 15.09 | -0.028 | -0.028 | -0.029 | -0.029 | -0.028 | -0.028 | -0.029 | -0.028 | -0.028 | -0.028 | -0.028 | -0.028 | -0.008 | 0.008 | 1.187 | 1.187 | |
| | 16.34 | -0.050 | -0.051 | -0.048 | -0.047 | -0.047 | -0.043 | -0.043 | -0.043 | -0.043 | -0.043 | -0.043 | -0.043 | -0.041 | -0.041 | 1.160 | 1.160 | |
| | 17.59 | -0.058 | -0.058 | -0.067 | -0.045 | -0.043 | -0.043 | -0.043 | -0.043 | -0.043 | -0.043 | -0.043 | -0.043 | -0.072 | -0.072 | 1.160 | 1.160 | |
| | 18.84 | -0.054 | -0.048 | -0.070 | -0.061 | -0.024 | -0.000 | -0.015 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.027 | -0.027 | 1.08 | 1.08 | |
| | 20.09 | -0.046 | -0.050 | -0.074 | -0.037 | -0.011 | -0.009 | -0.011 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.065 | -0.065 | 1.174 | 1.174 | |
| | 21.34 | -0.059 | -0.059 | -0.047 | -0.038 | -0.016 | -0.001 | -0.004 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | -0.054 | -0.054 | 1.174 | 1.174 | |
| | 22.59 | -0.059 | -0.059 | -0.051 | -0.030 | -0.018 | -0.001 | -0.006 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.054 | -0.054 | 1.174 | 1.174 | |
| | 23.84 | -0.059 | -0.059 | -0.055 | -0.036 | -0.004 | -0.008 | -0.010 | -0.009 | -0.009 | -0.009 | -0.009 | -0.009 | -0.048 | -0.048 | 1.174 | 1.174 | |
| | 25.09 | -0.016 | -0.028 | -0.007 | -0.007 | -0.000 | -0.011 | -0.015 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.103 | -0.103 | 1.174 | 1.174 | |
| 150° | 11.34 | -0.018 | -0.010 | -0.018 | -0.013 | -0.018 | -0.018 | -0.011 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.076 | -0.076 | 1.180 | 1.180 | |
| | 12.59 | -0.010 | -0.007 | -0.007 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 13.84 | -0.010 | -0.011 | -0.014 | -0.012 | -0.011 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 15.09 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 16.34 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 17.59 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 18.84 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 20.09 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 21.34 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 22.59 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 23.84 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| | 25.09 | -0.014 | -0.016 | -0.012 | -0.007 | -0.006 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.067 | -0.067 | 1.180 | 1.180 | |
| 165° | 11.34 | -0.016 | -0.015 | -0.018 | -0.016 | -0.016 | -0.016 | -0.015 | -0.015 | -0.015 | -0.015 | -0.015 | -0.015 | -0.15 | -0.15 | 1.140 | 1.140 | |
| | 12.59 | -0.010 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 13.84 | -0.010 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 15.09 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 16.34 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 17.59 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 18.84 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 20.09 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 21.34 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 22.59 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 23.84 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| | 25.09 | -0.014 | -0.014 | -0.014 | -0.007 | -0.006 | -0.006 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.140 | 1.140 | |
| 174° | 11.34 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 | -0.11 | -0.11 | 1.110 | 1.110 | |
| | 12.59 | -0.010 | -0.006 | -0.009 | -0.009 | -0.009 | -0.009 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 13.84 | -0.010 | -0.006 | -0.009 | -0.009 | -0.009 | -0.009 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.007 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 15.09 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 16.34 | -0.056 | -0.056 | -0.051 | -0.041 | -0.059 | -0.005 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 17.59 | -0.055 | -0.055 | -0.050 | -0.030 | -0.059 | -0.005 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 18.84 | -0.051 | -0.048 | -0.047 | -0.048 | -0.051 | -0.004 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 20.09 | -0.051 | -0.048 | -0.047 | -0.048 | -0.051 | -0.004 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 21.34 | -0.059 | -0.059 | -0.054 | -0.050 | -0.054 | -0.004 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 22.59 | -0.057 | -0.057 | -0.052 | -0.048 | -0.055 | -0.004 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 23.84 | -0.057 | -0.057 | -0.052 | -0.048 | -0.055 | -0.004 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.067 | -0.067 | 1.110 | 1.110 | |
| | 25.09 | -0.051 | -0.051 | -0.051 | -0.048 | -0.051 | -0.004 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.067 | -0.067 | 1.110 | 1.110 | |

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$ - Concluded

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (e) $A = 2/3$ triangular wing, $r/s = 0.4$ - Concluded

| θ | x/r | $\delta_W, \alpha_B = 0^\circ$ | | | | | | | | | | | | $\delta_W, \alpha_B = 0^\circ$ | | | | | | |
|----------|-------|--------------------------------|------|------|------|------|------|------|------|------|------|------|------|--------------------------------|------|------|------|------|------|------|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | |
| 120° | 6.94 | .086 | .029 | .029 | .029 | .026 | .031 | .026 | .026 | .026 | .027 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 |
| | 8.37 | .086 | .029 | .029 | .029 | .026 | .028 | .029 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 |
| | 9.81 | .087 | .031 | .030 | .030 | .029 | .029 | .029 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 | .028 |
| | 11.25 | .087 | .028 | .023 | .023 | .021 | .022 | .024 | .023 | .023 | .023 | .023 | .023 | .023 | .023 | .023 | .023 | .023 | .023 | .023 |
| | 12.69 | .087 | .016 | .016 | .016 | .015 | .015 | .017 | .016 | .015 | .014 | .014 | .014 | .014 | .014 | .014 | .014 | .014 | .014 | .014 |
| | 14.13 | .087 | .017 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 | .018 |
| | 15.56 | .087 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 |
| | 17.00 | .087 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 |
| | 18.44 | .087 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 |
| | 19.87 | .087 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 |
| | 21.31 | .087 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 | .004 |
| | 22.75 | .087 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 | .017 |
| | 24.19 | .087 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 |
| | 25.63 | .087 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 150° | 6.94 | .050 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 | .030 |
| | 8.37 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 |
| | 9.81 | .027 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 |
| | 11.25 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 |
| | 12.69 | .026 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 |
| | 14.13 | .026 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 |
| | 15.56 | .026 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 |
| | 17.00 | .026 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 |
| | 18.44 | .026 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 | .068 |
| | 19.87 | .026 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 | .015 |
| | 21.31 | .026 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 |
| | 24.19 | .026 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 |
| | 25.63 | .026 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 |
| 165° | 6.94 | .031 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 | .029 |
| | 8.37 | .026 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 |
| | 9.81 | .026 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 |
| | 11.25 | .026 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 | .016 |
| | 12.69 | .026 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 |
| | 14.13 | .026 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 |
| | 15.56 | .026 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 | .069 |
| | 17.00 | .026 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 | .036 |
| | 18.44 | .026 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 | .007 |
| | 19.87 | .026 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 | .011 |
| | 21.31 | .026 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 | .006 |
| | 24.19 | .026 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 | .010 |
| | 25.63 | .026 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 | .009 |
| 174° | 6.94 | .066 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 | .026 |
| | 8.37 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 | .024 |

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
(f) $A = 3/8$ triangular wing, $r/s = 0.4$

| θ | x_r | $\delta_w, \alpha_B = 0^\circ$ | | | | | | | | | | | | | $\alpha_B, \delta_w = 0^\circ$ | | | | | | | | | | | | |
|----------|-------|--------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------------------------------|-------|-------|-------|--|--|--|--|--|--|--|--|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | | | | | | | | |
| 6° | 694 | -0.33 | -0.34 | -0.33 | -0.27 | -0.26 | -0.25 | -0.29 | -0.29 | -0.29 | -0.27 | -0.28 | -0.41 | -0.42 | -0.41 | -0.50 | -0.51 | -0.50 | | | | | | | | | |
| | 837 | -0.25 | -0.25 | -0.24 | -0.20 | -0.18 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.32 | -0.32 | -0.32 | -0.50 | -0.50 | -0.50 | | | | | | | | | |
| | 981 | -0.21 | -0.21 | -0.20 | -0.16 | -0.16 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.29 | -0.29 | -0.29 | -0.54 | -0.54 | -0.54 | | | | | | | | | |
| | 1125 | -0.21 | -0.21 | -0.20 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.61 | -0.61 | -0.61 | | | | | | | | | |
| | 1269 | -0.20 | -0.20 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.21 | -0.21 | -0.21 | -0.67 | -0.67 | -0.67 | | | | | | | | | |
| | 1412 | -0.20 | -0.20 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.21 | -0.21 | -0.21 | -0.61 | -0.61 | -0.61 | | | | | | | | | |
| | 1556 | -0.20 | -0.20 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.21 | -0.21 | -0.21 | -0.67 | -0.67 | -0.67 | | | | | | | | | |
| | 1700 | -0.19 | -0.19 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.17 | -0.17 | -0.17 | -0.64 | -0.64 | -0.64 | | | | | | | | | |
| | 1844 | -0.19 | -0.19 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.17 | -0.17 | -0.17 | -0.75 | -0.75 | -0.75 | | | | | | | | | |
| | 1987 | -0.19 | -0.19 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.17 | -0.17 | -0.17 | -0.71 | -0.71 | -0.71 | | | | | | | | | |
| 15° | 2131 | -0.19 | -0.19 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.16 | -0.16 | -0.16 | -0.69 | -0.69 | -0.69 | | | | | | | | | |
| | 2275 | -0.19 | -0.19 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.16 | -0.16 | -0.16 | -0.69 | -0.69 | -0.69 | | | | | | | | | |
| | 2419 | -0.19 | -0.19 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.16 | -0.16 | -0.16 | -0.69 | -0.69 | -0.69 | | | | | | | | | |
| | 2558 | -0.19 | -0.19 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.16 | -0.16 | -0.16 | -0.69 | -0.69 | -0.69 | | | | | | | | | |
| | 694 | -0.33 | -0.34 | -0.33 | -0.27 | -0.26 | -0.25 | -0.29 | -0.29 | -0.29 | -0.27 | -0.28 | -0.43 | -0.43 | -0.43 | -0.73 | -0.73 | -0.73 | | | | | | | | | |
| | 837 | -0.26 | -0.26 | -0.25 | -0.20 | -0.19 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.36 | -0.36 | -0.36 | -0.65 | -0.65 | -0.65 | | | | | | | | | |
| | 981 | -0.22 | -0.22 | -0.21 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.32 | -0.32 | -0.32 | -0.68 | -0.68 | -0.68 | | | | | | | | | |
| | 1125 | -0.24 | -0.24 | -0.23 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.35 | -0.35 | -0.35 | -0.76 | -0.76 | -0.76 | | | | | | | | | |
| | 1269 | -0.18 | -0.18 | -0.18 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.28 | -0.28 | -0.28 | -0.79 | -0.79 | -0.79 | | | | | | | | | |
| 30° | 1412 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.84 | -0.84 | -0.84 | | | | | | | | | |
| | 1556 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.87 | -0.87 | -0.87 | | | | | | | | | |
| | 1700 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.91 | -0.91 | -0.91 | | | | | | | | | |
| | 1844 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.91 | -0.91 | -0.91 | | | | | | | | | |
| | 1987 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.91 | -0.91 | -0.91 | | | | | | | | | |
| | 2131 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.91 | -0.91 | -0.91 | | | | | | | | | |
| | 2275 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.91 | -0.91 | -0.91 | | | | | | | | | |
| | 2419 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.91 | -0.91 | -0.91 | | | | | | | | | |
| | 2558 | -0.17 | -0.17 | -0.17 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.24 | -0.24 | -0.24 | -0.91 | -0.91 | -0.91 | | | | | | | | | |
| 60° | 694 | -0.34 | -0.37 | -0.36 | -0.32 | -0.25 | -0.25 | -0.32 | -0.32 | -0.32 | -0.32 | -0.32 | -0.48 | -0.48 | -0.48 | -0.87 | -0.87 | -0.87 | | | | | | | | | |
| | 837 | -0.26 | -0.26 | -0.26 | -0.21 | -0.17 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.35 | -0.35 | -0.35 | -0.92 | -0.92 | -0.92 | | | | | | | | | |
| | 981 | -0.21 | -0.21 | -0.21 | -0.19 | -0.14 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.34 | -0.34 | -0.34 | -0.96 | -0.96 | -0.96 | | | | | | | | | |
| | 1125 | -0.21 | -0.21 | -0.21 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.97 | -0.97 | -0.97 | | | | | | | | | |
| | 1269 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.97 | -0.97 | -0.97 | | | | | | | | | |
| | 1412 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| | 1556 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| | 1700 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| | 1844 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| | 1987 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| 2131 | 2131 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| | 2275 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| | 2419 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |
| | 2558 | -0.19 | -0.19 | -0.19 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.34 | -0.34 | -0.34 | -0.98 | -0.98 | -0.98 | | | | | | | | | |

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (h) A = 2 rectangular wing, r/s = 0.2

| θ | x/r | $\delta_W, \alpha_B = 0^\circ$ | | | | | | | | | | $\alpha_B, \delta_W = 0^\circ$ | | | | | | |
|----------|-------|--------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------------------------------|-------|-------|-------|-------|-------|--|
| | | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | |
| 6° | 1.134 | -0.13 | -0.11 | -0.12 | -0.10 | -0.11 | -0.13 | - | -0.11 | -0.12 | - | -0.11 | -0.15 | -0.19 | -0.64 | -0.87 | -0.91 | |
| | 1.259 | -0.08 | -0.07 | -0.08 | -0.09 | -0.09 | -0.10 | - | -0.10 | -0.10 | - | -0.10 | -0.13 | -0.17 | -0.67 | -0.82 | -0.83 | |
| | 1.384 | -0.08 | -0.07 | -0.07 | -0.07 | -0.05 | -0.08 | - | -0.08 | -0.08 | - | -0.07 | -0.10 | -0.19 | -0.67 | -0.81 | -0.87 | |
| | 1.509 | -0.22 | -0.18 | -0.01 | -0.04 | -0.02 | -0.01 | - | -0.01 | -0.01 | - | -0.08 | -0.10 | -0.23 | -0.67 | -0.82 | -0.85 | |
| | 1.634 | -0.18 | -0.06 | -0.05 | -0.04 | -0.02 | -0.05 | - | -0.04 | -0.05 | - | -0.04 | -0.04 | -0.11 | -0.62 | -0.83 | -0.81 | |
| | 1.756 | -0.10 | -0.03 | -0.00 | -0.12 | -0.06 | -0.07 | - | -0.00 | -0.02 | - | -0.01 | -0.11 | -0.33 | -0.76 | -0.86 | -0.81 | |
| | 1.884 | -0.46 | -0.38 | -0.31 | -0.27 | -0.16 | -0.12 | - | -0.00 | -0.02 | - | -0.01 | -0.05 | -0.31 | -0.70 | -0.83 | -0.91 | |
| | 2.009 | -0.59 | -0.56 | -0.45 | -0.37 | -0.26 | -0.20 | - | -0.00 | -0.05 | - | -0.01 | -0.14 | -0.19 | -0.42 | -0.81 | -0.95 | |
| | 2.134 | -0.67 | -0.57 | -0.45 | -0.37 | -0.32 | -0.27 | - | -0.00 | -0.13 | - | -0.01 | -0.14 | -0.29 | -0.50 | -0.76 | -0.84 | |
| | 2.259 | -0.63 | -0.53 | -0.43 | -0.30 | -0.34 | -0.29 | - | -0.00 | -0.13 | - | -0.01 | -0.19 | -0.40 | -0.51 | -0.66 | -0.70 | |
| 15° | 2.384 | -0.51 | -0.30 | -0.24 | -0.18 | -0.24 | -0.21 | - | -0.04 | -0.04 | - | -0.00 | -0.07 | -0.26 | -0.34 | -0.63 | -0.68 | |
| | 2.509 | -0.27 | -0.06 | -0.00 | -0.05 | -0.11 | -0.09 | - | -0.00 | -0.13 | - | -0.00 | -0.06 | -0.05 | -0.05 | -0.48 | -0.68 | |
| | 1.134 | -0.14 | -0.14 | -0.15 | -0.12 | -0.16 | -0.15 | - | -0.14 | -0.16 | - | -0.13 | -0.18 | -0.44 | -0.76 | -0.80 | -0.87 | |
| | 1.259 | -0.11 | -0.10 | -0.11 | -0.13 | -0.12 | -0.13 | - | -0.12 | -0.12 | - | -0.10 | -0.10 | -0.43 | -0.69 | -0.74 | -0.83 | |
| | 1.384 | -0.10 | -0.09 | -0.07 | -0.09 | -0.10 | -0.09 | - | -0.09 | -0.10 | - | -0.07 | -0.09 | -0.40 | -0.64 | -0.72 | -0.82 | |
| | 1.509 | -0.16 | -0.07 | -0.06 | -0.02 | -0.07 | -0.08 | - | -0.07 | -0.08 | - | -0.05 | -0.16 | -0.43 | -0.68 | -0.77 | -0.81 | |
| | 1.634 | -0.41 | -0.32 | -0.27 | -0.01 | -0.01 | -0.07 | - | -0.00 | -0.00 | - | -0.05 | -0.05 | -0.43 | -0.61 | -0.83 | -0.79 | |
| | 1.756 | -0.04 | -0.06 | -0.05 | -0.19 | -0.11 | -0.08 | - | -0.00 | -0.00 | - | -0.00 | -0.00 | -0.41 | -0.67 | -0.86 | -0.82 | |
| | 1.884 | -0.46 | -0.40 | -0.37 | -0.36 | -0.81 | -0.17 | - | -0.04 | -0.00 | - | -0.00 | -0.07 | -0.41 | -0.68 | -0.86 | -0.92 | |
| | 2.009 | -0.60 | -0.56 | -0.52 | -0.42 | -0.31 | -0.25 | - | -0.01 | -0.09 | - | -0.01 | -0.07 | -0.49 | -0.53 | -0.78 | -0.94 | |
| 30° | 2.134 | -0.64 | -0.59 | -0.61 | -0.44 | -0.37 | -0.38 | - | -0.01 | -0.16 | - | -0.01 | -0.07 | -0.34 | -0.50 | -0.64 | -0.73 | |
| | 2.259 | -0.62 | -0.58 | -0.50 | -0.39 | -0.39 | -0.35 | - | -0.01 | -0.17 | - | -0.01 | -0.07 | -0.30 | -0.43 | -0.56 | -0.63 | |
| | 2.384 | -0.48 | -0.33 | -0.24 | -0.25 | -0.34 | -0.28 | - | -0.00 | -0.07 | - | -0.00 | -0.03 | -0.20 | -0.31 | -0.46 | -0.53 | |
| | 2.509 | -0.22 | -0.05 | -0.03 | -0.13 | -0.18 | -0.17 | - | -0.00 | -0.06 | - | -0.00 | -0.03 | -0.20 | -0.31 | -0.46 | -0.53 | |
| | 1.134 | -0.15 | -0.15 | -0.15 | -0.18 | -0.15 | -0.16 | - | -0.15 | -0.15 | - | -0.13 | -0.18 | -0.46 | -0.60 | -0.76 | -0.81 | |
| | 1.259 | -0.11 | -0.10 | -0.11 | -0.11 | -0.08 | -0.08 | - | -0.17 | -0.18 | - | -0.10 | -0.10 | -0.46 | -0.61 | -0.72 | -0.81 | |
| | 1.384 | -0.08 | -0.06 | -0.08 | -0.11 | -0.11 | -0.13 | - | -0.13 | -0.13 | - | -0.07 | -0.13 | -0.43 | -0.56 | -0.71 | -0.81 | |
| | 1.509 | -0.11 | -0.08 | -0.08 | -0.04 | -0.10 | -0.03 | - | -0.01 | -0.00 | - | -0.05 | -0.13 | -0.31 | -0.46 | -0.64 | -0.73 | |
| | 1.634 | -0.60 | -0.52 | -0.52 | -0.53 | -0.53 | -0.40 | - | -0.13 | -0.13 | - | -0.05 | -0.05 | -0.31 | -0.46 | -0.56 | -0.64 | |
| | 1.756 | -0.27 | -0.22 | -0.22 | -0.34 | -0.34 | -0.34 | - | -0.01 | -0.03 | - | -0.05 | -0.05 | -0.21 | -0.36 | -0.46 | -0.54 | |
| 60° | 1.884 | -0.60 | -0.56 | -0.52 | -0.53 | -0.49 | -0.40 | - | -0.13 | -0.19 | - | -0.09 | -0.09 | -0.28 | -0.46 | -0.57 | -0.65 | |
| | 2.009 | -0.76 | -0.62 | -0.64 | -0.59 | -0.49 | -0.40 | - | -0.18 | -0.19 | - | -0.10 | -0.10 | -0.31 | -0.48 | -0.58 | -0.66 | |
| | 2.134 | -0.76 | -0.65 | -0.81 | -0.58 | -0.53 | -0.47 | - | -0.31 | -0.34 | - | -0.11 | -0.11 | -0.28 | -0.48 | -0.58 | -0.66 | |
| | 2.259 | -0.72 | -0.61 | -0.46 | -0.48 | -0.58 | -0.48 | - | -0.31 | -0.19 | - | -0.11 | -0.11 | -0.28 | -0.48 | -0.58 | -0.66 | |
| | 2.384 | -0.63 | -0.24 | -0.04 | -0.19 | -0.87 | -0.47 | - | -0.19 | -0.09 | - | -0.00 | -0.06 | -0.22 | -0.31 | -0.49 | -0.56 | |
| | 2.509 | -0.27 | -0.04 | -0.06 | -0.16 | -0.18 | -0.22 | - | -0.00 | -0.06 | - | -0.00 | -0.03 | -0.22 | -0.31 | -0.49 | -0.56 | |
| | 1.134 | -0.19 | -0.19 | -0.17 | -0.14 | -0.19 | -0.18 | - | -0.19 | -0.19 | - | -0.13 | -0.14 | -0.34 | -0.51 | -0.69 | -0.78 | |
| | 1.259 | -0.11 | -0.10 | -0.12 | -0.10 | -0.12 | -0.12 | - | -0.15 | -0.11 | - | -0.10 | -0.10 | -0.26 | -0.44 | -0.66 | -0.73 | |
| | 1.384 | -0.10 | -0.11 | -0.14 | -0.14 | -0.13 | -0.13 | - | -0.13 | -0.13 | - | -0.10 | -0.10 | -0.27 | -0.47 | -0.63 | -0.68 | |
| | 1.509 | -0.06 | -0.26 | -0.08 | -0.08 | -0.11 | -0.10 | - | -0.10 | -0.10 | - | -0.07 | -0.10 | -0.21 | -0.47 | -0.66 | -0.78 | |
| Final | 1.634 | -0.23 | -0.17 | -0.05 | -0.59 | -0.33 | -0.33 | - | -0.04 | -0.18 | - | -0.04 | -0.18 | -0.38 | -0.53 | -0.81 | -0.94 | |
| | 1.756 | -0.13 | -0.11 | -0.12 | -0.96 | -0.75 | -0.78 | - | -0.38 | -0.38 | - | -0.38 | -0.38 | -0.46 | -0.63 | -0.88 | -1.00 | |
| | 1.884 | -0.10 | -0.06 | -0.04 | -0.94 | -0.84 | -0.78 | - | -0.44 | -0.44 | - | -0.44 | -0.44 | -0.50 | -0.69 | -0.89 | -0.99 | |
| | 2.009 | -0.02 | -0.27 | -0.04 | -0.04 | -0.76 | -0.83 | -0.78 | - | -0.30 | -0.17 | - | -0.14 | -0.19 | -0.46 | -0.57 | -0.88 | |
| | 2.134 | -0.96 | -0.71 | -0.66 | -0.48 | -0.74 | -0.71 | - | -0.30 | -0.17 | - | -0.14 | -0.14 | -0.53 | -0.67 | -0.99 | -1.00 | |
| | 2.259 | -0.82 | -0.42 | -0.32 | -0.38 | -0.38 | -0.37 | - | -0.16 | -0.16 | - | -0.14 | -0.17 | -0.48 | -0.68 | -0.95 | -1.00 | |
| | 2.384 | -0.45 | -0.28 | -0.26 | -0.20 | -0.22 | -0.22 | - | -0.06 | -0.04 | - | -0.04 | -0.01 | -0.39 | -0.51 | -0.78 | -0.86 | |
| | 2.509 | -0.39 | -0.16 | -0.15 | -0.15 | -0.20 | -0.15 | - | -0.04 | -0.03 | - | -0.01 | -0.01 | -0.39 | -0.51 | -0.78 | -0.86 | |

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (h) $A = 2$ rectangular wing, $r/s = 0.2$ - Concluded

| α | x/r | $\delta_w, \alpha_B = 0^\circ$ | | | | | | | | | | | | $a_B, \delta_w = 0^\circ$ | | | | | |
|----------|-------|--------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------------------|------|-----|-----|--|--|
| | | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | |
| 120° | 1.34 | -0.21 | -0.19 | -0.20 | -0.16 | -0.20 | -0.20 | -0.20 | -0.20 | -0.19 | -0.21 | -0.16 | -0.06 | 0.56 | 1.22 | | | | |
| | 1.59 | -0.21 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.07 | 0.45 | 1.27 | | | | |
| | 1.384 | -0.20 | -0.12 | -0.13 | -0.09 | -0.13 | -0.14 | -0.14 | -0.14 | -0.14 | -0.13 | -0.13 | -0.03 | 0.45 | 1.31 | | | | |
| | 1.634 | -0.17 | -0.15 | -0.10 | -0.13 | -0.13 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.14 | -0.01 | 0.45 | 1.31 | | | | |
| | 1.67 | -0.02 | -0.05 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | 0.45 | 1.31 | | | | |
| | 1.756 | -0.05 | -0.39 | -0.31 | -0.05 | -0.31 | -0.49 | -0.55 | -0.55 | -0.55 | -0.55 | -0.55 | -0.41 | 0.41 | 1.68 | | | | |
| | 1.884 | -1.09 | -1.00 | -1.00 | -0.78 | -0.70 | -0.68 | -0.68 | -0.68 | -0.68 | -0.68 | -0.68 | -0.68 | 1.28 | 1.65 | | | | |
| | 2.009 | -1.03 | -0.96 | -0.96 | -0.65 | -0.51 | -0.44 | -0.44 | -0.44 | -0.44 | -0.44 | -0.44 | -0.44 | 1.65 | 1.95 | | | | |
| | 2.134 | -0.68 | -0.75 | -0.65 | -0.50 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | 1.14 | 1.69 | | | | |
| | 2.259 | -0.89 | -0.66 | -0.50 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | 0.82 | 1.69 | | | | |
| 150° | 1.34 | -0.21 | -0.16 | -0.48 | -0.31 | -0.37 | -0.09 | -0.09 | -0.11 | -0.09 | -0.09 | -0.09 | -0.07 | 0.26 | 1.15 | | | | |
| | 1.59 | -0.16 | -0.16 | -0.11 | -0.11 | -0.11 | -0.11 | -0.11 | -0.11 | -0.11 | -0.11 | -0.11 | -0.00 | 0.30 | 0.90 | | | | |
| | 1.384 | -0.18 | -0.11 | -0.11 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.04 | 0.75 | 1.65 | | | | |
| | 1.509 | -0.93 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | -0.07 | 0.78 | 1.51 | | | | |
| | 1.634 | -1.64 | -1.39 | -0.11 | -0.18 | -0.13 | -0.18 | -0.18 | -0.18 | -0.18 | -0.18 | -0.18 | -0.07 | 0.65 | 1.60 | | | | |
| | 2.116 | -0.54 | -0.74 | -1.01 | -0.80 | -0.80 | -0.53 | -0.53 | -0.53 | -0.53 | -0.53 | -0.53 | -0.53 | 0.94 | 1.60 | | | | |
| | 1.756 | -2.99 | -2.78 | -1.79 | -1.13 | -1.38 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | 0.88 | 1.48 | | | | |
| | 1.884 | -0.26 | -1.16 | -1.94 | -1.88 | -1.88 | -1.87 | -1.87 | -1.87 | -1.87 | -1.87 | -1.87 | -1.87 | 0.47 | 0.98 | | | | |
| | 2.009 | -0.86 | -0.47 | -0.81 | -0.61 | -0.58 | -0.60 | -0.60 | -0.60 | -0.60 | -0.60 | -0.60 | -0.60 | 0.71 | 1.24 | | | | |
| | 2.134 | -0.89 | -0.49 | -0.13 | -0.39 | -0.45 | -0.45 | -0.45 | -0.45 | -0.45 | -0.45 | -0.45 | -0.45 | 0.79 | 1.30 | | | | |
| 165° | 1.34 | -0.03 | -0.10 | -0.08 | -0.01 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | 0.75 | 1.37 | | | | |
| | 1.59 | -0.48 | -0.13 | -0.10 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | 0.80 | 1.50 | | | | |
| | 1.384 | -0.17 | -0.17 | -0.15 | -0.15 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | 0.88 | 1.90 | | | | |
| | 1.509 | -0.34 | -0.12 | -0.11 | -0.06 | -0.09 | -0.12 | -0.12 | -0.12 | -0.12 | -0.12 | -0.12 | -0.12 | 0.94 | 1.65 | | | | |
| | 1.634 | -1.43 | -1.52 | -1.06 | -0.09 | -0.09 | -0.10 | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | 0.95 | 1.65 | | | | |
| | 2.116 | -2.76 | -1.84 | -2.82 | -1.39 | -1.39 | -0.68 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | 0.97 | 1.67 | | | | |
| | 1.756 | -0.64 | -0.06 | -2.57 | -1.96 | -1.18 | -0.79 | -0.79 | -0.79 | -0.79 | -0.79 | -0.79 | -0.79 | 0.98 | 1.67 | | | | |
| | 2.009 | -0.70 | -0.15 | -0.82 | -1.36 | -1.36 | -0.78 | -0.78 | -0.78 | -0.78 | -0.78 | -0.78 | -0.78 | 0.67 | 1.21 | | | | |
| | 2.134 | -0.74 | -0.61 | -0.39 | -0.66 | -0.78 | -0.69 | -0.69 | -0.69 | -0.69 | -0.69 | -0.69 | -0.69 | 0.71 | 1.41 | | | | |
| | 2.259 | -0.38 | -0.31 | -0.45 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | -0.48 | 0.48 | 1.51 | | | | |
| 174° | 1.34 | -0.13 | -0.10 | -0.15 | -0.31 | -0.31 | -0.35 | -0.38 | -0.38 | -0.19 | -0.04 | -0.17 | -0.17 | 0.37 | 0.61 | | | | |
| | 1.59 | -0.10 | -0.10 | -0.09 | -0.09 | -0.08 | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | 0.42 | 0.78 | | | | |
| | 1.384 | -0.78 | -0.09 | -0.09 | -0.09 | -0.09 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | -0.10 | 0.68 | 1.68 | | | | |
| | 1.509 | -1.69 | -1.56 | -0.63 | -0.01 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | -0.08 | 0.71 | 1.71 | | | | |
| | 1.634 | -2.66 | -2.62 | -2.58 | -1.36 | -0.84 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | 0.70 | 1.61 | | | | |
| | 1.756 | -3.41 | -2.71 | -1.63 | -2.49 | -1.91 | -1.36 | -0.35 | -0.35 | -0.35 | -0.35 | -0.35 | -0.35 | 0.61 | 1.27 | | | | |
| | 1.884 | -2.75 | -2.52 | -2.68 | -1.68 | -1.68 | -0.75 | -0.75 | -0.75 | -0.75 | -0.75 | -0.75 | -0.75 | 0.61 | 1.52 | | | | |
| | 2.009 | -1.74 | -2.46 | -2.14 | -1.61 | -1.49 | -0.95 | -0.95 | -0.95 | -0.95 | -0.95 | -0.95 | -0.95 | 0.67 | 1.27 | | | | |
| | 2.134 | -1.26 | -1.89 | -1.43 | -1.05 | -0.86 | -0.73 | -0.73 | -0.73 | -0.73 | -0.73 | -0.73 | -0.73 | 0.67 | 1.62 | | | | |
| | 2.259 | -0.49 | -0.36 | -0.57 | -0.72 | -0.49 | -0.45 | -0.45 | -0.45 | -0.45 | -0.45 | -0.45 | -0.45 | 0.67 | 1.63 | | | | |
| | 2.384 | -0.00 | -0.01 | -0.11 | -0.20 | -0.31 | -0.38 | -0.38 | -0.38 | -0.38 | -0.38 | -0.38 | -0.38 | 0.44 | 1.49 | | | | |
| | 2.509 | -0.01 | -0.04 | -0.04 | -0.04 | -0.04 | -0.04 | -0.04 | -0.04 | -0.04 | -0.04 | -0.04 | -0.04 | 0.49 | 1.49 | | | | |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL
(a) $A = 4$ triangular wing, $r/s = 0.2$

| α_B | y/s | δ_w | | | | | | | | | | | |
|------------|-------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | |
| 0° | Upper | .025 | -1.45 | -1.32 | -1.44 | -1.39 | -1.25 | -1.11 | -0.93 | -0.61 | -0.30 | -0.06 | .019 |
| | | .250 | -1.11 | -1.02 | -1.17 | -1.14 | -1.06 | -0.94 | -0.87 | -0.68 | -0.38 | -0.07 | .033 |
| | | .500 | -0.72 | -0.67 | -0.76 | -0.75 | -0.67 | -0.51 | -0.48 | -0.48 | -0.30 | -0.10 | .019 |
| | | .750 | -0.53 | -0.32 | -0.37 | -0.36 | -0.24 | -0.30 | -0.26 | -0.23 | -0.15 | -0.07 | .005 |
| | Lower | .025 | 1.798 | 1.512 | 1.244 | 9.47 | 5.87 | 5.16 | 3.81 | -1.75 | 10.2 | 0.52 | .019 |
| | | .250 | 1.529 | 1.325 | 1.120 | 9.16 | 7.05 | 5.38 | 3.77 | 2.31 | 13.8 | 0.76 | .033 |
| | | .500 | 1.027 | .910 | .795 | 6.67 | 5.23 | 4.01 | 2.81 | 1.62 | 8.93 | 0.46 | .019 |
| | | .750 | .517 | .463 | .408 | 3.44 | 2.70 | 2.05 | 1.34 | 0.72 | 0.37 | 0.37 | .005 |
| | Total | .025 | 1.943 | 1.644 | 1.388 | 10.86 | 8.12 | 6.27 | 4.14 | 2.36 | 13.2 | 0.58 | .000 |
| 3° | Upper | .025 | 1.640 | 1.427 | 1.237 | 1.030 | 8.11 | 6.32 | 4.64 | 2.99 | 1.76 | 8.83 | .000 |
| | | .250 | 1.099 | .977 | .871 | .742 | 5.90 | 4.72 | 3.32 | 2.10 | 1.83 | 0.56 | .000 |
| | | .500 | .550 | .495 | .445 | 3.80 | 2.94 | 2.35 | 1.60 | 0.95 | 0.52 | 0.44 | .000 |
| | | .750 | .335 | -0.35 | -0.39 | -0.36 | -0.30 | -0.34 | -0.31 | -0.26 | -0.20 | -0.15 | -0.06 |
| | Lower | .025 | 1.707 | 1.663 | 1.429 | 1.187 | 9.21 | 6.80 | 4.61 | 3.03 | 1.97 | 1.32 | 0.77 |
| | | .250 | 1.614 | 1.448 | 1.248 | 1.072 | 8.58 | 6.65 | 4.87 | 3.37 | 2.27 | 1.54 | 0.88 |
| | | .500 | 1.089 | .979 | .865 | .750 | 6.25 | 4.90 | 3.60 | 2.41 | 1.53 | 0.99 | 0.51 |
| | | .750 | .546 | .500 | .444 | 3.86 | 3.22 | 2.54 | 1.79 | 1.10 | 0.65 | 0.40 | 0.17 |
| | Total | .025 | 1.849 | 1.803 | 1.578 | 1.326 | 1.034 | 8.01 | 5.65 | 3.85 | 2.58 | 1.76 | 0.97 |
| 6° | Upper | .025 | 1.725 | 1.557 | 1.369 | 1.185 | 9.53 | 7.72 | 5.86 | 4.21 | 2.94 | 2.00 | 1.09 |
| | | .250 | 1.162 | 1.051 | .944 | .824 | 6.89 | 5.60 | 4.25 | 2.97 | 1.97 | 1.30 | 0.64 |
| | | .500 | .581 | .536 | .483 | .422 | 3.52 | 2.88 | 2.10 | 1.36 | 0.85 | 0.55 | 0.23 |
| | | .750 | .37 | .37 | .37 | .37 | .34 | .32 | .32 | .26 | .21 | .14 | |
| | Lower | .025 | 1.218 | 1.290 | 1.079 | 8.47 | 6.62 | 4.61 | 3.38 | 2.48 | 1.69 | | |
| | | .250 | 1.339 | 1.159 | 9.65 | 7.84 | 6.10 | 4.43 | 3.26 | 2.44 | 1.78 | | |
| | | .500 | .953 | .833 | .708 | 5.85 | 4.60 | 3.34 | 2.41 | 1.73 | 1.20 | | |
| | | .750 | .486 | .427 | 3.65 | 3.06 | 2.38 | 1.67 | 1.08 | 0.73 | 0.49 | | |
| | Total | .025 | 1.368 | 1.435 | 1.225 | 0.80 | 7.83 | 5.70 | 4.27 | 3.30 | 2.36 | | |
| 10° | Upper | .025 | 1.456 | 1.275 | 1.084 | 0.96 | 7.15 | 5.49 | 4.17 | 3.24 | 2.38 | | |
| | | .250 | 1.089 | .908 | .786 | 6.58 | 5.29 | 4.03 | 2.99 | 2.22 | 1.54 | | |
| | | .500 | .583 | .464 | 4.02 | 3.40 | 2.70 | 1.99 | 1.34 | 0.94 | 0.63 | | |
| | | .750 | .37 | .37 | .37 | .36 | .33 | .33 | .29 | .23 | .22 | | |
| | Lower | .025 | 1.675 | 1.190 | 1.008 | 0.839 | 6.74 | 5.01 | 3.72 | 3.13 | 2.37 | | |
| | | .250 | .973 | .868 | .753 | 6.30 | 5.14 | 3.87 | 3.02 | 2.43 | 1.79 | | |
| | | .500 | .497 | .451 | 3.91 | 3.29 | 2.78 | 2.03 | 1.55 | 1.13 | 0.79 | | |
| | | .750 | .621 | .707 | 8.23 | 8.85 | 7.25 | 6.09 | 5.03 | 4.30 | 3.40 | | |
| | Total | .025 | 1.785 | 1.295 | 1.127 | 0.957 | 7.84 | 6.14 | 4.75 | 4.03 | 3.25 | | |
| | | .250 | 1.047 | .937 | .831 | 7.07 | 5.85 | 4.58 | 3.43 | 2.98 | 2.31 | | |
| | | .500 | .531 | .483 | .429 | 3.65 | 3.05 | 2.36 | 1.84 | 1.36 | 1.01 | | |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE
BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
(a) $A = 4$ triangular wing, $r/s = 0.2$ - Continued

| a_B | y/s | δ_w | | | | | | | | | | |
|-------|-------|------------|-------|-------|-------|-------|-------|-------|-------|--------|--------|--------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° | |
| 0° | Upper | .025 | | | | | | | | | | |
| | | .250 | | | | | | | | | | |
| | | .500 | | | | | | | | | | |
| | | .750 | | | | | | | | | | |
| | Lower | .025 | | | | | | | | | | |
| | | .250 | | | | | | | | | | |
| | | .500 | | | | | | | | | | |
| | | .750 | | | | | | | | | | |
| | Total | .025 | | | | | | | | | | |
| | | .250 | | | | | | | | | | |
| | | .500 | | | | | | | | | | |
| | | .750 | | | | | | | | | | |
| 3° | Upper | .025 | .004 | .019 | .077 | .178 | .324 | .498 | .723 | 1.010 | 1.299 | 1.545 |
| | | .250 | .016 | .055 | .134 | .251 | .390 | .554 | .729 | .944 | 1.141 | 1.342 |
| | | .500 | .010 | .037 | .096 | .188 | .303 | .426 | .551 | .689 | .816 | .918 |
| | | .750 | .005 | .016 | .043 | .087 | .149 | .223 | .291 | .362 | .421 | .468 |
| | Lower | .025 | .037 | -.004 | -.039 | -.070 | -.082 | -.114 | -.131 | -.132 | -.121 | -.133 |
| | | .250 | .038 | -.006 | -.043 | -.064 | -.069 | -.095 | -.104 | -.109 | -.096 | -.105 |
| | | .500 | .017 | -.013 | -.033 | -.041 | -.041 | -.064 | -.084 | -.071 | -.063 | -.069 |
| | | .750 | .003 | -.009 | -.016 | -.018 | -.018 | -.031 | -.036 | -.034 | -.030 | -.033 |
| | Total | .025 | .033 | -.023 | -.116 | -.248 | -.406 | -.612 | -.854 | -.1142 | -.1420 | -.1678 |
| | | .250 | .022 | -.061 | -.177 | -.315 | -.459 | -.649 | -.833 | -.1053 | -.1237 | -.1447 |
| | | .500 | .007 | -.050 | -.129 | -.229 | -.344 | -.490 | -.635 | -.760 | -.879 | -.987 |
| | | .750 | -.002 | -.025 | -.059 | -.105 | -.167 | -.254 | -.327 | -.396 | -.451 | -.501 |
| 6° | Upper | .025 | -.057 | -.037 | -.012 | .053 | .177 | .334 | .544 | .783 | 1.045 | 1.375 |
| | | .250 | -.041 | -.010 | .037 | .130 | .257 | .399 | .569 | .751 | .950 | 1.176 |
| | | .500 | -.020 | .005 | .038 | .110 | | | .452 | .580 | .717 | .853 |
| | | .750 | -.006 | .006 | .021 | .057 | .108 | .178 | .251 | .317 | .384 | .448 |
| | Lower | .025 | .113 | .066 | .007 | -.045 | -.071 | -.096 | -.115 | -.127 | -.106 | -.126 |
| | | .250 | .119 | .073 | .010 | -.041 | -.060 | -.079 | -.094 | -.100 | -.082 | -.098 |
| | | .500 | .075 | .044 | .001 | -.031 | -.041 | -.052 | -.062 | -.065 | -.047 | -.029 |
| | | .750 | .030 | .018 | -.002 | -.016 | -.019 | -.025 | -.029 | -.031 | -.026 | -.029 |
| | Total | .025 | .170 | .103 | .019 | -.098 | -.248 | -.430 | -.659 | -.910 | -.1151 | -.1501 |
| | | .250 | .160 | .083 | -.027 | -.171 | -.317 | -.478 | -.663 | -.851 | -.1038 | -.1274 |
| | | .500 | .095 | .039 | -.037 | -.141 | -.254 | -.380 | -.514 | -.645 | -.764 | -.911 |
| | | .750 | .036 | .012 | -.003 | -.073 | -.127 | -.203 | -.380 | -.348 | -.410 | -.477 |
| 10° | Upper | .025 | -.101 | -.101 | -.080 | -.030 | .073 | .212 | .389 | | .818 | 1.064 |
| | | .250 | -.085 | -.078 | -.039 | .030 | .129 | .242 | .385 | | .719 | .908 |
| | | .500 | -.044 | -.035 | -.004 | .053 | .135 | .235 | .346 | | .569 | .688 |
| | | .750 | -.017 | -.014 | .003 | .032 | .073 | .129 | .199 | | .322 | .381 |
| | Lower | .025 | .160 | .092 | .033 | -.022 | -.081 | -.102 | -.117 | | .142 | -.136 |
| | | .250 | .179 | .115 | .047 | -.008 | -.061 | -.084 | -.097 | | .114 | -.109 |
| | | .500 | .132 | .082 | .032 | -.006 | -.043 | -.054 | -.062 | | .075 | -.072 |
| | | .750 | .056 | .032 | .010 | -.005 | -.020 | -.025 | -.030 | | .035 | -.034 |
| | Total | .025 | .261 | .193 | .113 | -.008 | -.154 | -.314 | -.506 | | .960 | -.1200 |
| | | .250 | .264 | .193 | .086 | -.038 | -.195 | -.326 | -.482 | | .833 | -.1011 |
| | | .500 | .176 | .117 | .036 | -.059 | -.178 | -.289 | -.408 | | .644 | -.760 |
| | | .750 | .073 | .046 | .007 | -.037 | -.093 | -.154 | -.229 | | .357 | -.415 |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (a) $A = 4$ triangular wing, $r/s = 0.2$ - Continued

| | | SW | | | | | | | | | | |
|------------|-------|------|-----|-----|-------|-------|-------|-------|-------|-------|-------|------|
| α_8 | y/s | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° |
| 15° | Upper | .025 | | | -149 | -148 | -140 | -147 | -143 | -134 | -141 | -127 |
| | | .250 | | | -117 | -116 | -108 | -116 | -110 | -102 | -111 | -101 |
| | | .500 | | | -076 | -075 | -069 | -074 | -069 | -064 | -070 | -063 |
| | | .750 | | | -036 | -035 | -033 | -035 | -033 | -030 | -033 | -029 |
| | Lower | .025 | | | 495 | 1.753 | 1.474 | .733 | .667 | .580 | .502 | .391 |
| | | .250 | | | 1.597 | 1.346 | 1.142 | .983 | .763 | .611 | .509 | .407 |
| | | .500 | | | 0.994 | .960 | .829 | .730 | .573 | .464 | .391 | .315 |
| | | .750 | | | .565 | .506 | .439 | .389 | .318 | .252 | .211 | .168 |
| | Total | .025 | | | .644 | 1.901 | .614 | .880 | .810 | .714 | .643 | .518 |
| | | .250 | | | 1.714 | 1.462 | 1.250 | 1.099 | .873 | .713 | .620 | .508 |
| | | .500 | | | 1.170 | 1.035 | .898 | .804 | .642 | .526 | .461 | .378 |
| | | .750 | | | .601 | .541 | .472 | .424 | .345 | .262 | .244 | .197 |
| 20° | Upper | .025 | | | -126 | -141 | -157 | -149 | -157 | -155 | -156 | -141 |
| | | .250 | | | -096 | -105 | -119 | -112 | -117 | -119 | -121 | -107 |
| | | .500 | | | -061 | -067 | -076 | -074 | -076 | -084 | -080 | -065 |
| | | .750 | | | -028 | -031 | -036 | -035 | -036 | -036 | -039 | -029 |
| | Lower | .025 | | | .704 | .716 | .762 | .960 | .888 | .798 | .770 | .565 |
| | | .250 | | | 1.944 | 1.680 | 1.460 | 1.211 | .990 | .806 | .693 | .569 |
| | | .500 | | | 1.314 | 1.179 | 1.042 | .886 | .733 | .605 | .527 | .440 |
| | | .750 | | | .653 | .605 | .537 | .462 | .388 | .327 | .304 | .240 |
| | Total | .025 | | | .830 | .857 | .919 | 1.109 | 1.039 | .953 | .926 | .706 |
| | | .250 | | | 2.040 | 1.785 | 1.559 | 1.323 | 1.107 | .925 | .814 | .676 |
| | | .500 | | | 1.375 | 1.246 | 1.118 | .960 | .809 | .689 | .607 | .505 |
| | | .750 | | | .681 | .636 | .573 | .497 | .424 | .363 | .343 | .269 |
| 25° | Upper | .025 | | | -142 | -148 | -168 | -168 | -155 | -139 | -149 | |
| | | .250 | | | -110 | -114 | -134 | -134 | -122 | -113 | -112 | |
| | | .500 | | | -071 | -073 | -088 | -088 | -078 | -074 | -074 | |
| | | .750 | | | -034 | -034 | -041 | -041 | -036 | -034 | -029 | |
| | Lower | .025 | | | 1.240 | 1.466 | 1.305 | 1.257 | 1.120 | 1.020 | 1.039 | |
| | | .250 | | | 1.849 | 1.584 | 1.325 | 1.125 | .976 | .830 | .730 | |
| | | .500 | | | 1.323 | 1.411 | .967 | .831 | .728 | .629 | .540 | |
| | | .750 | | | .715 | .621 | .531 | .463 | .409 | .334 | .264 | |
| | Total | .025 | | | 1.182 | 1.614 | 1.473 | 1.412 | 1.259 | 1.125 | 1.089 | |
| | | .250 | | | 1.959 | 1.698 | 1.459 | 1.247 | 1.089 | 9.42 | 9.42 | |
| | | .500 | | | 1.394 | 1.214 | 1.055 | .909 | .802 | .697 | .563 | |
| | | .750 | | | .749 | .655 | .578 | .499 | .443 | .363 | .263 | |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (a) $A = \frac{1}{4}$ triangular wing, $r/s = 0.2$ - Concluded

| α_B | y/s | | δ_w | | | | | | | | | |
|------------|-------|------|------------|-------|-------|-------|-------|-------|-------|-------|-------|--------|
| | | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 15° | Upper | .025 | -129 | -122 | .000 | -.026 | | .228 | .395 | .609 | .846 | 1.082 |
| | | .250 | -.098 | -.087 | .000 | .007 | | .203 | .339 | .496 | .668 | .846 |
| | | .500 | -.053 | -.043 | .000 | .027 | | .191 | .296 | .412 | .517 | .637 |
| | | .750 | -.022 | -.017 | .000 | .018 | | .101 | .168 | .236 | .295 | .352 |
| | Lower | .025 | .295 | .205 | .000 | .031 | | -.061 | -.090 | -.060 | -.122 | -.107 |
| | | .250 | .330 | .246 | .000 | .055 | | -.063 | -.078 | -.100 | -.103 | -.089 |
| | | .500 | .255 | .189 | .000 | .038 | | -.034 | -.050 | -.062 | -.065 | -.059 |
| | | .750 | .129 | .090 | .000 | .015 | | -.017 | -.023 | -.029 | -.033 | -.027 |
| | Total | .025 | .424 | .327 | .000 | .057 | | -.289 | -.485 | -.669 | -.968 | -1.189 |
| | | .250 | .428 | .333 | .000 | .048 | | -.266 | -.417 | -.596 | -.771 | .935 |
| | | .500 | .308 | .232 | .000 | .011 | | -.225 | -.346 | -.474 | -.582 | -.696 |
| | | .750 | .151 | .107 | .000 | -.003 | | -.118 | -.191 | -.265 | -.328 | -.379 |
| 20° | Upper | .025 | -150 | -142 | -.098 | | .097 | .284 | .455 | .662 | .911 | 1.152 |
| | | .250 | -112 | -101 | -.063 | | .088 | .215 | .356 | .520 | .712 | .914 |
| | | .500 | -.066 | -.054 | -.027 | | .080 | .181 | .284 | .393 | .509 | .633 |
| | | .750 | -.030 | -.022 | -.009 | | .041 | .092 | .159 | .227 | .290 | .352 |
| | Lower | .025 | .437 | .350 | .230 | | .050 | -.007 | -.061 | -.088 | .157 | .195 |
| | | .250 | .474 | .383 | .265 | | .052 | -.011 | -.064 | -.086 | .138 | .145 |
| | | .500 | .371 | .298 | .203 | | .040 | -.005 | -.042 | -.054 | -.068 | .041 |
| | | .750 | .201 | .157 | .101 | | .019 | -.001 | -.019 | -.025 | .043 | -.034 |
| | Total | .025 | .587 | .492 | .328 | | -.047 | -.291 | -.516 | -.750 | -.754 | -.957 |
| | | .250 | .484 | .328 | | | -.036 | -.226 | -.420 | -.606 | -.574 | -.769 |
| | | .500 | .437 | .352 | .230 | | -.040 | -.186 | -.326 | -.447 | -.577 | -.592 |
| | | .750 | .231 | .179 | .110 | | -.022 | -.093 | -.178 | -.252 | -.347 | -.386 |
| 25° | Upper | .025 | -132 | -113 | -.067 | -.006 | .163 | .344 | .631 | .736 | .846 | 1.112 |
| | | .250 | -.096 | -.046 | -.001 | .108 | .230 | .523 | .566 | .767 | 1.001 | |
| | | .500 | -.055 | -.046 | -.020 | -.006 | .080 | .173 | .353 | .406 | .531 | .670 |
| | | .750 | -.022 | -.017 | -.004 | .008 | .043 | .088 | .201 | .226 | .291 | .357 |
| | Lower | .025 | .651 | .535 | .390 | .260 | .236 | .188 | .147 | .106 | .134 | .167 |
| | | .250 | .678 | .563 | .426 | .275 | .157 | .055 | .041 | .072 | .102 | .123 |
| | | .500 | .513 | .437 | .331 | .212 | .117 | .042 | .033 | .049 | .067 | .082 |
| | | .750 | .281 | .235 | .174 | .106 | .060 | .021 | .013 | .024 | .033 | .041 |
| | Total | .025 | .783 | .648 | .457 | .266 | .073 | -.156 | -.484 | -.630 | -.712 | -.945 |
| | | .250 | .774 | .647 | .472 | .276 | .049 | -.175 | -.482 | -.494 | -.565 | -.878 |
| | | .500 | .568 | .483 | .351 | .206 | .037 | -.131 | -.320 | -.357 | -.464 | -.588 |
| | | .750 | .303 | .252 | .178 | .098 | .017 | -.067 | -.188 | -.202 | -.258 | -.316 |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$

| α_s | y/s | δ_w | | | | | | | | | | | |
|------------|-------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | |
| 0° | Upper | .025 | -1.30 | -1.23 | -1.31 | -1.15 | -1.17 | -1.04 | -0.88 | -0.63 | -0.28 | -0.09 | .017 |
| | | .050 | -0.97 | -0.94 | -1.05 | -0.99 | -1.02 | -0.87 | -0.83 | -0.63 | -0.35 | -0.16 | .011 |
| | | .075 | -0.64 | -0.65 | -0.78 | -0.67 | -0.69 | -0.56 | -0.61 | -0.50 | -0.28 | -0.10 | .017 |
| | | .100 | -0.29 | -0.30 | -0.35 | -0.34 | -0.35 | -0.34 | -0.31 | -0.25 | -0.14 | -0.06 | .010 |
| | | .125 | -0.13 | -0.14 | -0.17 | -0.17 | -0.18 | -0.17 | -0.15 | -0.13 | -0.07 | -0.03 | .005 |
| | Lower | .025 | 1.657 | 1.410 | 1.086 | 8.34 | 5.85 | 3.95 | 2.50 | 1.09 | 0.60 | 0.35 | .017 |
| | | .050 | 1.255 | 1.078 | .870 | .670 | .504 | .367 | .239 | .125 | .076 | .040 | .011 |
| | | .075 | .799 | .714 | .587 | .476 | .375 | .276 | .192 | .106 | .069 | .041 | .017 |
| | | .100 | .413 | .366 | .313 | .268 | .218 | .167 | .123 | .073 | .050 | .029 | .010 |
| | | .125 | .211 | .188 | .162 | .139 | .118 | .093 | .070 | .046 | .031 | .017 | .005 |
| 3° | Total | .025 | 1.787 | 1.533 | 1.217 | 9.49 | 7.02 | 4.99 | 3.32 | 1.72 | 0.88 | 0.44 | .000 |
| | | .050 | 1.352 | 1.172 | .975 | .769 | .606 | .454 | .322 | .188 | .111 | .055 | .000 |
| | | .075 | .863 | .779 | .659 | .543 | .444 | .342 | .253 | .156 | .097 | .051 | .000 |
| | | .100 | .442 | .396 | .348 | .302 | .253 | .201 | .154 | .098 | .064 | .035 | .000 |
| | | .125 | .224 | .200 | .179 | .156 | .136 | .110 | .085 | .059 | .038 | .020 | .000 |
| | Upper | .025 | -1.15 | -1.09 | -0.95 | -1.18 | -1.07 | -1.18 | -0.81 | -0.49 | -0.44 | -0.30 | -0.19 |
| | | .050 | -0.92 | -0.90 | -0.83 | -1.02 | -0.98 | -0.99 | -0.80 | -0.59 | -0.52 | -0.37 | -0.22 |
| | | .075 | -0.60 | -0.59 | -0.53 | -0.68 | -0.64 | -0.64 | -0.53 | -0.40 | -0.36 | -0.23 | -0.09 |
| | | .100 | -0.28 | -0.28 | -0.26 | -0.34 | -0.32 | -0.31 | -0.27 | -0.20 | -0.17 | -0.11 | -0.03 |
| | | .125 | -0.13 | -0.13 | -0.12 | -0.17 | -0.15 | -0.14 | -0.10 | -0.09 | -0.05 | -0.02 | -0.02 |
| 6° | Lower | .025 | 1.611 | 1.597 | 1.396 | 1.107 | .809 | .561 | .362 | .226 | .142 | .094 | .054 |
| | | .050 | 1.762 | 1.232 | .973 | .811 | .640 | .481 | .320 | .218 | .139 | .091 | .052 |
| | | .075 | .833 | .755 | .637 | .551 | .440 | .352 | .247 | .167 | .109 | .075 | .045 |
| | | .100 | .442 | .403 | .353 | .297 | .246 | .197 | .147 | .105 | .074 | .054 | .034 |
| | | .125 | .227 | .209 | .185 | .161 | .134 | .108 | .084 | .062 | .045 | .033 | .019 |
| | Total | .025 | 1.726 | 1.706 | 1.491 | 1.225 | 9.16 | 6.79 | 4.43 | 2.75 | 1.86 | 1.24 | .073 |
| | | .050 | 1.854 | 1.322 | 1.056 | .913 | .738 | .580 | .410 | .277 | .191 | .128 | .074 |
| | | .075 | .893 | .814 | .690 | .619 | .504 | .415 | .300 | .207 | .145 | .098 | .054 |
| | | .100 | .470 | .431 | .378 | .331 | .278 | .228 | .174 | .126 | .091 | .065 | .037 |
| | | .125 | .240 | .222 | .197 | .178 | .151 | .123 | .098 | .072 | .054 | .038 | .021 |
| 10° | Upper | .025 | -1.29 | -1.19 | -1.09 | -1.19 | -1.13 | -1.00 | -0.82 | -0.81 | -0.81 | -0.72 | -0.73 |
| | | .050 | -0.92 | -0.98 | -0.94 | -1.06 | -1.05 | -0.98 | -0.86 | -0.86 | -0.86 | -0.84 | -0.84 |
| | | .075 | -0.54 | -0.64 | -0.60 | -0.71 | -0.69 | -0.65 | -0.57 | -0.57 | -0.56 | -0.49 | -0.49 |
| | | .100 | -0.29 | -0.30 | -0.29 | -0.34 | -0.34 | -0.32 | -0.29 | -0.29 | -0.29 | -0.21 | -0.21 |
| | | .125 | -0.14 | -0.15 | -0.15 | -0.17 | -0.17 | -0.16 | -0.15 | -0.15 | -0.15 | -0.10 | -0.10 |
| | Lower | .025 | 1.366 | 1.202 | 1.065 | .902 | .668 | .497 | .335 | .229 | .169 | .109 | .096 |
| | | .050 | 1.605 | 1.352 | .895 | .721 | .559 | .421 | .321 | .215 | .151 | .078 | .078 |
| | | .075 | .872 | .700 | .595 | .493 | .393 | .305 | .215 | .151 | .097 | .055 | .033 |
| | | .100 | .443 | .390 | .334 | .279 | .224 | .180 | .132 | .076 | .057 | .033 | .021 |
| | | .125 | .257 | .203 | .177 | .151 | .124 | .101 | .076 | .057 | .037 | .023 | .013 |
| Total | Upper | .025 | 1.495 | 1.321 | 1.174 | 1.021 | .781 | .597 | .417 | .310 | .181 | .169 | .141 |
| | | .050 | 1.704 | 1.450 | .989 | .827 | .604 | .519 | .377 | .285 | .187 | .127 | .106 |
| | | .075 | .936 | .764 | .655 | .565 | .462 | .370 | .272 | .209 | .161 | .126 | .076 |
| | | .100 | .472 | .420 | .363 | .313 | .269 | .212 | .161 | .126 | .072 | .043 | .023 |
| | | .125 | .271 | .218 | .192 | .160 | .141 | .117 | .091 | .072 | .043 | .023 | .013 |
| | Lower | .025 | -1.09 | -1.29 | -1.26 | -1.23 | -1.05 | -1.13 | -1.03 | -1.06 | -1.14 | -1.05 | -1.05 |
| | | .050 | -0.87 | -1.06 | -1.02 | -1.01 | -0.94 | -1.00 | -b.92 | -b.95 | -b.92 | -b.95 | -b.95 |
| | | .075 | -0.54 | -0.69 | -0.67 | -0.67 | -0.59 | -0.65 | -b.59 | -b.59 | -b.59 | -b.62 | -b.62 |
| | | .100 | -0.24 | -0.31 | -0.32 | -0.32 | -0.29 | -0.32 | -b.29 | -b.29 | -b.29 | -b.29 | -b.29 |
| | | .125 | -0.11 | -0.15 | -0.16 | -0.15 | -0.15 | -0.16 | -b.15 | -b.15 | -b.14 | -b.14 | -b.14 |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$ - Continued

| a_B | y/s | δ_w | | | | | | | | | | |
|-------|-------|------------|-------|-------|-------|-------|-------|-------|-------|---------|---------|-------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° | |
| 0° | Upper | .025 | | | | | | | | | | |
| | | .250 | | | | | | | | | | |
| | | .500 | | | | | | | | | | |
| | | .750 | | | | | | | | | | |
| | | .875 | | | | | | | | | | |
| | Lower | .025 | | | | | | | | | | |
| | | .250 | | | | | | | | | | |
| | | .500 | | | | | | | | | | |
| | | .750 | | | | | | | | | | |
| | | .875 | | | | | | | | | | |
| | Total | .025 | | | | | | | | | | |
| | | .250 | | | | | | | | | | |
| | | .500 | | | | | | | | | | |
| | | .750 | | | | | | | | | | |
| | | .875 | | | | | | | | | | |
| 45° | Upper | .025 | .005 | .007 | .060 | .131 | .266 | .434 | .653 | .905 | 1.191 | 1.496 |
| | | .050 | .001 | .018 | .076 | .148 | .256 | .386 | .537 | .719 | .897 | 1.142 |
| | | .100 | .010 | .030 | .075 | .128 | .207 | .396 | .598 | .813 | .620 | .744 |
| | | .150 | .007 | .024 | .053 | .089 | .131 | .181 | .233 | .291 | .331 | .372 |
| | | .200 | .004 | .015 | .033 | .054 | .077 | .100 | .127 | .152 | .171 | .191 |
| | Lower | .025 | .023 | -.005 | -.044 | -.074 | -.084 | -.100 | -.111 | -.126 | -.125 | .109 |
| | | .050 | .019 | -.006 | -.041 | -.072 | -.084 | -.095 | -.102 | -.101 | -.101 | .087 |
| | | .100 | .023 | -.008 | -.032 | -.052 | -.056 | -.063 | -.067 | -.063 | -.065 | .053 |
| | | .150 | .014 | -.001 | -.017 | -.027 | -.029 | -.032 | -.034 | -.030 | -.032 | .024 |
| | | .200 | .007 | -.001 | -.008 | -.014 | -.014 | -.016 | -.017 | -.014 | -.015 | .011 |
| | Total | .025 | .018 | -.012 | -.104 | -.205 | -.350 | -.534 | -.764 | -.1.031 | -.1.316 | 1.605 |
| | | .050 | .018 | -.024 | -.117 | -.220 | -.340 | -.481 | -.639 | -.880 | -.998 | 1.229 |
| | | .100 | .013 | -.032 | -.107 | -.180 | -.263 | -.359 | -.465 | -.576 | -.685 | .797 |
| | | .150 | .007 | -.025 | -.070 | -.116 | -.160 | -.213 | -.267 | -.321 | -.363 | .396 |
| | | .200 | .003 | -.016 | -.041 | -.068 | -.091 | -.116 | -.144 | -.166 | -.186 | .202 |
| 60° | Upper | .025 | -.055 | -.044 | -.003 | .052 | .147 | .297 | .489 | .686 | .972 | 1.281 |
| | | .050 | -.053 | -.033 | .010 | .072 | .158 | .269 | .408 | .562 | .779 | .922 |
| | | .100 | -.037 | -.017 | .022 | .073 | .138 | .216 | .310 | .411 | .522 | .638 |
| | | .150 | -.014 | -.001 | .024 | .059 | .096 | .139 | .188 | .243 | .263 | .345 |
| | | .200 | -.006 | -.000 | .015 | .038 | .059 | .080 | .105 | .130 | .160 | .176 |
| | Lower | .025 | .063 | .023 | -.015 | -.055 | -.072 | -.087 | -.087 | -.106 | -.115 | -.118 |
| | | .050 | .057 | .027 | -.007 | -.048 | -.068 | -.085 | -.082 | -.096 | -.099 | -.094 |
| | | .100 | .057 | .028 | -.003 | -.037 | -.048 | -.058 | -.053 | -.062 | -.064 | -.059 |
| | | .150 | .036 | .019 | -.001 | -.019 | -.025 | -.029 | -.029 | -.031 | -.032 | -.029 |
| | | .200 | .021 | .010 | -.001 | -.010 | -.013 | -.015 | -.013 | -.016 | -.016 | -.013 |
| | Total | .025 | .118 | .067 | -.012 | -.107 | -.219 | -.384 | -.576 | -.792 | -.1.087 | 1.399 |
| | | .050 | .110 | .060 | -.017 | -.120 | -.226 | -.354 | -.490 | -.658 | -.878 | 1.016 |
| | | .100 | .094 | .045 | -.025 | -.110 | -.186 | -.274 | -.363 | -.473 | -.586 | .697 |
| | | .150 | .050 | .020 | -.025 | -.078 | -.121 | -.168 | -.214 | -.274 | -.295 | .374 |
| | | .200 | .027 | .010 | -.016 | -.048 | -.072 | -.095 | -.118 | -.146 | -.176 | .189 |
| 10° | Upper | .025 | -.082 | -.040 | -.038 | .015 | .097 | .220 | | | | |
| | | .050 | -.075 | -.037 | -.032 | .010 | .087 | .183 | | | | |
| | | .100 | -.043 | -.012 | -.006 | .030 | .082 | .142 | | | | |
| | | .150 | -.019 | -.004 | -.006 | .034 | .067 | .103 | | | | |
| | | .200 | -.010 | -.002 | -.004 | .024 | .044 | .064 | | | | |
| | Lower | .025 | .122 | .066 | .014 | -.027 | -.081 | -.073 | | | | |
| | | .050 | .113 | .073 | .025 | -.023 | -.058 | -.074 | | | | |
| | | .100 | .098 | .065 | .025 | -.022 | -.046 | -.055 | | | | |
| | | .150 | .064 | .045 | .019 | -.009 | -.023 | -.027 | | | | |
| | | .200 | .039 | .027 | .011 | -.005 | -.011 | -.014 | | | | |
| | Total | .025 | .204 | .108 | .052 | -.042 | -.158 | -.293 | | | | |
| | | .050 | .186 | .110 | .057 | -.033 | -.145 | -.257 | | | | |
| | | .100 | .141 | .077 | .031 | -.052 | -.128 | -.197 | | | | |
| | | .150 | .083 | .049 | .013 | -.043 | -.090 | -.130 | | | | |
| | | .200 | .049 | .029 | .007 | -.029 | -.055 | -.078 | | | | |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (b) A = 2 triangular wing, r/s = 0.2 - Continued

| a_B | y/s | δ_w | | | | | | | | | | | | | | | | | |
|-------|-------|------------|-------|-------|-------|-------|------|------|------|------|------|-------|-------|-------|------|------|------|------|------|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | | | | | | | |
| 15° | Upper | .025 | - | 1.65 | - | 1.50 | - | 1.71 | - | 1.65 | - | 1.53 | - | 1.39 | - | 1.29 | - | .068 | |
| | | .250 | - | 1.28 | - | 1.20 | - | 1.35 | - | 1.32 | - | 1.26 | - | 1.15 | - | 1.07 | - | .059 | |
| | | .500 | - | 0.80 | - | 0.75 | - | 0.89 | - | 0.85 | - | 0.80 | - | 0.72 | - | 0.65 | - | .035 | |
| | | .750 | - | 0.38 | - | 0.37 | - | 0.44 | - | 0.42 | - | 0.39 | - | 0.35 | - | 0.30 | - | .019 | |
| | | .875 | - | 0.19 | - | 0.18 | - | 0.22 | - | 0.21 | - | 0.20 | - | 0.17 | - | 0.14 | - | .009 | |
| | | Lower | .025 | 1.127 | .842 | .938 | .731 | 5.69 | 4.56 | 4.09 | 3.17 | 1.508 | 1.228 | .890 | .716 | .551 | .423 | 3.41 | 2.62 |
| | | .250 | 1.500 | .901 | .752 | .835 | .569 | .596 | .309 | .251 | .195 | .474 | .404 | .149 | .285 | .227 | .183 | .153 | .123 |
| | | .500 | .875 | .245 | .214 | .185 | .155 | .126 | .103 | .087 | .072 | .264 | .232 | .007 | .176 | .146 | .120 | .101 | .081 |
| | | Total | .025 | 1.292 | .992 | 1.109 | .896 | .722 | .595 | .538 | .385 | 1.636 | 1.348 | .1625 | .850 | .677 | .538 | .448 | .321 |
| | | .250 | .500 | .981 | .827 | .784 | .594 | .476 | .381 | .316 | .230 | .512 | .441 | .393 | .328 | .266 | .218 | .182 | .142 |
| | | .750 | .875 | .264 | .232 | .207 | .176 | .146 | .120 | .101 | .081 | .016 | .016 | .016 | .016 | .015 | .016 | .015 | .015 |
| 20° | Upper | .025 | - | 1.33 | - | 1.31 | - | 1.26 | - | 1.20 | - | 1.10 | - | 1.20 | - | 1.09 | - | .093 | |
| | | .250 | - | 1.03 | - | 1.03 | - | 1.01 | - | 0.98 | - | 0.92 | - | 1.00 | - | 0.93 | - | .060 | |
| | | .500 | - | 0.68 | - | 0.68 | - | 0.66 | - | 0.63 | - | 0.59 | - | 0.65 | - | 0.60 | - | .030 | |
| | | .750 | - | 0.33 | - | 0.33 | - | 0.32 | - | 0.31 | - | 0.29 | - | 0.33 | - | 0.31 | - | .015 | |
| | | .875 | - | 0.16 | - | 0.16 | - | 0.16 | - | 0.15 | - | 0.15 | - | 0.16 | - | 0.16 | - | .015 | |
| | | Lower | .025 | .828 | .864 | .822 | .704 | .647 | .619 | .530 | .419 | 1.683 | 1.301 | .951 | .750 | .600 | .500 | .429 | .304 |
| | | .250 | .500 | .965 | .811 | .667 | .533 | .429 | .360 | .298 | .208 | .503 | .430 | .360 | .294 | .243 | .208 | .178 | .101 |
| | | .750 | .875 | .258 | .226 | .190 | .160 | .136 | .116 | .101 | .081 | .274 | .242 | .206 | .175 | .151 | .132 | .116 | .015 |
| | | Total | .025 | .961 | .995 | .948 | .824 | .757 | .739 | .639 | .518 | 1.786 | 1.404 | 1.052 | .848 | .692 | .600 | .518 | .364 |
| | | .250 | .500 | 1.033 | .879 | .733 | .596 | .488 | .425 | .364 | .328 | .536 | .463 | .392 | .325 | .272 | .241 | .208 | .166 |
| | | .750 | .875 | .274 | .242 | .206 | .175 | .151 | .132 | .116 | .081 | .016 | .016 | .016 | .014 | .013 | .012 | .015 | .015 |
| 25° | Upper | .025 | - | 1.22 | - | 1.34 | - | 1.30 | - | 1.18 | - | 1.04 | - | 1.08 | - | .094 | - | .093 | |
| | | .250 | - | 0.94 | - | 1.04 | - | 1.01 | - | 0.95 | - | 0.86 | - | 0.93 | - | .061 | - | .059 | |
| | | .500 | - | 0.61 | - | 0.68 | - | 0.66 | - | 0.61 | - | 0.55 | - | 0.60 | - | .029 | - | .029 | |
| | | .750 | - | 0.29 | - | 0.33 | - | 0.32 | - | 0.29 | - | 0.27 | - | 0.27 | - | .014 | - | .015 | |
| | | .875 | - | 0.14 | - | 0.16 | - | 0.16 | - | 0.14 | - | 0.13 | - | 0.13 | - | .013 | - | .015 | |
| | | Lower | .025 | 1.255 | 1.191 | .983 | .878 | .893 | .765 | .599 | .478 | 1.556 | 1.278 | 1.023 | .848 | .724 | .599 | .478 | .332 |
| | | .250 | .500 | 1.019 | .879 | .720 | .503 | .416 | .327 | .284 | .203 | .510 | .457 | .386 | .327 | .284 | .241 | .184 | .131 |
| | | .750 | .875 | .232 | .212 | .184 | .165 | .151 | .132 | .116 | .101 | .246 | .228 | .200 | .179 | .165 | .146 | .131 | .081 |
| | | Total | .025 | 1.377 | 1.325 | 1.113 | .996 | .997 | .873 | .750 | .650 | 1.650 | 1.382 | 1.124 | .943 | .810 | .698 | .571 | .491 |
| | | .250 | .500 | 1.080 | .947 | .786 | .664 | .571 | .491 | .439 | .356 | .539 | .490 | .418 | .356 | .311 | .270 | .210 | .146 |
| | | .750 | .875 | .246 | .228 | .200 | .179 | .165 | .146 | .131 | .101 | .084 | .076 | .066 | .056 | .046 | .036 | .026 | .016 |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE
BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
(b) $A = 2$ triangular wing, $r/s = 0.2$ - Concluded

| α_B | y_s | δ_w | | | | | | | | | | |
|------------|-------|------------|------|------|------|-------|------|-------|-------|------|------|-------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° | |
| 15° | Upper | .025 | .093 | .077 | .058 | .007 | .104 | .174 | .348 | .484 | .672 | .924 |
| | | .250 | .081 | .073 | .058 | .015 | .060 | .150 | .257 | .391 | .510 | .681 |
| | | .500 | .050 | .044 | .033 | .004 | .054 | .105 | .169 | .251 | .333 | .432 |
| | | .750 | .026 | .021 | .014 | .014 | .044 | .074 | .107 | .148 | .187 | .236 |
| | Lower | .875 | .013 | .011 | .007 | .010 | .029 | .046 | .064 | .085 | .105 | .129 |
| | | .025 | .226 | .155 | .087 | .022 | .015 | .040 | .038 | .079 | .096 | .115 |
| | | .250 | .203 | .149 | .091 | .027 | .015 | .046 | .057 | .084 | .094 | .097 |
| | | .500 | .162 | .120 | .075 | .021 | .018 | .040 | .042 | .059 | .064 | .066 |
| | Total | .750 | .100 | .079 | .052 | .017 | .006 | .019 | .021 | .029 | .032 | .032 |
| | | .875 | .060 | .047 | .031 | .011 | .002 | .009 | .010 | .015 | .016 | .016 |
| | | .025 | .319 | .232 | .145 | .015 | .119 | .214 | .386 | .563 | .768 | .1039 |
| | | .250 | .284 | .222 | .149 | .042 | .075 | .196 | .314 | .475 | .604 | .778 |
| 20° | Upper | .500 | .212 | .164 | .108 | .017 | .072 | .145 | .211 | .310 | .397 | .498 |
| | | .750 | .126 | .100 | .066 | .003 | .050 | .093 | .128 | .177 | .219 | .270 |
| | | .875 | .073 | .058 | .038 | .001 | .031 | .055 | .074 | .100 | .121 | .145 |
| | Lower | .025 | .092 | .068 | .029 | .046 | .142 | .224 | | .447 | | |
| | | .250 | .083 | .066 | .039 | .010 | .078 | .147 | | .381 | | |
| | | .500 | .053 | .041 | .023 | .016 | .059 | .096 | | .336 | | |
| | | .750 | .026 | .020 | .011 | .012 | .070 | .092 | | .130 | | |
| | Total | .875 | .013 | .011 | .005 | .006 | .022 | .036 | | .072 | | |
| | | .025 | .363 | .280 | .196 | .105 | .044 | .006 | | .055 | | |
| | | .250 | .318 | .251 | .178 | .098 | .041 | .004 | | .062 | | |
| | | .500 | .239 | .191 | .134 | .071 | .018 | .019 | | .053 | | |
| 25° | Upper | .750 | .142 | .114 | .082 | .045 | .009 | .012 | | .027 | | |
| | | .875 | .082 | .067 | .049 | .028 | .006 | .005 | | .014 | | |
| | Lower | .025 | .455 | .348 | .225 | .059 | .098 | .230 | | .502 | | |
| | | .250 | .401 | .317 | .217 | .088 | .037 | .151 | | .443 | | |
| | | .500 | .292 | .232 | .157 | .055 | .041 | .115 | | .289 | | |
| | | .750 | .168 | .134 | .093 | .033 | .061 | .104 | | .157 | | |
| | Total | .875 | .095 | .078 | .054 | .022 | .016 | .041 | | .086 | | |
| | | .025 | .090 | .055 | .016 | .059 | .099 | .172 | .259 | .401 | .494 | .739 |
| | | .250 | .083 | .062 | .040 | .017 | .090 | .164 | .268 | .345 | .495 | .648 |
| | | .500 | .052 | .036 | .032 | .008 | .060 | .100 | .160 | .241 | .334 | .446 |
| Total | Upper | .750 | .026 | .019 | .018 | .001 | .035 | .058 | .088 | .124 | .161 | .205 |
| | | .875 | .013 | .010 | .010 | -.001 | .018 | .032 | .047 | .064 | .084 | .104 |
| | | .025 | .589 | .479 | .362 | .236 | .114 | .025 | .013 | .029 | .041 | .068 |
| | | .250 | .495 | .406 | .312 | .207 | .130 | .049 | .009 | .027 | .041 | .069 |
| | Lower | .500 | .363 | .300 | .228 | .146 | .081 | .010 | .018 | .037 | .043 | .058 |
| | | .750 | .203 | .169 | .130 | .085 | .044 | -.006 | .017 | .022 | .023 | .030 |
| | | .875 | .112 | .095 | .074 | .049 | .026 | -.004 | .009 | .011 | .011 | .015 |
| | Total | .025 | .679 | .534 | .378 | .177 | .015 | -.147 | -.272 | .430 | .535 | .807 |
| | | .250 | .578 | .468 | .352 | .190 | .040 | -.115 | -.259 | .372 | .536 | .717 |
| | | .500 | .415 | .336 | .260 | .138 | .021 | -.090 | -.178 | .278 | .377 | .504 |
| | | .750 | .229 | .188 | .148 | .084 | .009 | -.064 | -.105 | .146 | .184 | .235 |
| | | .875 | .125 | .105 | .084 | .048 | .008 | -.036 | -.056 | .075 | .095 | .119 |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (c) $A = 2$ rectangular wing, $r/s = 0.2$

| α_B | y/s | δ_w | | | | | | | | | | | |
|------------|-------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | |
| 0° | Upper | .025 | - .081 | - .074 | - .076 | - .066 | - .056 | - .034 | - .018 | .001 | .015 | | |
| | | .250 | - .089 | - .084 | - .084 | - .079 | - .073 | - .051 | - .033 | - .056 | .017 | | |
| | | .563 | - .092 | - .086 | - .086 | - .083 | - .077 | - .060 | - .046 | - .020 | .006 | | |
| | | .875 | - .090 | - .085 | - .082 | - .076 | - .071 | - .046 | - .030 | - .010 | .010 | | |
| | Lower | .025 | .825 | .602 | .427 | .317 | .280 | .141 | .081 | .049 | .015 | | |
| | | .250 | .850 | .842 | .648 | .476 | .329 | .204 | .123 | .068 | .017 | | |
| | | .563 | .991 | .849 | .648 | .468 | .313 | .190 | .108 | .047 | .006 | | |
| | | .875 | .948 | .765 | .574 | .419 | .280 | .176 | .098 | .046 | .010 | | |
| | Total | .025 | .906 | .676 | .503 | .383 | .276 | .175 | .099 | .048 | .000 | | |
| | | .250 | 1.093 | .926 | .738 | .555 | .402 | .255 | .155 | .124 | .000 | | |
| | | .563 | 1.083 | .936 | .734 | .551 | .390 | .250 | .150 | .067 | .000 | | |
| | | .875 | 1.038 | .850 | .656 | .495 | .351 | .222 | .128 | .056 | .000 | | |
| 3° | Upper | .025 | - .087 | - .079 | - .068 | - .062 | - .061 | - .053 | - .044 | - .033 | - .019 | | |
| | | .250 | - .092 | - .086 | - .080 | - .073 | - .074 | - .067 | - .061 | - .050 | - .024 | | |
| | | .563 | - .093 | - .087 | - .079 | - .075 | - .076 | - .068 | - .062 | - .051 | - .025 | | |
| | | .875 | - .090 | - .086 | - .077 | - .072 | - .067 | - .059 | - .050 | - .039 | - .013 | | |
| | Lower | .025 | .883 | .795 | .570 | .416 | .299 | .188 | .135 | .093 | .057 | | |
| | | .250 | 1.114 | .936 | .770 | .571 | .411 | .269 | .177 | .112 | .066 | | |
| | | .563 | 1.082 | .935 | .761 | .559 | .389 | .244 | .154 | .090 | .046 | | |
| | | .875 | 1.020 | .854 | .669 | .483 | .340 | .217 | .137 | .081 | .048 | | |
| | Total | .025 | .970 | .874 | .638 | .478 | .360 | .241 | .179 | .126 | .076 | | |
| | | .250 | 1.206 | 1.022 | .850 | .644 | .485 | .336 | .238 | .162 | .090 | | |
| | | .563 | 1.175 | 1.082 | .840 | .534 | .465 | .318 | .216 | .141 | .071 | | |
| | | .875 | 1.110 | .940 | .746 | .555 | .407 | .276 | .187 | .120 | .055 | | |
| 6° | Upper | .025 | - .087 | - .092 | - .084 | - .073 | - .072 | - .069 | - .049 | - .037 | | | |
| | | .250 | - .094 | - .096 | - .098 | - .088 | - .085 | - .071 | - .065 | - .044 | | | |
| | | .563 | - .096 | - .101 | - .090 | - .088 | - .086 | - .066 | - .062 | - .041 | | | |
| | | .875 | - .092 | - .096 | - .095 | - .084 | - .073 | - .061 | - .045 | - .032 | | | |
| | Lower | .025 | .754 | .730 | .562 | .412 | .299 | .224 | .172 | .125 | | | |
| | | .250 | .979 | .836 | .670 | .498 | .345 | .249 | .181 | .125 | | | |
| | | .563 | .990 | .843 | .665 | .482 | .320 | .222 | .155 | .104 | | | |
| | | .875 | .930 | .764 | .578 | .416 | .280 | .193 | .137 | .093 | | | |
| | Total | .025 | .841 | .822 | .646 | .485 | .371 | .293 | .221 | .168 | | | |
| | | .250 | 1.073 | .938 | .762 | .580 | .430 | .380 | .246 | .169 | | | |
| | | .563 | 1.086 | .944 | .756 | .570 | .406 | .388 | .217 | .145 | | | |
| | | .875 | 1.022 | .860 | .673 | .500 | .353 | .254 | .182 | .125 | | | |
| 10° | Upper | .025 | - .088 | - .086 | - .080 | - .076 | - .076 | - .078 | - .064 | | | | |
| | | .250 | - .091 | - .090 | - .084 | - .081 | - .080 | - .068 | - .068 | | | | |
| | | .563 | - .090 | - .087 | - .082 | - .083 | - .077 | - .074 | - .064 | | | | |
| | | .875 | - .087 | - .083 | - .083 | - .077 | - .074 | - .069 | - .048 | | | | |
| | Lower | .025 | .539 | .546 | .414 | .312 | .256 | .195 | | | | | |
| | | .250 | .784 | .629 | .466 | .358 | .281 | .211 | | | | | |
| | | .563 | .831 | .689 | .476 | .357 | .271 | .199 | | | | | |
| | | .875 | .753 | .579 | .416 | .315 | .242 | .177 | | | | | |
| | Total | .025 | .627 | .638 | .494 | .388 | .334 | .259 | | | | | |
| | | .250 | .875 | .719 | .550 | .439 | .361 | .279 | | | | | |
| | | .563 | .921 | .746 | .558 | .434 | .345 | .261 | | | | | |
| | | .875 | .840 | .662 | .493 | .389 | .311 | .225 | | | | | |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (c) A = 2 rectangular wing, r/s = 0.2 - Continued

| α_B | y/s | δ_w | | | | | | | | | |
|------------|-------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|----------------------------------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 0° | Upper | .025 .250 .563 .875 | | | | | | | | | |
| | Lower | .025 .250 .563 .875 | | | | | | | | | |
| | Total | .025 .250 .563 .875 | | | | | | | | | |
| 3° | Upper | .025 .250 .563 .875 | .001 .003 .005 .012 | .016 .036 .037 .042 | .044 .095 .096 .096 | .108 .195 .199 .190 | .200 .318 .322 .304 | .307 .470 .487 .447 | .474 .539 .558 .598 | .628 .833 .840 .781 | .741 .1001 .1014 .955 |
| | Lower | .025 .250 .563 .875 | .027 .026 .008 .011 | .007 .004 .018 .012 | .018 .034 .046 .036 | .048 .063 .070 .062 | .062 .073 .078 .073 | .076 .084 .088 .083 | .081 .086 .088 .084 | .085 .090 .093 .091 | .089 .095 .098 .095 |
| | Total | .025 .250 .563 .875 | .028 .023 .003 .001 | .009 .040 .055 .054 | .062 .129 .142 .132 | .156 .258 .269 .252 | .262 .391 .400 .377 | .383 .554 .575 .530 | .555 .725 .746 .682 | .713 .923 .933 .872 | .830 .1096 .1112 .1050 |
| 6° | Upper | .025 .250 .563 .875 | .033 .043 .046 .020 | .086 .028 .003 .020 | .004 .028 .050 .061 | .031 .102 .129 .140 | .098 .208 .231 .227 | .209 .334 .385 .375 | .348 .505 .556 .533 | .548 .683 .736 .696 | .69 ; .88 ; .93 ; .89 ; |
| | Lower | .025 .250 .563 .875 | .079 .075 .056 .051 | .043 .038 .024 .030 | .009 .000 .014 .010 | .027 .033 .041 .036 | .043 .049 .052 .048 | .059 .063 .065 .061 | .069 .072 .070 .071 | .075 .077 .076 .076 | .07 .08 .080 .083 |
| | Total | .025 .250 .563 .875 | .112 .118 .102 .071 | .069 .060 .027 .071 | .013 .028 .064 .071 | .058 .135 .170 .176 | .141 .257 .283 .275 | .268 .397 .450 .436 | .417 .577 .526 .504 | .523 .760 .812 .772 | .770 .969 .1016 .973 |
| 10° | Upper | .025 .250 .563 .875 | .062 .071 .059 .042 | .053 .059 .040 .017 | .051 .040 .008 .015 | .018 .013 .063 .082 | .037 .097 .156 .179 | .102 .203 .276 .291 | .188 .325 .413 .422 | .329 .507 .615 .591 | .523 .683 .762 .755 |
| | Lower | .025 .250 .563 .875 | .140 .156 .142 .129 | .087 .101 .089 .081 | .039 .047 .036 .037 | .013 .009 .016 .010 | .039 .043 .049 .038 | .061 .063 .065 .059 | .067 .067 .070 .066 | .065 .069 .070 .069 | .078 .080 .080 .080 |
| Total | | .025 .250 .563 .875 | .202 .227 .201 .171 | .140 .160 .129 .098 | .090 .087 .044 .022 | .005 .022 .079 .093 | .076 .140 .205 .217 | .163 .266 .341 .350 | .255 .392 .483 .488 | .394 .576 .585 .560 | .601 .763 .848 .835 |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (c) A = 2 rectangular wing, r/s = 0.2 - Continued

| a_B | y/s | δ_w | | | | | | | | | | |
|-------|-------|------------|--------|-------|------|------|------|------|------|----|----|----|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° |
| 15° | Upper | .025 | | | | | | | | | | |
| | | .050 | .074 | .092 | .083 | .084 | .076 | .080 | .073 | | | |
| | | .063 | .081 | .097 | .085 | .085 | .078 | .080 | .071 | | | |
| | | .075 | .083 | .097 | .086 | .083 | .079 | .079 | .071 | | | |
| | Lower | .025 | .082 | .091 | .083 | .083 | .074 | .075 | .064 | | | |
| | | .050 | .873 | .735 | .641 | .515 | .431 | .363 | .275 | | | |
| | | .063 | 1.121 | .964 | .813 | .632 | .486 | .398 | .310 | | | |
| | | .075 | 1.189 | 1.034 | .879 | .577 | .522 | .421 | .325 | | | |
| | Total | .025 | .097 | .827 | .724 | .599 | .507 | .443 | .348 | | | |
| | | .050 | 1.202 | 1.061 | .898 | .717 | .564 | .478 | .381 | | | |
| | | .063 | 1.272 | 1.131 | .969 | .760 | .601 | .500 | .396 | | | |
| | | .075 | 1.226 | 1.058 | .878 | .685 | .536 | .450 | .349 | | | |
| 20° | Upper | .025 | | | | | | | | | | |
| | | .050 | .097 | .093 | .088 | .088 | .086 | | | | | |
| | | .063 | .097 | .092 | .087 | .087 | .084 | | | | | |
| | | .075 | .096 | .091 | .082 | .082 | .079 | | | | | |
| | Lower | .025 | | | | | | | | | | |
| | | .050 | .868 | .770 | .633 | .540 | | | | | | |
| | | .063 | 1.069 | .886 | .716 | .545 | | | | | | |
| | | .075 | 1.148 | .957 | .778 | .649 | | | | | | |
| | Total | .025 | | | | | | | | | | |
| | | .050 | .965 | .863 | .721 | .626 | | | | | | |
| | | .063 | 1.166 | .978 | .803 | .629 | | | | | | |
| | | .075 | 1.244 | 1.048 | .860 | .728 | | | | | | |
| 25° | Upper | .025 | | | | | | | | | | |
| | | .050 | .070 | .071 | .073 | .073 | .072 | | | | | |
| | | .063 | .072 | .072 | .072 | .072 | .073 | | | | | |
| | | .075 | .066 | .067 | .067 | .069 | .068 | | | | | |
| | Lower | .025 | | | | | | | | | | |
| | | .050 | -1.039 | .882 | .748 | .602 | | | | | | |
| | | .063 | 1.139 | .966 | .821 | .696 | | | | | | |
| | | .075 | 1.199 | 1.033 | .892 | .757 | | | | | | |
| | Total | .025 | | | | | | | | | | |
| | | .050 | 1.109 | .953 | .821 | .674 | | | | | | |
| | | .063 | 1.211 | 1.038 | .893 | .769 | | | | | | |
| | | .075 | 1.265 | 1.100 | .961 | .825 | | | | | | |

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE
BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Concluded
(c) A = 2 rectangular wing, r/s = 0.2 - Concluded

| α_B | y/s | δ_w | | | | | | | | | | |
|------------|-------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° | |
| 15° | Upper | .025 | -.064 | -.078 | -.060 | -.028 | .037 | .098 | .193 | .294 | .456 | |
| | | .250 | -.066 | -.073 | -.048 | -.003 | .071 | .172 | .302 | .455 | .636 | |
| | | .563 | -.056 | -.060 | -.022 | .049 | .119 | .239 | .383 | .561 | .752 | |
| | | .875 | -.046 | -.033 | -.004 | | | | | | | |
| | Lower | .025 | .206 | .148 | .087 | .018 | -.022 | -.051 | -.067 | -.074 | -.083 | |
| | | .250 | .248 | .183 | .115 | .034 | -.015 | -.047 | -.062 | -.072 | -.080 | |
| | | .563 | .251 | .182 | .105 | .028 | -.019 | -.053 | -.067 | -.075 | -.082 | |
| | | .875 | .221 | .164 | .099 | .032 | -.009 | -.025 | -.057 | -.066 | -.077 | |
| | Total | .025 | .270 | .226 | .147 | .046 | -.059 | -.149 | -.260 | -.368 | .539 | |
| | | .250 | .314 | .256 | .163 | .037 | -.086 | -.219 | -.364 | -.527 | .716 | |
| | | .563 | .307 | .242 | .127 | -.021 | -.138 | -.292 | -.450 | -.536 | .834 | |
| | | .875 | .267 | .197 | .103 | -.012 | -.154 | -.290 | -.447 | -.622 | .808 | |
| 20° | Upper | .025 | -.075 | -.078 | -.055 | -.023 | .042 | .131 | .208 | .325 | .485 | |
| | | .250 | -.074 | -.075 | -.043 | -.009 | .065 | .167 | .295 | .445 | .618 | |
| | | .563 | -.065 | -.060 | -.021 | .026 | .105 | .214 | .354 | .522 | .720 | |
| | | .875 | -.051 | -.046 | -.003 | .050 | .115 | .209 | .329 | .464 | .629 | |
| | Lower | .025 | .333 | .254 | .162 | .066 | .024 | -.017 | -.040 | -.059 | .068 | |
| | | .250 | .403 | .312 | .213 | .100 | .038 | -.009 | -.038 | -.057 | .066 | |
| | | .563 | .431 | .331 | .221 | .104 | .038 | -.010 | -.040 | -.057 | .068 | |
| | | .875 | .389 | .301 | .204 | .101 | .048 | -.001 | -.029 | -.048 | .064 | |
| | Total | .025 | .408 | .332 | .217 | .089 | -.018 | -.148 | -.248 | -.384 | .553 | |
| | | .250 | .477 | .387 | .256 | .109 | -.027 | -.176 | -.333 | .508 | .684 | |
| | | .563 | .496 | .391 | .242 | .078 | -.067 | -.224 | -.394 | .579 | .788 | |
| | | .875 | .440 | .347 | .207 | .051 | -.067 | -.206 | -.358 | .512 | .693 | |
| 25° | Upper | .025 | -.066 | -.069 | -.046 | .006 | .085 | .165 | .227 | | .556 | |
| | | .250 | -.068 | -.063 | -.043 | .015 | .089 | .181 | .302 | | .634 | |
| | | .563 | -.065 | -.062 | -.023 | .043 | .123 | .214 | .331 | | .709 | |
| | | .875 | -.060 | -.045 | -.023 | .029 | .079 | .130 | .228 | | .514 | |
| | Lower | .025 | .476 | .387 | .267 | .170 | .078 | .018 | -.019 | | .054 | |
| | | .250 | .578 | .469 | .343 | .218 | .115 | .043 | -.016 | | .058 | |
| | | .563 | .631 | .507 | .366 | .226 | .118 | .042 | -.018 | | .059 | |
| | | .875 | .517 | .421 | .308 | .188 | .089 | .023 | -.027 | | .064 | |
| | Total | .025 | .542 | .456 | .313 | .164 | -.007 | -.147 | -.246 | | .510 | |
| | | .250 | .646 | .532 | .386 | .203 | -.026 | -.138 | -.318 | | .692 | |
| | | .563 | .696 | .569 | .389 | .185 | -.005 | -.172 | -.349 | | .768 | |
| | | .875 | .577 | .466 | .331 | .159 | .010 | -.107 | -.255 | | .578 | |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS
(a) $A = 4$ triangular wing, $r/s = 0.2$

| α_B | X/r | δ_w | | | | | | | | | | | |
|------------|-------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | |
| 0° | 1.134 | -0.004 | 0.000 | 0.000 | -0.001 | -0.001 | .001 | .001 | .001 | 0.000 | 0.000 | 0.000 | |
| | 1.259 | -0.001 | 0.001 | 0.001 | 0.003 | -0.001 | -0.001 | -0.001 | -0.001 | 0.001 | 0.001 | 0.001 | |
| | 1.384 | -0.039 | 0.000 | 0.000 | -0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | 1.509 | -0.039 | 0.164 | -0.008 | -0.005 | -0.021 | -0.059 | 0.000 | -0.003 | -0.002 | -0.002 | -0.002 | |
| | 1.634 | -0.093 | 0.043 | 0.043 | 0.056 | 0.052 | 0.060 | 0.044 | 0.027 | 0.016 | 0.009 | 0.009 | |
| | 1.756 | -0.167 | 0.110 | 0.097 | 0.116 | 0.121 | 0.100 | 0.084 | 0.061 | 0.034 | 0.016 | 0.016 | |
| | 1.884 | -0.060 | 0.111 | 0.148 | 0.131 | 0.104 | 0.086 | 0.068 | 0.057 | 0.037 | 0.018 | 0.018 | |
| | 2.009 | -0.048 | 0.081 | 0.107 | 0.104 | 0.102 | 0.087 | 0.068 | 0.050 | 0.033 | 0.016 | 0.016 | |
| | 2.134 | -0.027 | 0.045 | 0.055 | 0.071 | 0.072 | 0.069 | 0.060 | 0.050 | 0.036 | 0.014 | 0.014 | |
| | 2.259 | -0.013 | 0.022 | 0.030 | 0.044 | 0.045 | 0.049 | 0.046 | 0.036 | 0.025 | 0.012 | 0.012 | |
| 3° | 2.384 | -0.016 | 0.010 | 0.008 | 0.021 | 0.027 | 0.033 | 0.033 | 0.027 | 0.024 | 0.012 | 0.010 | |
| | 2.509 | 0.14 | -0.05 | -0.05 | -0.05 | -0.09 | 0.18 | 0.16 | 0.14 | 0.07 | 0.008 | 0.002 | |
| | 1.134 | -0.008 | -0.003 | -0.002 | -0.002 | -0.002 | .001 | -0.002 | -0.002 | -0.001 | 0.001 | 0.001 | |
| | 1.259 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.002 | 0.001 | 0.001 | |
| | 1.384 | -0.001 | -0.01 | -0.000 | -0.003 | -0.000 | -0.001 | -0.000 | -0.001 | -0.001 | 0.001 | 0.001 | |
| | 1.509 | -0.067 | -0.027 | -0.074 | -0.058 | -0.053 | -0.083 | -0.006 | -0.001 | -0.001 | 0.001 | 0.001 | |
| | 1.634 | -0.128 | -0.122 | -0.086 | -0.089 | -0.091 | -0.083 | -0.060 | -0.040 | -0.030 | 0.023 | 0.023 | |
| | 1.756 | -0.080 | -0.065 | -0.149 | -0.164 | -0.169 | -0.141 | -0.126 | -0.100 | -0.078 | 0.048 | 0.048 | |
| | 1.884 | -0.097 | -0.088 | -0.158 | -0.168 | -0.136 | -0.108 | -0.093 | -0.076 | -0.055 | 0.038 | 0.038 | |
| | 2.009 | -0.087 | -0.078 | -0.128 | -0.138 | -0.133 | -0.113 | -0.093 | -0.076 | -0.055 | 0.037 | 0.037 | |
| 6° | 2.134 | -0.053 | -0.069 | -0.087 | -0.101 | -0.099 | -0.084 | -0.076 | -0.055 | -0.041 | 0.020 | 0.017 | |
| | 2.259 | -0.020 | -0.027 | -0.042 | -0.049 | -0.057 | -0.055 | -0.053 | -0.041 | -0.028 | 0.012 | 0.005 | |
| | 2.384 | -0.107 | -0.092 | -0.16 | -0.24 | -0.27 | -0.27 | -0.28 | -0.22 | -0.14 | 0.10 | 0.05 | |
| | 2.509 | -0.012 | -0.012 | -0.014 | -0.012 | -0.011 | -0.017 | -0.015 | -0.012 | -0.008 | 0.005 | 0.005 | |
| | 1.134 | 0.000 | -0.001 | 0.000 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | 0.000 | 0.000 | |
| | 1.259 | -0.001 | -0.002 | -0.002 | -0.001 | -0.002 | -0.002 | -0.001 | -0.001 | -0.001 | 0.001 | 0.003 | |
| | 1.384 | -0.006 | -0.003 | -0.001 | -0.003 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | 0.003 | 0.003 | |
| | 1.509 | -0.005 | -0.028 | -0.048 | -0.048 | -0.059 | -0.058 | -0.058 | -0.058 | -0.058 | 0.029 | 0.029 | |
| | 1.634 | -0.150 | -0.130 | -0.111 | -0.095 | -0.074 | -0.059 | -0.040 | -0.028 | -0.018 | 0.048 | 0.048 | |
| | 1.756 | -0.094 | -0.100 | -0.168 | -0.168 | -0.156 | -0.139 | -0.118 | -0.098 | -0.078 | 0.050 | 0.050 | |
| 10° | 1.884 | -0.147 | -0.165 | -0.171 | -0.156 | -0.135 | -0.125 | -0.101 | -0.078 | -0.058 | 0.037 | 0.037 | |
| | 2.009 | -0.137 | -0.156 | -0.160 | -0.126 | -0.107 | -0.095 | -0.071 | -0.058 | -0.045 | 0.026 | 0.026 | |
| | 2.134 | -0.096 | -0.116 | -0.121 | -0.097 | -0.082 | -0.076 | -0.068 | -0.055 | -0.045 | 0.024 | 0.024 | |
| | 2.259 | -0.041 | -0.057 | -0.068 | -0.065 | -0.058 | -0.058 | -0.049 | -0.040 | -0.030 | 0.013 | 0.013 | |
| | 2.384 | -0.021 | -0.014 | -0.013 | -0.010 | -0.001 | -0.006 | -0.004 | -0.004 | -0.004 | 0.001 | 0.001 | |
| | 2.509 | -0.009 | -0.011 | -0.009 | -0.009 | -0.012 | -0.018 | -0.008 | -0.008 | -0.008 | 0.009 | 0.009 | |
| | 1.134 | -0.008 | -0.008 | -0.008 | -0.008 | -0.012 | -0.018 | -0.008 | -0.008 | -0.008 | 0.015 | 0.015 | |
| | 1.259 | -0.040 | -0.010 | -0.008 | -0.008 | -0.003 | -0.008 | -0.004 | -0.004 | -0.004 | 0.000 | 0.000 | |
| | 1.384 | -0.003 | -0.003 | -0.000 | -0.000 | -0.003 | -0.003 | -0.004 | -0.004 | -0.004 | 0.002 | 0.002 | |
| | 1.509 | -0.028 | -0.024 | -0.024 | -0.024 | -0.010 | -0.003 | -0.003 | -0.003 | -0.003 | 0.047 | 0.047 | |
| 15° | 1.634 | -0.165 | -0.165 | -0.165 | -0.165 | -0.093 | -0.061 | -0.051 | -0.047 | -0.047 | 0.040 | 0.040 | |
| | 1.756 | -0.107 | -0.107 | -0.134 | -0.134 | -0.134 | -0.140 | -0.140 | -0.140 | -0.140 | 0.118 | 0.118 | |
| | 1.884 | -0.149 | -0.145 | -0.166 | -0.166 | -0.166 | -0.166 | -0.166 | -0.166 | -0.166 | 0.053 | 0.053 | |
| | 2.009 | -0.113 | -0.075 | -0.093 | -0.093 | -0.093 | -0.135 | -0.135 | -0.135 | -0.135 | 0.036 | 0.036 | |
| | 2.134 | -0.055 | -0.037 | -0.053 | -0.053 | -0.053 | -0.056 | -0.056 | -0.056 | -0.056 | 0.020 | 0.020 | |
| | 2.259 | -0.028 | -0.028 | -0.035 | -0.035 | -0.035 | -0.016 | -0.016 | -0.016 | -0.016 | 0.013 | 0.013 | |
| | 2.384 | -0.149 | -0.17 | -0.17 | -0.17 | -0.17 | -0.15 | -0.15 | -0.15 | -0.15 | 0.015 | 0.015 | |
| | 2.509 | -0.015 | -0.029 | -0.034 | -0.035 | -0.036 | -0.036 | -0.034 | -0.034 | -0.034 | 0.049 | 0.049 | |
| | 1.134 | -0.17 | -0.17 | -0.17 | -0.17 | -0.17 | -0.15 | -0.14 | -0.14 | -0.14 | 0.15 | 0.15 | |
| | 1.259 | -0.001 | -0.01 | -0.01 | -0.01 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | 0.002 | 0.002 | |
| 20° | 1.384 | -0.048 | -0.021 | -0.021 | -0.021 | -0.021 | -0.006 | -0.003 | -0.003 | -0.003 | 0.004 | 0.004 | |
| | 1.509 | -0.024 | -0.024 | -0.024 | -0.024 | -0.024 | -0.014 | -0.007 | -0.007 | -0.007 | 0.006 | 0.006 | |
| | 1.634 | -0.113 | -0.193 | -0.140 | -0.140 | -0.081 | -0.058 | -0.034 | -0.034 | -0.034 | 0.028 | 0.028 | |
| | 1.756 | -0.043 | -0.243 | -0.244 | -0.244 | -0.207 | -0.180 | -0.170 | -0.170 | -0.170 | 0.064 | 0.064 | |
| | 1.884 | -0.033 | -0.217 | -0.24 | -0.24 | -0.167 | -0.167 | -0.147 | -0.147 | -0.147 | 0.072 | 0.072 | |
| | 2.009 | -0.184 | -0.178 | -0.171 | -0.148 | -0.139 | -0.139 | -0.129 | -0.129 | -0.129 | 0.068 | 0.068 | |
| | 2.134 | -0.119 | -0.137 | -0.145 | -0.139 | -0.139 | -0.124 | -0.124 | -0.124 | -0.124 | 0.090 | 0.090 | |
| | 2.259 | -0.067 | -0.106 | -0.120 | -0.128 | -0.128 | -0.130 | -0.130 | -0.130 | -0.130 | 0.046 | 0.046 | |
| | 2.384 | -0.070 | -0.081 | -0.099 | -0.104 | -0.104 | -0.095 | -0.095 | -0.095 | -0.095 | 0.078 | 0.078 | |
| | 2.509 | -0.083 | -0.100 | -0.094 | -0.120 | -0.120 | -0.084 | -0.111 | -0.107 | -0.093 | 0.049 | 0.049 | |
| 25° | 1.134 | -0.035 | -0.035 | -0.034 | -0.034 | -0.034 | -0.038 | -0.038 | -0.038 | -0.038 | 0.33 | 0.33 | |
| | 1.259 | -0.055 | -0.050 | -0.052 | -0.052 | -0.052 | -0.054 | -0.054 | -0.054 | -0.054 | 0.006 | 0.006 | |
| | 1.384 | -0.048 | -0.048 | -0.044 | -0.044 | -0.044 | -0.042 | -0.042 | -0.042 | -0.042 | 0.007 | 0.007 | |
| | 1.509 | -0.144 | -0.144 | -0.148 | -0.148 | -0.148 | -0.142 | -0.142 | -0.142 | -0.142 | 0.028 | 0.028 | |
| | 1.634 | -0.154 | -0.154 | -0.154 | -0.154 | -0.154 | -0.146 | -0.146 | -0.146 | -0.146 | 0.015 | 0.015 | |
| | 1.756 | -0.099 | -0.193 | -0.206 | -0.206 | -0.206 | -0.181 | -0.181 | -0.181 | -0.181 | 0.072 | 0.072 | |
| | 1.884 | -0.064 | -0.166 | -0.166 | -0.166 | -0.166 | -0.166 | -0.166 | -0.166 | -0.166 | 0.107 | 0.107 | |
| | 2.009 | -0.154 | -0.154 | -0.154 | -0.154 | -0.154 | -0.154 | -0.154 | -0.154 | -0.154 | 0.118 | 0.118 | |
| 28° | 2.134 | -0.119 | -0.192 | -0.173 | -0.173 | -0.173 | -0.157 | -0.157 | -0.157 | -0.157 | 0.102 | 0.102 | |
| | 2.259 | -0.070 | -0.107 | -0.189 | -0.173 | -0.173 | -0.168 | -0.168 | -0.168 | -0.168 | 0.126 | 0.126 | |
| | 2.384 | -0.070 | -0.100 | -0.186 | -0.173 | -0.173 | -0.168 | -0.168 | -0.168 | -0.168 | 0.128 | 0.128 | |
| | 2.509 | -0.083 | -0.102 | -0.186 | -0.186 | -0.186 | -0.186 | -0.186 | -0.186 | -0.186 | 0.142 | 0.142 | |
| | 1.134 | -0.035 | -0.035 | -0.035 | -0.035 | -0.035 | -0.035 | -0.035 | -0.035 | -0.035 | 0.33 | 0.33 | |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(a) $A = \frac{1}{4}$ triangular wing, $r/s = 0.2$ - Concluded

| a_B | x/r | δ_w | | | | | | | | | |
|-------|-------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 0° | 1.134 | - .001 | - .001 | - .007 | - .001 | - .007 | - .001 | - .002 | - .002 | - .001 | .000 |
| | 1.259 | - .003 | - .002 | - .006 | - .002 | - .001 | - .002 | - .003 | - .003 | - .001 | .000 |
| | 1.384 | - .001 | - .001 | - .006 | .000 | .001 | .001 | .002 | .002 | .001 | .001 |
| | 1.509 | - .008 | - .005 | - .006 | .009 | .001 | .000 | .002 | .002 | .001 | .001 |
| | 1.634 | - .010 | - .001 | - .014 | - .019 | .011 | .007 | .005 | .009 | .023 | - .032 |
| | 1.756 | - .010 | - .004 | - .024 | - .042 | .054 | .034 | .047 | .045 | .072 | - .082 |
| | 1.884 | - .013 | - .004 | - .024 | - .043 | .062 | .043 | .049 | .047 | .073 | - .083 |
| | 2.009 | - .011 | - .007 | - .027 | - .037 | .054 | .033 | .048 | .046 | .073 | - .083 |
| | 2.134 | - .005 | - .007 | - .024 | - .037 | .038 | .022 | .033 | .024 | .066 | - .073 |
| | 2.259 | - .001 | - .010 | - .026 | - .037 | .037 | .021 | .016 | .014 | .033 | - .040 |
| 3° | 1.134 | - .002 | - .004 | - .003 | - .001 | - .002 | - .002 | - .002 | - .002 | - .001 | .000 |
| | 1.259 | - .001 | - .000 | - .001 | - .002 | - .001 | - .003 | - .001 | - .001 | - .000 | .001 |
| | 1.384 | - .003 | - .001 | - .001 | - .003 | - .002 | - .002 | - .002 | - .002 | - .001 | .001 |
| | 1.509 | - .007 | - .007 | .012 | .019 | .007 | .005 | .003 | .003 | .003 | .018 |
| | 1.634 | - .023 | - .023 | - .027 | - .008 | - .005 | - .013 | - .013 | - .013 | - .018 | .067 |
| | 1.756 | - .021 | - .003 | - .007 | - .021 | - .044 | - .054 | - .047 | - .048 | - .059 | .059 |
| | 1.884 | - .022 | - .004 | - .021 | - .021 | - .035 | - .049 | - .048 | - .049 | - .053 | .063 |
| | 2.009 | - .030 | - .019 | .001 | - .011 | - .019 | - .021 | - .023 | - .023 | - .031 | .031 |
| | 2.134 | - .026 | - .014 | .000 | - .006 | - .010 | - .014 | - .016 | - .016 | - .025 | .028 |
| | 2.259 | - .014 | - .004 | - .005 | - .010 | - .010 | - .006 | - .015 | - .015 | - .028 | .034 |
| 6° | 1.134 | - .002 | - .007 | - .003 | - .001 | - .002 | - .002 | - .002 | - .002 | - .001 | .000 |
| | 1.259 | - .001 | - .000 | - .001 | - .002 | - .001 | - .003 | - .001 | - .001 | - .000 | .001 |
| | 1.384 | - .003 | - .001 | - .001 | - .003 | - .002 | - .002 | - .002 | - .002 | - .001 | .001 |
| | 1.509 | - .007 | - .007 | .012 | .019 | .007 | .005 | .003 | .003 | .003 | .018 |
| | 1.634 | - .023 | - .023 | - .027 | - .008 | - .005 | - .013 | - .013 | - .013 | - .018 | .067 |
| | 1.756 | - .021 | - .003 | - .007 | - .021 | - .044 | - .054 | - .047 | - .048 | - .059 | .059 |
| | 1.884 | - .022 | - .004 | - .021 | - .021 | - .035 | - .049 | - .048 | - .049 | - .053 | .063 |
| | 2.009 | - .030 | - .019 | .001 | - .011 | - .019 | - .021 | - .023 | - .023 | - .031 | .031 |
| | 2.134 | - .026 | - .014 | .000 | - .006 | - .010 | - .014 | - .016 | - .016 | - .025 | .028 |
| | 2.259 | - .014 | - .004 | - .005 | - .010 | - .010 | - .006 | - .015 | - .015 | - .028 | .034 |
| 10° | 1.134 | - .004 | - .017 | - .007 | - .008 | - .008 | - .007 | - .009 | - .010 | - .009 | - .010 |
| | 1.259 | - .002 | - .005 | - .001 | - .001 | - .002 | - .001 | - .000 | - .000 | - .001 | - .001 |
| | 1.384 | - .003 | - .005 | - .000 | - .001 | - .002 | - .001 | - .000 | - .000 | - .001 | - .001 |
| | 1.509 | - .002 | - .004 | - .015 | - .024 | - .004 | - .002 | - .002 | - .003 | - .002 | - .003 |
| | 1.634 | - .035 | - .027 | - .034 | - .017 | - .015 | - .022 | - .072 | - .056 | - .032 | - .099 |
| | 1.756 | - .041 | - .028 | - .021 | - .004 | - .008 | - .036 | - .045 | - .046 | - .065 | - .080 |
| | 1.884 | - .039 | - .028 | - .009 | - .006 | - .020 | - .030 | - .037 | - .020 | - .026 | - .038 |
| | 2.009 | - .042 | - .033 | - .018 | - .001 | - .010 | - .014 | - .014 | - .020 | - .026 | - .038 |
| | 2.134 | - .027 | - .000 | - .018 | - .001 | - .003 | - .001 | - .005 | - .005 | - .015 | - .023 |
| | 2.259 | - .017 | - .011 | - .030 | - .020 | - .012 | - .001 | - .005 | - .005 | - .009 | - .023 |
| 15° | 1.134 | - .015 | - .025 | - .014 | - .003 | - .016 | - .015 | - .015 | - .014 | - .015 | - .015 |
| | 1.259 | - .004 | - .004 | - .002 | - .002 | - .004 | - .003 | - .003 | - .003 | - .002 | - .002 |
| | 1.384 | - .001 | - .001 | - .002 | - .002 | - .004 | - .003 | - .003 | - .003 | - .002 | - .002 |
| | 1.509 | - .002 | - .002 | - .003 | - .002 | - .008 | - .008 | - .008 | - .008 | - .001 | - .001 |
| | 1.634 | - .049 | - .059 | - .056 | - .015 | - .035 | - .083 | - .082 | - .049 | - .124 | - .244 |
| | 1.756 | - .047 | - .059 | - .056 | - .015 | - .032 | - .039 | - .054 | - .074 | - .066 | - .066 |
| | 1.884 | - .048 | - .055 | - .053 | - .003 | - .028 | - .038 | - .045 | - .047 | - .068 | - .068 |
| | 2.009 | - .061 | - .040 | - .033 | - .007 | - .007 | - .005 | - .008 | - .014 | - .028 | - .028 |
| | 2.134 | - .060 | - .045 | - .015 | - .005 | - .005 | - .008 | - .006 | - .001 | - .14 | - .201 |
| | 2.259 | - .056 | - .041 | - .008 | - .008 | - .008 | - .010 | - .007 | - .003 | - .001 | - .001 |
| 20° | 1.134 | - .017 | - .035 | - .021 | - .020 | - .017 | - .021 | - .030 | - .021 | - .014 | - .020 |
| | 1.259 | - .010 | - .009 | - .011 | - .010 | - .009 | - .004 | - .004 | - .003 | - .011 | - .005 |
| | 1.384 | - .011 | - .009 | - .011 | - .010 | - .009 | - .003 | - .003 | - .004 | - .010 | - .004 |
| | 1.509 | - .004 | - .001 | - .023 | - .041 | - .003 | - .003 | - .003 | - .003 | - .002 | - .002 |
| | 1.634 | - .031 | - .011 | - .037 | - .027 | - .017 | - .001 | - .007 | - .017 | - .027 | - .033 |
| | 1.756 | - .056 | - .050 | - .035 | - .024 | - .006 | - .016 | - .066 | - .083 | - .062 | - .086 |
| | 1.884 | - .052 | - .036 | - .018 | - .005 | - .016 | - .030 | - .034 | - .037 | - .032 | - .047 |
| | 2.009 | - .075 | - .047 | - .029 | - .007 | - .004 | - .002 | - .010 | - .009 | - .018 | - .030 |
| | 2.134 | - .082 | - .063 | - .033 | - .015 | - .005 | - .003 | - .008 | - .003 | - .014 | - .000 |
| | 2.259 | - .084 | - .062 | - .029 | - .011 | - .000 | - .003 | - .013 | - .002 | - .010 | - .021 |
| 25° | 1.134 | - .017 | - .035 | - .021 | - .020 | - .017 | - .021 | - .030 | - .021 | - .014 | - .020 |
| | 1.259 | - .010 | - .009 | - .011 | - .010 | - .009 | - .004 | - .004 | - .003 | - .011 | - .005 |
| | 1.384 | - .011 | - .009 | - .011 | - .010 | - .009 | - .004 | - .004 | - .004 | - .010 | - .004 |
| | 1.509 | - .004 | - .001 | - .023 | - .041 | - .003 | - .003 | - .003 | - .003 | - .002 | - .002 |
| | 1.634 | - .031 | - .011 | - .037 | - .027 | - .017 | - .001 | - .007 | - .017 | - .027 | - .033 |
| | 1.756 | - .067 | - .038 | - .022 | - .002 | - .013 | - .007 | - .025 | - .021 | - .036 | - .049 |
| | 1.884 | - .065 | - .040 | - .017 | - .005 | - .008 | - .008 | - .010 | - .024 | - .027 | - .039 |
| | 2.009 | - .086 | - .038 | - .018 | - .004 | - .008 | - .007 | - .014 | - .020 | - .031 | - .031 |
| | 2.134 | - .092 | - .038 | - .014 | - .004 | - .008 | - .006 | - .014 | - .018 | - .027 | - .039 |
| | 2.259 | - .071 | - .021 | - .003 | - .003 | - .004 | - .006 | - .008 | - .007 | - .012 | - .008 |
| 28° | 1.134 | - .097 | - .039 | - .016 | - .006 | - .013 | - .005 | - .014 | - .015 | - .019 | - .012 |
| | 1.259 | - .099 | - .050 | - .031 | - .026 | - .019 | - .026 | - .026 | - .029 | - .030 | - .020 |
| | 1.384 | - .071 | - .021 | - .003 | - .003 | - .004 | - .005 | - .006 | - .008 | - .012 | - .008 |
| | 1.509 | - .071 | - .021 | - .003 | - .003 | - .004 | - .005 | - .006 | - .008 | - .012 | - .008 |
| | 1.634 | - .071 | - .021 | - .003 | - .003 | - .004 | - .005 | - .006 | - .008 | - .012 | - .008 |
| | 1.756 | - .071 | - .021 | - .003 | - .003 | - .004 | - .005 | - .006 | - .008 | - .012 | - .008 |
| | 1.884 | - .065 | - .017 | - .005 | - .008 | - .008 | - .007 | - .010 | - .014 | - .020 | - .016 |
| | 2.009 | - .066 | - .018 | - .006 | - .009 | - .009 | - .008 | - .010 | - .014 | - .020 | - .016 |
| | 2.134 | - .092 | - .038 | - .014 | - .004 | - .008 | - .007 | - .014 | - .018 | - .027 | - .031 |
| | 2.259 | - .071 | - .021 | - .003 | - .003 | - .004 | - .005 | - .006 | - .008 | - .012 | - .008 |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(b) $A = 2$ triangular wing, $r/s = 0.2$

| α_B | x/r | δ_w | | | | | | | | | | | |
|------------|-------|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | |
| 0° | 1.134 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .003 | .072 | |
| | 1.259 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .002 | .002 | .000 | .000 | |
| | 1.384 | - .003 | .000 | .000 | .000 | .000 | - .018 | -.089 | .016 | .005 | .002 | .000 | |
| | 1.509 | - .019 | - .018 | - .017 | - .017 | - .018 | - .021 | -.040 | .032 | .019 | .009 | .000 | |
| | 1.634 | - .100 | - .039 | - .004 | - .004 | - .011 | - .083 | -.088 | .056 | .027 | .013 | .001 | |
| | 1.756 | - .126 | - .001 | .007 | .007 | .074 | .089 | .088 | .057 | .042 | .033 | - .001 | |
| | 1.884 | .077 | .099 | .011 | .024 | .126 | .103 | .079 | .061 | .052 | .026 | - .003 | |
| | 2.009 | .057 | .088 | .009 | .017 | .124 | .111 | .077 | .047 | .036 | .019 | - .001 | |
| | 2.134 | .067 | .088 | .006 | .017 | .099 | .099 | .067 | .059 | .040 | .020 | .000 | |
| | 2.259 | .047 | .035 | .004 | .015 | .051 | .071 | .061 | .049 | .030 | .014 | .003 | |
| 3° | 1.134 | - .013 | .013 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | |
| | 1.259 | - .004 | - .001 | .000 | .001 | .001 | .001 | .001 | .018 | .005 | .001 | .003 | |
| | 1.384 | - .008 | - .001 | - .001 | - .001 | - .001 | - .036 | -.066 | .029 | .024 | .016 | .009 | |
| | 1.509 | - .008 | - .008 | - .008 | - .008 | - .008 | - .083 | -.042 | .068 | .040 | .026 | .020 | |
| | 1.634 | - .020 | - .008 | - .008 | - .008 | - .008 | - .081 | -.072 | .068 | .051 | .038 | .024 | |
| | 1.756 | - .013 | - .049 | - .019 | - .047 | - .054 | - .130 | -.149 | .099 | .076 | .060 | .041 | |
| | 1.884 | .006 | .044 | .007 | .047 | .189 | .164 | .146 | .121 | .081 | .068 | .042 | |
| | 2.009 | .009 | .082 | .003 | .062 | .162 | .157 | .147 | .114 | .085 | .065 | .043 | |
| | 2.134 | .007 | .082 | .069 | .113 | .135 | .147 | .104 | .099 | .063 | .040 | .024 | |
| | 2.259 | .000 | .059 | .047 | .099 | .109 | .100 | .085 | .067 | .044 | .029 | .010 | |
| 6° | 1.134 | - .010 | .026 | .017 | .072 | .061 | .061 | .045 | .047 | .028 | .012 | .000 | |
| | 1.259 | .037 | .001 | .013 | .057 | .025 | .034 | .049 | .033 | .015 | .006 | .000 | |
| | 1.384 | - .056 | - .003 | - .001 | - .001 | - .008 | - .007 | - .002 | - .004 | - .001 | - .001 | - .001 | |
| | 1.509 | - .071 | - .064 | - .014 | - .004 | - .004 | - .004 | - .004 | - .027 | - .005 | - .005 | - .028 | |
| | 1.634 | - .015 | - .042 | - .072 | - .071 | - .086 | - .159 | .028 | .045 | .030 | .022 | .037 | |
| | 1.756 | - .319 | .193 | .182 | .151 | .134 | .101 | .079 | .061 | .051 | .042 | .042 | |
| | 1.884 | .272 | .214 | .178 | .150 | .160 | .153 | .130 | .099 | .080 | .064 | .064 | |
| | 2.009 | .172 | .165 | .173 | .169 | .164 | .139 | .108 | .129 | .098 | .078 | .078 | |
| | 2.134 | .086 | .090 | .118 | .152 | .152 | .126 | .135 | .110 | .107 | .100 | .073 | |
| | 2.259 | .101 | .078 | .079 | .110 | .119 | .138 | .114 | .075 | .066 | .055 | .055 | |
| 10° | 1.134 | - .008 | .039 | .046 | .057 | .058 | .064 | .046 | .020 | .015 | .009 | .002 | |
| | 1.259 | - .066 | - .041 | - .013 | - .005 | - .002 | - .002 | - .003 | - .002 | - .003 | - .003 | - .003 | |
| | 1.384 | - .089 | - .067 | - .048 | - .022 | - .008 | - .008 | - .048 | - .005 | - .003 | - .004 | - .004 | |
| | 1.509 | - .025 | - .064 | - .085 | - .111 | - .157 | - .196 | .038 | .047 | .038 | .034 | .034 | |
| | 1.634 | - .442 | .288 | .239 | .184 | .165 | .125 | .098 | .085 | .075 | .059 | .059 | |
| | 1.756 | .360 | .299 | .245 | .184 | .144 | .129 | .141 | .135 | .115 | .091 | .091 | |
| | 1.884 | .159 | .189 | .188 | .189 | .165 | .133 | .113 | .165 | .119 | .092 | .092 | |
| | 2.009 | .038 | .068 | .107 | .119 | .167 | .158 | .127 | .137 | .129 | .097 | .097 | |
| | 2.134 | .057 | .073 | .079 | .086 | .124 | .158 | .134 | .160 | .093 | .078 | .078 | |
| | 2.259 | .043 | .053 | .053 | .073 | .093 | .090 | .124 | .087 | .059 | .055 | .055 | |
| 15° | 1.134 | - .026 | .024 | .013 | .019 | .019 | .019 | .040 | .044 | .024 | .021 | .019 | |
| | 1.259 | - .017 | - .009 | - .006 | - .004 | - .005 | - .005 | - .019 | - .034 | - .026 | - .026 | - .027 | |
| | 1.384 | - .040 | - .004 | - .003 | - .001 | - .001 | - .001 | - .003 | - .003 | - .003 | - .003 | - .003 | |
| | 1.509 | - .090 | - .041 | - .041 | - .045 | - .045 | - .041 | - .025 | - .050 | - .047 | - .044 | - .044 | |
| | 1.634 | - .101 | - .101 | - .114 | - .145 | - .241 | - .241 | - .096 | - .091 | - .078 | - .073 | - .058 | |
| | 1.756 | .110 | .288 | .239 | .184 | .165 | .125 | .098 | .085 | .075 | .061 | .061 | |
| | 1.884 | .344 | .241 | .244 | .158 | .146 | .162 | .151 | .157 | .104 | .081 | .081 | |
| | 2.009 | .045 | .241 | .282 | .282 | .282 | .185 | .154 | .220 | .151 | .120 | .121 | |
| | 2.134 | .037 | .080 | .120 | .178 | .180 | .156 | .186 | .167 | .121 | .105 | .105 | |
| | 2.259 | .038 | .048 | .072 | .079 | .079 | .079 | .081 | .094 | .088 | .088 | .088 | |
| 20° | 1.134 | - .040 | .026 | .013 | .019 | .019 | .019 | .012 | .004 | .011 | .025 | .049 | |
| | 1.259 | - .051 | - .006 | - .006 | - .006 | - .006 | - .006 | - .002 | - .001 | - .001 | - .001 | - .001 | |
| | 1.384 | - .090 | - .059 | - .028 | - .048 | - .048 | - .048 | - .002 | - .002 | - .002 | - .002 | - .002 | |
| | 1.509 | - .110 | - .162 | - .195 | - .187 | - .187 | - .187 | - .096 | - .091 | - .078 | - .073 | - .058 | |
| | 1.634 | - .339 | .160 | .169 | .233 | .185 | .136 | .093 | .093 | .077 | .077 | .077 | |
| | 1.756 | .356 | .303 | .163 | .186 | .186 | .186 | .166 | .166 | .165 | .128 | .128 | |
| | 1.884 | .896 | .896 | .896 | .896 | .896 | .896 | .273 | .197 | .163 | .163 | .163 | |
| | 2.009 | .096 | .177 | .234 | .234 | .207 | .232 | .220 | .197 | .182 | .182 | .182 | |
| | 2.134 | .088 | .141 | .192 | .192 | .171 | .171 | .163 | .163 | .155 | .155 | .155 | |
| | 2.259 | .106 | .104 | .129 | .147 | .151 | .151 | .139 | .139 | .127 | .127 | .127 | |
| 25° | 1.134 | - .071 | .094 | .084 | .103 | .103 | .103 | .109 | .109 | .109 | .111 | .111 | |
| | 1.259 | - .061 | .022 | .106 | .109 | .109 | .109 | .109 | .109 | .109 | .128 | .121 | |
| | 1.384 | - .043 | .017 | .006 | .004 | .004 | .004 | .005 | .005 | .004 | .004 | .004 | |
| | 1.509 | - .078 | .078 | .003 | .007 | .007 | .007 | .003 | .001 | .001 | .003 | .003 | |
| | 1.634 | - .191 | .201 | .007 | .064 | .064 | .064 | .078 | .080 | .080 | .080 | .080 | |
| | 1.756 | .344 | .279 | .293 | .295 | .279 | .279 | .242 | .242 | .242 | .242 | .242 | |
| | 1.884 | .237 | .308 | .280 | .243 | .243 | .243 | .221 | .221 | .221 | .202 | .202 | |
| | 2.009 | .239 | .244 | .254 | .230 | .230 | .230 | .200 | .200 | .200 | .171 | .171 | |
| | 2.134 | .206 | .217 | .235 | .224 | .224 | .224 | .232 | .232 | .232 | .214 | .214 | |
| | 2.259 | .189 | .213 | .219 | .218 | .218 | .218 | .208 | .208 | .208 | .197 | .197 | |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(b) A = 2 triangular wing, r/s = 0.2 - Concluded

| a_B | x/r | δ_w | | | | | | | | | |
|----------------------|-------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 1.34 | 0.03 | .001 | .001 | .000 | .001 | .000 | -.001 | .000 | .000 | .000 | .000 |
| 12.59 | .009 | .010 | .002 | .000 | .002 | .000 | -.003 | -.003 | -.003 | -.003 | -.001 |
| 13.84 | .004 | .007 | .011 | .064 | -.002 | -.003 | -.003 | -.003 | -.003 | -.003 | -.004 |
| 15.09 | .009 | .004 | .001 | .001 | .009 | .172 | .179 | .051 | .045 | .045 | .045 |
| 16.34 | .009 | .004 | .001 | .001 | .009 | .044 | .045 | .021 | .106 | .106 | .106 |
| 0 ^e 17.56 | .009 | .004 | .025 | .025 | .039 | .044 | .045 | .026 | .044 | .044 | .066 |
| 18.84 | .010 | -.005 | -.027 | -.025 | -.035 | -.058 | -.043 | -.026 | -.044 | -.044 | .066 |
| 20.09 | .019 | .003 | .016 | .048 | .074 | .090 | .101 | .090 | .077 | .077 | .058 |
| 21.34 | .009 | .009 | .027 | .038 | .047 | .049 | .080 | .096 | .076 | .088 | .063 |
| 22.59 | -.001 | -.013 | -.034 | -.041 | -.034 | -.039 | -.043 | -.028 | -.059 | -.039 | .039 |
| 23.84 | -.008 | -.014 | -.027 | -.045 | -.034 | -.024 | -.029 | -.010 | -.033 | -.030 | .030 |
| 25.09 | -.005 | -.010 | -.018 | -.026 | -.037 | -.015 | -.006 | -.002 | -.019 | -.001 | .005 |
| 1.34 | .000 | .004 | -.001 | -.001 | .000 | .001 | -.001 | .002 | .001 | -.001 | .001 |
| 12.59 | .006 | .008 | .002 | .003 | .003 | .005 | -.002 | .003 | .003 | .003 | .004 |
| 13.84 | .023 | .012 | .014 | .038 | .001 | .005 | .008 | .003 | .002 | .002 | .004 |
| 16.34 | .036 | .032 | .030 | .016 | .006 | .148 | .349 | .174 | .116 | .089 | .089 |
| 18.84 | .033 | .018 | .003 | .002 | .000 | .001 | .005 | .046 | .144 | .347 | .347 |
| 20.09 | .048 | .028 | .009 | .010 | .023 | .035 | .046 | .065 | .072 | .072 | .077 |
| 21.34 | .038 | .014 | .002 | .004 | .007 | .005 | .018 | .010 | .051 | .051 | .052 |
| 22.59 | .023 | .005 | -.007 | -.015 | .012 | .007 | .008 | .002 | .008 | .008 | .006 |
| 23.84 | -.002 | -.011 | -.008 | -.027 | -.022 | -.016 | -.008 | -.002 | -.003 | -.003 | .015 |
| 25.09 | -.007 | -.013 | -.014 | -.031 | -.034 | -.029 | -.007 | -.003 | -.010 | -.010 | .012 |
| 1.34 | .000 | .001 | -.001 | -.001 | .000 | .001 | -.001 | .002 | .001 | -.001 | .001 |
| 12.59 | .006 | .008 | .002 | .003 | .003 | .005 | -.002 | .003 | .003 | .003 | .004 |
| 13.84 | .023 | .023 | .023 | .036 | .036 | .036 | .005 | .009 | .006 | .006 | .006 |
| 16.34 | .046 | .050 | .042 | .026 | .004 | .130 | .335 | .152 | .086 | .087 | .087 |
| 18.84 | .054 | .036 | .036 | .030 | .025 | .011 | .011 | .010 | .051 | .210 | .269 |
| 20.09 | .071 | .016 | .019 | .008 | .020 | .043 | .059 | .064 | .044 | .002 | .017 |
| 21.34 | .052 | .027 | .011 | .002 | .001 | .025 | .053 | .075 | .082 | .079 | .084 |
| 22.59 | .035 | .014 | .005 | .006 | .001 | .005 | .004 | .003 | .012 | .025 | .025 |
| 23.84 | .011 | -.017 | -.016 | -.009 | -.005 | -.004 | -.004 | -.003 | -.004 | -.011 | .011 |
| 25.09 | .024 | .017 | .005 | .002 | .000 | .005 | .006 | .001 | .009 | .015 | .015 |
| 1.34 | -.001 | -.017 | -.004 | -.002 | -.004 | -.002 | -.002 | -.003 | -.001 | -.001 | .001 |
| 12.59 | .003 | .020 | .008 | .005 | .006 | .006 | .005 | .007 | .006 | .006 | .006 |
| 13.84 | .043 | .050 | .038 | .033 | .007 | .007 | .007 | .007 | .006 | .006 | .006 |
| 15.09 | .052 | .062 | .068 | .048 | .047 | .094 | .338 | .113 | .013 | .013 | .277 |
| 16.34 | .061 | .040 | .043 | .040 | .028 | .013 | .811 | .044 | .160 | .160 | .277 |
| 18.84 | .068 | .043 | .027 | -.007 | .037 | .051 | .084 | .081 | .039 | .039 | .011 |
| 20.09 | .099 | .069 | .036 | .005 | .016 | .056 | .088 | .111 | .107 | .107 | .087 |
| 21.34 | .091 | .066 | .042 | .012 | .004 | .018 | .028 | .068 | .102 | .102 | .107 |
| 22.59 | .079 | .048 | .025 | .007 | .003 | .004 | .003 | .006 | .028 | .028 | .054 |
| 23.84 | .059 | .015 | .006 | .002 | .001 | .001 | .001 | .009 | .015 | .015 | .010 |
| 25.09 | .029 | .007 | -.013 | -.020 | -.022 | -.021 | -.013 | -.008 | -.004 | -.008 | .037 |
| 1.34 | .001 | .017 | .004 | .002 | .003 | .012 | .003 | .005 | .004 | .005 | .005 |
| 12.59 | .003 | .020 | .008 | .005 | .005 | .006 | .005 | .006 | .006 | .006 | .006 |
| 13.84 | .043 | .050 | .038 | .033 | .007 | .007 | .007 | .007 | .006 | .006 | .006 |
| 16.34 | .061 | .040 | .043 | .040 | .028 | .013 | .811 | .044 | .160 | .160 | .277 |
| 18.84 | .068 | .043 | .027 | -.007 | .037 | .051 | .084 | .081 | .039 | .039 | .011 |
| 20.09 | .099 | .069 | .036 | .005 | .016 | .056 | .088 | .111 | .107 | .107 | .087 |
| 21.34 | .091 | .066 | .042 | .012 | .004 | .018 | .028 | .068 | .102 | .102 | .107 |
| 22.59 | .079 | .048 | .025 | .007 | .003 | .004 | .003 | .006 | .028 | .028 | .054 |
| 23.84 | .059 | .015 | .006 | .002 | .001 | .001 | .001 | .009 | .015 | .015 | .010 |
| 25.09 | .027 | .008 | -.013 | -.020 | -.022 | -.021 | -.013 | -.008 | -.004 | -.008 | .037 |
| 1.34 | -.002 | -.003 | -.008 | -.002 | -.004 | -.004 | -.003 | -.005 | -.002 | -.008 | .008 |
| 12.59 | .000 | .032 | .011 | .003 | .005 | .003 | .005 | .006 | .005 | .005 | .011 |
| 13.84 | .067 | .079 | .060 | .040 | .026 | .004 | .005 | .005 | .004 | .004 | .009 |
| 15.09 | .076 | .067 | .067 | .079 | .066 | .066 | .297 | .137 | .004 | .004 | .018 |
| 16.34 | .085 | .068 | .069 | .077 | .067 | .039 | .06 | .043 | .105 | .105 | .195 |
| 18.84 | .081 | .059 | .044 | .004 | .032 | .068 | .093 | .105 | .086 | .086 | .047 |
| 20.09 | .131 | .099 | .057 | .022 | .008 | .031 | .067 | .111 | .135 | .135 | .135 |
| 21.34 | .132 | .099 | .069 | .030 | .010 | .04 | .017 | .042 | .073 | .073 | .016 |
| 22.59 | .119 | .081 | .046 | .022 | .007 | .006 | .009 | .018 | .031 | .031 | .055 |
| 23.84 | .101 | .070 | .036 | .011 | .006 | .018 | .016 | .011 | .003 | .003 | .017 |
| 25.09 | .095 | .070 | .034 | .007 | .002 | .020 | .026 | .034 | .025 | .025 | .005 |
| 1.34 | .098 | .071 | .034 | .009 | .002 | .011 | .014 | .013 | .014 | .014 | .039 |
| 12.59 | .004 | .005 | .005 | .006 | .005 | .006 | .005 | .006 | .005 | .005 | .003 |
| 13.84 | .088 | .112 | .079 | .037 | .007 | .007 | .007 | .007 | .008 | .008 | .005 |
| 15.09 | .103 | .146 | .101 | .079 | .019 | .004 | .004 | .002 | .004 | .004 | .001 |
| 16.34 | .120 | .100 | .093 | .181 | .098 | .093 | .132 | .162 | .005 | .005 | .009 |
| 18.84 | .109 | .088 | .061 | .015 | .012 | .004 | .080 | .093 | .134 | .134 | .039 |
| 20.09 | .181 | .127 | .086 | .034 | .017 | .008 | .035 | .037 | .100 | .100 | .137 |
| 21.34 | .165 | .115 | .062 | .021 | .006 | .011 | .023 | .026 | .040 | .040 | .060 |
| 22.59 | .132 | .093 | .045 | .020 | .008 | .007 | .016 | .014 | .019 | .019 | .037 |
| 23.84 | .167 | .114 | .065 | .086 | .016 | .004 | .004 | .004 | .003 | .003 | .022 |
| 25.09 | 157 | .104 | .060 | .036 | .022 | .008 | .005 | .006 | .005 | .005 | .004 |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(c) A = 1 triangular wing, $r/s = 0.2$

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(c) $A = 1$ triangular wing, $r/s = 0.2$ - Concluded

| a_b | x/r | δ_w | | | | | | | | | |
|-------|-------|------------|------|-------|------|------|------|------|-------|------|------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 0° | 69.4 | .002 | .001 | .001 | | .001 | .001 | .001 | .001 | .001 | .001 |
| | 83.7 | .002 | .017 | .003 | | .001 | .001 | .002 | .001 | .001 | .001 |
| | 98.1 | -.003 | .011 | .044 | | .001 | .001 | .001 | .001 | .001 | .001 |
| | 112.6 | -.020 | .022 | .037 | | .034 | - | .003 | -.113 | .088 | .114 |
| | 141.2 | -.012 | .031 | -.027 | | | | | | | |
| | 155.6 | -.014 | .037 | -.024 | | | | | | | |
| | 170.0 | -.016 | .035 | -.028 | | | | | | | |
| | 184.4 | -.016 | .035 | -.025 | | | | | | | |
| | 198.8 | -.015 | .035 | -.026 | | | | | | | |
| | 213.1 | -.011 | .036 | -.025 | | | | | | | |
| 3° | 69.4 | .004 | .002 | .003 | | .002 | | .002 | .002 | .002 | .002 |
| | 83.7 | .005 | .014 | .003 | | .002 | | .003 | .003 | .003 | .003 |
| | 98.1 | .011 | .024 | .004 | | .001 | | .001 | .001 | .001 | .001 |
| | 112.6 | .016 | .020 | .005 | | .011 | | .003 | .032 | | |
| | 141.2 | .014 | .021 | .006 | | .012 | | .006 | .436 | | |
| | 155.6 | .018 | .025 | .007 | | .017 | | .007 | .149 | | |
| | 170.0 | .011 | .028 | .008 | | .021 | | .009 | .001 | | |
| | 184.4 | .018 | .025 | .008 | | .021 | | .009 | .001 | | |
| | 198.8 | .015 | .025 | .008 | | .021 | | .009 | .001 | | |
| | 213.1 | .011 | .025 | .008 | | .021 | | .009 | .001 | | |
| 6° | 69.4 | .003 | .001 | .004 | | .001 | | .001 | .001 | .001 | .001 |
| | 83.7 | .005 | .008 | .037 | | .008 | | .008 | .008 | .008 | .008 |
| | 98.1 | .011 | .015 | .033 | | .011 | | .011 | .011 | .011 | .011 |
| | 112.6 | .015 | .018 | .030 | | .015 | | .015 | .015 | .015 | .015 |
| | 141.2 | .017 | .020 | .037 | | .017 | | .017 | .017 | .017 | .017 |
| | 155.6 | .020 | .023 | .040 | | .020 | | .020 | .020 | .020 | .020 |
| | 170.0 | .011 | .015 | .041 | | .011 | | .011 | .011 | .011 | .011 |
| | 184.4 | .011 | .016 | .000 | | .012 | | .012 | .012 | .012 | .012 |
| | 198.8 | .011 | .016 | .000 | | .012 | | .012 | .012 | .012 | .012 |
| | 213.1 | .011 | .016 | .000 | | .012 | | .012 | .012 | .012 | .012 |
| 10° | 69.4 | .003 | .001 | .001 | | .001 | | .001 | .001 | .001 | .001 |
| | 83.7 | .005 | .001 | .001 | | .001 | | .001 | .001 | .001 | .001 |
| | 98.1 | .016 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 112.6 | .015 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 141.2 | .019 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 155.6 | .024 | .025 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 170.0 | .011 | .020 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 184.4 | .011 | .020 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 198.8 | .011 | .020 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 213.1 | .011 | .020 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| 15° | 69.4 | .003 | .001 | .001 | | .001 | | .001 | .001 | .001 | .001 |
| | 83.7 | .005 | .001 | .001 | | .001 | | .001 | .001 | .001 | .001 |
| | 98.1 | .016 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 112.6 | .016 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 141.2 | .021 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 155.6 | .026 | .028 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 170.0 | .011 | .021 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 184.4 | .011 | .021 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 198.8 | .011 | .021 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| | 213.1 | .011 | .021 | .005 | | .005 | | .005 | .005 | .005 | .005 |
| 20° | 69.4 | .003 | .001 | .001 | | .001 | | .001 | .001 | .001 | .001 |
| | 83.7 | .005 | .001 | .001 | | .001 | | .001 | .001 | .001 | .001 |
| | 98.1 | .016 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 112.6 | .013 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 141.2 | .013 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 155.6 | .019 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 170.0 | .011 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 184.4 | .011 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 198.8 | .011 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| | 213.1 | .011 | .021 | .000 | | .000 | | .000 | .000 | .000 | .000 |
| 25° | 69.4 | .002 | .000 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 83.7 | .005 | .008 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 98.1 | .013 | .075 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 112.6 | .018 | .077 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 141.2 | .015 | .077 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 155.6 | .017 | .077 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 170.0 | .014 | .060 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 184.4 | .014 | .060 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 198.8 | .014 | .060 | .008 | | .001 | | .001 | .001 | .001 | .001 |
| | 213.1 | .014 | .060 | .008 | | .001 | | .001 | .001 | .001 | .001 |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(d) $A = 1$ triangular wing, $r/s = 0.4$

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(d) $A = 1$ triangular wing, $r/s = 0.4$ - Concluded

| a_B | x/r | δ_w | | | | | | | | | |
|-------|-------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 0° | 6.94 | .002 | .000 | .000 | .001 | .000 | .001 | .002 | .001 | .001 | .001 |
| | 8.37 | -.003 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 9.81 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 11.25 | -.002 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 12.69 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 14.12 | -.001 | -.000 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 15.56 | -.003 | -.001 | -.001 | -.001 | -.001 | -.001 | -.002 | -.002 | -.001 | -.000 |
| | 17.00 | -.016 | -.027 | -.044 | -.074 | -.11 | -.16 | -.21 | -.27 | -.33 | -.40 |
| | 18.44 | -.015 | -.023 | -.040 | -.074 | -.11 | -.16 | -.21 | -.27 | -.33 | -.40 |
| | 19.87 | -.018 | -.026 | -.045 | -.076 | -.11 | -.16 | -.21 | -.27 | -.33 | -.40 |
| 3° | 8.131 | -.016 | -.026 | -.045 | -.074 | -.11 | -.16 | -.21 | -.27 | -.33 | -.40 |
| | 8.275 | -.008 | -.016 | -.030 | -.050 | -.073 | -.095 | -.117 | -.137 | -.155 | -.175 |
| | 8.419 | -.001 | -.005 | -.014 | -.024 | -.038 | -.052 | -.067 | -.081 | -.096 | -.112 |
| | 8.562 | .003 | .003 | .006 | .014 | .017 | .019 | .027 | .037 | .047 | .052 |
| | 6.94 | .000 | .001 | .001 | .001 | .000 | .000 | .001 | .000 | .000 | .001 |
| | 8.37 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 9.81 | -.001 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 11.25 | -.001 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 12.69 | -.001 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 14.12 | -.001 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| 6° | 15.56 | -.002 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 17.00 | -.002 | -.003 | -.009 | -.014 | -.019 | -.024 | -.029 | -.034 | -.039 | -.044 |
| | 18.44 | -.003 | -.004 | -.014 | -.024 | -.031 | -.037 | -.043 | -.049 | -.055 | -.060 |
| | 19.87 | -.004 | -.005 | -.017 | -.027 | -.035 | -.042 | -.049 | -.056 | -.063 | -.068 |
| | 21.31 | -.005 | -.006 | -.017 | -.027 | -.035 | -.042 | -.049 | -.056 | -.063 | -.068 |
| | 22.75 | -.005 | -.006 | -.017 | -.027 | -.035 | -.042 | -.049 | -.056 | -.063 | -.068 |
| | 24.19 | -.007 | -.010 | -.020 | -.030 | -.038 | -.045 | -.052 | -.059 | -.066 | -.072 |
| | 25.62 | -.004 | -.006 | -.014 | -.024 | -.032 | -.038 | -.045 | -.052 | -.059 | -.066 |
| | 6.94 | .000 | .000 | .001 | .001 | .000 | .000 | .001 | .000 | .000 | .001 |
| | 8.37 | -.001 | -.003 | -.008 | -.012 | -.017 | -.022 | -.027 | -.032 | -.037 | -.042 |
| 10° | 9.81 | -.001 | -.003 | -.008 | -.012 | -.017 | -.022 | -.027 | -.032 | -.037 | -.042 |
| | 11.25 | -.002 | -.003 | -.008 | -.012 | -.017 | -.022 | -.027 | -.032 | -.037 | -.042 |
| | 12.69 | -.006 | -.005 | -.016 | -.026 | -.034 | -.044 | -.054 | -.064 | -.074 | -.084 |
| | 14.12 | -.004 | -.004 | -.016 | -.026 | -.034 | -.044 | -.054 | -.064 | -.074 | -.084 |
| | 15.56 | -.017 | -.015 | -.027 | -.037 | -.045 | -.055 | -.065 | -.075 | -.085 | -.095 |
| | 17.00 | -.024 | -.022 | -.034 | -.044 | -.052 | -.062 | -.072 | -.082 | -.092 | -.102 |
| | 18.44 | -.030 | -.027 | -.039 | -.049 | -.057 | -.067 | -.077 | -.087 | -.097 | -.107 |
| | 19.87 | -.037 | -.034 | -.046 | -.056 | -.064 | -.074 | -.084 | -.094 | -.104 | -.114 |
| | 21.31 | -.043 | -.040 | -.052 | -.062 | -.070 | -.080 | -.090 | -.100 | -.110 | -.120 |
| | 22.75 | -.050 | -.047 | -.058 | -.068 | -.076 | -.086 | -.096 | -.106 | -.116 | -.126 |
| 15° | 24.19 | -.012 | -.013 | -.022 | -.032 | -.042 | -.052 | -.062 | -.072 | -.082 | -.092 |
| | 25.62 | -.008 | -.009 | -.018 | -.028 | -.038 | -.048 | -.058 | -.068 | -.078 | -.088 |
| | 6.94 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
| | 8.37 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 9.81 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 11.25 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 12.69 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 14.12 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 15.56 | -.000 | -.001 | -.001 | -.001 | -.000 | -.000 | -.001 | -.001 | -.000 | -.000 |
| | 17.00 | -.023 | -.025 | -.035 | -.045 | -.055 | -.065 | -.075 | -.085 | -.095 | -.105 |
| 20° | 18.44 | -.029 | -.031 | -.041 | -.051 | -.061 | -.071 | -.081 | -.091 | -.101 | -.111 |
| | 19.87 | -.037 | -.039 | -.049 | -.059 | -.069 | -.079 | -.089 | -.099 | -.109 | -.119 |
| | 21.31 | -.046 | -.047 | -.057 | -.067 | -.077 | -.087 | -.097 | -.107 | -.117 | -.127 |
| | 22.75 | -.054 | -.055 | -.065 | -.075 | -.085 | -.095 | -.105 | -.115 | -.125 | -.135 |
| | 24.19 | -.062 | -.063 | -.073 | -.083 | -.093 | -.103 | -.113 | -.123 | -.133 | -.143 |
| | 25.62 | -.070 | -.071 | -.081 | -.091 | -.101 | -.111 | -.121 | -.131 | -.141 | -.151 |
| | 6.94 | -.001 | -.002 | -.005 | -.006 | -.009 | -.012 | -.015 | -.018 | -.021 | -.024 |
| | 8.37 | -.006 | -.004 | -.003 | -.005 | -.008 | -.010 | -.013 | -.016 | -.019 | -.022 |
| | 9.81 | -.004 | -.003 | -.002 | -.004 | -.007 | -.009 | -.012 | -.015 | -.018 | -.021 |
| | 11.25 | -.002 | -.001 | -.001 | -.002 | -.005 | -.007 | -.010 | -.013 | -.016 | -.019 |
| 25° | 12.69 | -.001 | -.001 | -.001 | -.001 | -.004 | -.006 | -.009 | -.012 | -.015 | -.018 |
| | 14.12 | -.002 | -.001 | -.001 | -.001 | -.004 | -.006 | -.009 | -.012 | -.015 | -.018 |
| | 15.56 | -.002 | -.001 | -.001 | -.001 | -.004 | -.006 | -.009 | -.012 | -.015 | -.018 |
| | 17.00 | -.064 | -.067 | -.074 | -.081 | -.088 | -.095 | -.102 | -.109 | -.116 | -.123 |
| | 18.44 | -.074 | -.076 | -.083 | -.090 | -.097 | -.104 | -.111 | -.118 | -.125 | -.132 |
| | 19.87 | -.083 | -.085 | -.092 | -.099 | -.106 | -.113 | -.120 | -.127 | -.134 | -.141 |
| | 21.31 | -.092 | -.094 | -.101 | -.108 | -.115 | -.122 | -.129 | -.136 | -.143 | -.150 |
| | 22.75 | -.101 | -.103 | -.110 | -.117 | -.124 | -.131 | -.138 | -.145 | -.152 | -.160 |
| | 24.19 | -.109 | -.111 | -.118 | -.125 | -.132 | -.139 | -.146 | -.153 | -.160 | -.168 |
| | 25.62 | -.118 | -.120 | -.127 | -.134 | -.141 | -.148 | -.155 | -.162 | -.170 | -.178 |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE
WINGS - Continued

(e) $A = 2/3$ triangular wing, $r/s = 0.4$

| x/r | $\delta_w, \alpha_B = 0^\circ$ | | | | | | | | | | | | $\alpha_B, \delta_w = 0^\circ$ | | | | | | |
|-------|--------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------------------------------|--------|--------|--------|--------|--------|--|
| | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | |
| 6.94 | .005 | .006 | .004 | .003 | .004 | .003 | .004 | .003 | .003 | .000 | .003 | .004 | .000 | .007 | .006 | .003 | .006 | .006 | |
| 8.37 | - .001 | - .000 | - .001 | - .001 | - .000 | - .001 | - .001 | - .001 | - .002 | - .000 | - .006 | - .006 | - .005 | - .002 | - .003 | - .003 | - .003 | - .003 | |
| 9.81 | - .007 | - .003 | - .004 | - .005 | - .005 | - .001 | - .005 | - .004 | - .003 | - .001 | - .003 | - .001 | - .001 | - .002 | - .000 | - .000 | - .000 | - .000 | |
| 11.25 | - .004 | - .002 | - .003 | - .003 | - .002 | - .001 | - .003 | - .002 | - .001 | - .003 | - .000 | - .006 | - .004 | - .000 | - .000 | - .002 | - .004 | - .004 | |
| 12.69 | .001 | .002 | .002 | .001 | .001 | .001 | .000 | .000 | .016 | .000 | .004 | .000 | .011 | .007 | .006 | .004 | .005 | .009 | |
| 14.12 | .000 | .000 | .000 | .000 | .000 | .000 | .017 | .017 | .002 | .000 | .011 | .024 | .032 | .039 | .044 | .056 | .068 | .079 | |
| 15.56 | .017 | - .083 | - .251 | - .348 | - .180 | - .030 | .051 | .032 | .016 | .007 | .000 | .016 | .032 | .047 | .053 | .065 | .080 | .102 | |
| 17.00 | .020 | .017 | .010 | .029 | .039 | .084 | .073 | .047 | .024 | .009 | .000 | .019 | .039 | .057 | .065 | .080 | .102 | .123 | |
| 18.44 | .076 | .067 | .074 | .086 | .090 | .060 | .060 | .045 | .044 | .006 | - .005 | .019 | .042 | .063 | .073 | .093 | .123 | .183 | |
| 19.87 | .068 | .070 | .068 | .068 | .061 | .057 | .031 | .031 | .025 | .008 | .005 | .018 | .047 | .061 | .086 | .107 | .133 | .133 | |
| 21.31 | .039 | .047 | .029 | .086 | .086 | .086 | .087 | .031 | .020 | .017 | .000 | .015 | .036 | .054 | .069 | .096 | .117 | .117 | |
| 22.75 | .028 | .033 | .017 | .011 | .013 | .018 | .020 | .017 | .014 | .001 | - .003 | .008 | .017 | .036 | .054 | .087 | .109 | .109 | |
| 24.19 | .000 | .000 | - .008 | - .005 | - .007 | - .006 | .016 | .008 | .007 | .002 | - .001 | .001 | .003 | .019 | .080 | .060 | - .087 | - .090 | |
| 25.62 | - .030 | - .083 | - .011 | .010 | .020 | .023 | - .005 | - .002 | .006 | .006 | - .009 | - .003 | - .043 | .037 | .050 | - .050 | - .090 | - .090 | |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE
WINGS - Continued

(f) $A = 3/8$ triangular wing, $r/s = 0.4$

| x/r | $\delta_w, \alpha_B = 0^\circ$ | | | | | | | | | | | | $\alpha_B, \delta_w = 0^\circ$ | | | | | | |
|-------|--------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------------------------------|------|------|------|------|------|--|
| | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | |
| 6.94 | .004 | .002 | - .015 | .001 | .001 | .000 | .001 | .001 | .000 | - .002 | .002 | .000 | .000 | .000 | .000 | .000 | .000 | .003 | |
| 8.37 | .001 | - .002 | - .016 | - .001 | - .001 | .012 | .000 | - .001 | - .002 | - .002 | .005 | .001 | .001 | .001 | .001 | .001 | .000 | .000 | |
| 9.81 | - .001 | - .001 | - .020 | - .004 | - .003 | - .005 | - .003 | - .011 | - .012 | - .001 | - .002 | .005 | .009 | .019 | .031 | .046 | .060 | .080 | |
| 11.25 | - .000 | - .001 | - .018 | - .001 | - .001 | - .001 | - .002 | - .000 | - .003 | - .002 | - .002 | .003 | .009 | .017 | .037 | .046 | .060 | .080 | |
| 12.69 | .003 | .000 | - .015 | - .044 | - .000 | - .037 | - .086 | .009 | .013 | - .004 | - .000 | .001 | .030 | .032 | .049 | .064 | .077 | .090 | |
| 14.12 | - .052 | - .095 | - .132 | - .206 | - .289 | - .557 | .013 | .044 | .014 | - .005 | - .000 | .015 | .031 | .053 | .075 | .086 | .104 | .104 | |
| 15.56 | - .054 | - .054 | - .059 | - .004 | - .001 | .046 | .074 | .056 | .020 | - .008 | - .007 | - .006 | .017 | .038 | .061 | .080 | .109 | .126 | |
| 17.00 | - .046 | - .065 | - .149 | .063 | .063 | .078 | .084 | .069 | .048 | .021 | - .006 | - .015 | .038 | .064 | .088 | .104 | .157 | .157 | |
| 18.44 | .060 | .060 | .088 | .038 | .071 | .034 | .058 | .026 | .020 | - .004 | - .006 | - .015 | .038 | .068 | .096 | .127 | .159 | .159 | |
| 19.87 | .060 | .060 | .084 | .038 | .071 | .034 | .058 | .026 | .020 | - .004 | - .006 | - .016 | .039 | .068 | .096 | .126 | .158 | .158 | |
| 21.31 | .000 | .000 | - .006 | .006 | .013 | .009 | .032 | .010 | .011 | - .001 | - .001 | .014 | .040 | .078 | .095 | .126 | .157 | .157 | |
| 22.75 | .000 | .000 | - .038 | - .016 | - .014 | - .010 | - .007 | - .005 | - .003 | - .005 | - .005 | .014 | .038 | .076 | .094 | .126 | .158 | .158 | |
| 24.19 | - .014 | - .004 | - .038 | - .086 | - .035 | - .030 | - .088 | - .007 | - .004 | - .003 | - .005 | .001 | - .005 | .039 | .051 | .109 | .168 | .168 | |
| 25.62 | - .021 | - .020 | - .048 | - .071 | - .036 | - .023 | - .011 | .001 | .007 | - .005 | - .005 | - .001 | - .005 | .067 | .084 | .131 | | | |

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TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(g) $A = 3$ rectangular wing, $r/s = 0.2$

| α_B | x/r | δ_w | | | | | | | | | | | |
|------------|-------|------------|------|------|------|------|------|------|------|------|------|------|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | |
| 0° | 6.94 | .008 | .001 | .001 | .001 | .000 | .000 | .001 | .000 | .001 | .002 | .001 | |
| | 8.37 | b001 | b002 | b000 | b000 | - | .001 | b000 | b000 | b000 | b001 | b000 | |
| | 9.81 | b000 | .001 | b000 | b000 | - | .001 | b000 | b000 | b000 | b001 | b000 | |
| | 11.25 | b000 | b001 | b000 | b000 | - | .001 | b000 | b000 | b000 | b001 | b000 | |
| | 12.69 | b001 | .001 | b001 | b000 | - | .001 | b001 | b001 | b001 | b001 | b000 | |
| | 14.12 | b119 | b005 | b005 | b000 | - | .004 | b000 | b002 | b001 | b001 | b000 | |
| | 15.56 | b599 | b005 | b005 | b000 | - | .006 | b004 | b001 | b004 | b002 | b001 | |
| | 16.99 | b119 | b119 | b005 | b000 | - | .003 | b003 | b001 | b003 | b002 | b001 | |
| | 18.44 | b592 | b119 | b004 | b000 | - | .003 | b003 | b001 | b004 | b002 | b001 | |
| | 19.87 | b075 | b564 | b088 | b084 | - | .001 | b001 | b001 | b001 | b001 | b000 | |
| | 21.31 | b57 | b558 | b50 | b65 | - | .008 | b008 | b007 | b017 | b04 | b04 | |
| 3° | 22.75 | b30 | b584 | b119 | b42 | - | .001 | b001 | b003 | b008 | b008 | b005 | |
| | 24.19 | b003 | - | b006 | - | - | .000 | b000 | b001 | b014 | b006 | b005 | |
| | 25.62 | b116 | - | b003 | - | - | .000 | b001 | b015 | b10 | b005 | b005 | |
| | 6.94 | .002 | .003 | .003 | .004 | .002 | .004 | .003 | .003 | .003 | .004 | .004 | |
| | 8.37 | b001 | b001 | .003 | .003 | b001 | .003 | b001 | b002 | b002 | b002 | b001 | |
| | 9.81 | b000 | b001 | b002 | b002 | - | .003 | b001 | b000 | b000 | b000 | b000 | |
| | 11.25 | b001 | b001 | b001 | b001 | - | .001 | b001 | b000 | b007 | b006 | b007 | |
| | 12.69 | b006 | b006 | b006 | b006 | - | .007 | b006 | b006 | b007 | b006 | b007 | |
| | 14.12 | b001 | b001 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b000 | |
| | 15.56 | b108 | b103 | b13 | b000 | - | .000 | b000 | b001 | b016 | b000 | b000 | |
| | 17.00 | b124 | b118 | b67 | b000 | - | .000 | b000 | b001 | b016 | b000 | b000 | |
| | 18.44 | b556 | b44 | b000 | b000 | - | .000 | b000 | b001 | b016 | b000 | b000 | |
| | 19.87 | b172 | b172 | b172 | b172 | - | .000 | b000 | b001 | b016 | b000 | b000 | |
| | 21.31 | b071 | b084 | b099 | b06 | - | .006 | b076 | b063 | b043 | b031 | b028 | |
| 6° | 22.75 | b16 | b305 | b051 | b055 | - | .005 | b054 | b049 | b032 | b021 | b016 | |
| | 24.19 | b001 | b003 | b012 | b004 | - | .000 | b022 | b013 | b008 | b006 | b001 | |
| | 25.62 | b004 | - | b003 | - | - | .000 | b004 | b013 | b008 | b006 | b001 | |
| | 6.94 | .003 | .003 | .000 | .000 | - | .000 | .000 | .000 | .000 | .000 | .003 | |
| | 8.37 | b000 | b000 | b000 | b000 | - | .001 | b001 | b001 | b001 | b001 | b004 | |
| | 9.81 | b000 | b000 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b005 | |
| | 11.25 | b000 | b006 | b006 | b006 | - | .006 | b005 | b005 | b005 | b005 | b000 | |
| | 12.69 | b006 | b006 | b006 | b006 | - | .006 | b006 | b006 | b006 | b006 | b000 | |
| | 14.12 | b561 | b67 | b019 | b019 | - | .019 | b001 | b001 | b019 | b107 | b007 | |
| | 15.56 | b172 | b24 | b094 | b082 | - | .000 | b001 | b001 | b019 | b107 | b007 | |
| | 17.00 | b256 | b44 | b182 | b182 | - | .000 | b000 | b001 | b068 | b147 | b048 | |
| 10° | 18.44 | b172 | b172 | b172 | b172 | - | .000 | b000 | b001 | b068 | b147 | b048 | |
| | 19.87 | b099 | b099 | b099 | b099 | - | .000 | b000 | b001 | b068 | b147 | b048 | |
| | 21.31 | b011 | b011 | b011 | b011 | - | .000 | b000 | b001 | b068 | b147 | b048 | |
| | 22.75 | b004 | - | b003 | - | - | .000 | b004 | b023 | b117 | b003 | b000 | |
| | 24.19 | b001 | - | b001 | - | - | .000 | b001 | b023 | b117 | b003 | b000 | |
| | 25.62 | b004 | - | b003 | - | - | .000 | b004 | b023 | b117 | b003 | b000 | |
| | 6.94 | .000 | .001 | .001 | .001 | - | .001 | .001 | .002 | .002 | .005 | .005 | |
| | 8.37 | b000 | b000 | b000 | b000 | - | .001 | b001 | b002 | b002 | b002 | b002 | |
| | 9.81 | b001 | b003 | b003 | b003 | - | .001 | b001 | b004 | b004 | b004 | b004 | |
| | 11.25 | b000 | b000 | b000 | b000 | - | .000 | b000 | b003 | b003 | b003 | b003 | |
| | 12.69 | b000 | b000 | b000 | b000 | - | .000 | b000 | b003 | b003 | b003 | b003 | |
| 15° | 14.12 | b399 | b008 | b008 | b008 | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 15.56 | b172 | b172 | b172 | b172 | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 17.00 | b28 | b173 | b105 | b07 | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 18.44 | b171 | b179 | b179 | b179 | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 19.87 | b089 | b090 | b086 | b086 | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 21.31 | b027 | b057 | b086 | b086 | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 22.75 | b001 | b001 | b001 | b001 | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 24.19 | b001 | - | b001 | - | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 25.62 | b005 | - | b005 | - | - | .008 | b008 | b008 | b008 | b008 | b008 | |
| | 6.94 | .001 | .000 | .000 | .000 | - | .000 | .000 | .000 | .000 | .000 | .000 | |
| | 8.37 | b001 | b001 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b001 | |
| 20° | 9.81 | b001 | b001 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b001 | |
| | 11.25 | b001 | b001 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b001 | |
| | 12.69 | b001 | b001 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b001 | |
| | 14.12 | b006 | b006 | b006 | b006 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 15.56 | b006 | b006 | b006 | b006 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 17.00 | b006 | b006 | b006 | b006 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 18.44 | b230 | b230 | b230 | b230 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 19.87 | b255 | b255 | b255 | b255 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 21.31 | b117 | b117 | b117 | b117 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 22.75 | b126 | b126 | b126 | b126 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| 25° | 24.19 | b064 | b097 | b097 | b111 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 25.62 | b001 | b001 | b001 | b001 | - | .001 | b006 | b006 | b006 | b006 | b006 | |
| | 6.94 | .001 | .012 | .001 | .001 | - | .003 | .003 | .004 | .004 | .004 | .004 | |
| | 8.37 | b001 | b001 | b001 | b001 | - | .002 | b001 | b001 | b001 | b001 | b001 | |
| | 9.81 | b001 | b001 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b001 | |
| | 11.25 | b001 | b001 | b001 | b001 | - | .001 | b001 | b001 | b001 | b001 | b001 | |
| | 12.69 | b005 | b005 | b005 | b005 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 14.12 | b005 | b005 | b005 | b005 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 15.56 | b005 | b005 | b005 | b005 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 17.00 | b005 | b005 | b005 | b005 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 18.44 | b372 | b372 | b372 | b372 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 19.87 | b372 | b372 | b372 | b372 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 21.31 | b372 | b372 | b372 | b372 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 22.75 | b372 | b372 | b372 | b372 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 24.19 | b372 | b372 | b372 | b372 | - | .001 | b005 | b005 | b005 | b005 | b005 | |
| | 25.62 | b372 | b372 | b372 | b372 | - | .001 | b005 | b005 | b005 | b005 | b005 | |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(g) $A = 3$ rectangular wing, $r/s = 0.2$ - Concluded

| α_B | x/r | | δ_w | | | | | | | | | |
|------------|-------|------|------------|------|------|------|------|------|------|------|------|------|
| | | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 0° | 6.94 | .001 | .002 | .000 | .001 | .000 | .002 | .003 | .002 | .001 | .001 | .001 |
| | 8.37 | .000 | .001 | .000 | .000 | .000 | .000 | .001 | .001 | .000 | .000 | .001 |
| | 9.81 | .000 | .001 | .000 | .000 | .000 | .000 | .000 | .001 | .001 | .000 | .000 |
| | 11.25 | .001 | .001 | .000 | .001 | .000 | .000 | .000 | .001 | .001 | .000 | .000 |
| | 12.69 | .001 | .001 | .000 | .001 | .000 | .000 | .000 | .001 | .001 | .000 | .000 |
| | 14.12 | .002 | .002 | .000 | .001 | .000 | .001 | .002 | .002 | .001 | .001 | .000 |
| | 15.56 | .003 | .002 | .000 | .001 | .000 | .001 | .002 | .002 | .001 | .001 | .000 |
| | 17.00 | - | .002 | .001 | .000 | .001 | .000 | .001 | .001 | .001 | .001 | .000 |
| | 18.44 | - | .002 | .001 | .000 | .001 | .000 | .001 | .001 | .001 | .001 | .000 |
| | 19.87 | - | .003 | .002 | .000 | .001 | .000 | .001 | .001 | .001 | .001 | .000 |
| | 21.31 | - | .003 | .002 | .000 | .001 | .000 | .001 | .001 | .001 | .001 | .000 |
| | 22.75 | - | .010 | .008 | .000 | .004 | .000 | .005 | .004 | .005 | .004 | .003 |
| | 24.19 | - | .015 | .013 | .000 | .006 | .000 | .007 | .006 | .007 | .006 | .005 |
| | 25.62 | .001 | .003 | .000 | .002 | .000 | .001 | .002 | .001 | .002 | .001 | .000 |
| 3° | 6.94 | .002 | .003 | .000 | .001 | .000 | .003 | .002 | .002 | .003 | .003 | .002 |
| | 8.37 | .001 | .001 | .000 | .001 | .000 | .001 | .002 | .002 | .003 | .003 | .002 |
| | 9.81 | .001 | .001 | .000 | .001 | .000 | .001 | .001 | .001 | .001 | .001 | .000 |
| | 11.25 | .001 | .001 | .000 | .001 | .000 | .001 | .001 | .001 | .001 | .001 | .000 |
| | 12.69 | .006 | .007 | .000 | .005 | .000 | .006 | .006 | .006 | .004 | .004 | .003 |
| | 14.12 | .000 | .008 | .000 | .006 | .000 | .000 | .000 | .000 | .001 | .000 | .000 |
| | 15.56 | .000 | .009 | .000 | .007 | .000 | .000 | .000 | .000 | .001 | .000 | .000 |
| | 17.00 | .002 | .001 | .000 | .029 | .000 | .045 | .061 | .078 | .141 | .141 | .141 |
| | 18.44 | .007 | .001 | .000 | .043 | .000 | .052 | .063 | .074 | .134 | .134 | .134 |
| | 19.87 | .007 | .001 | .000 | .032 | .000 | .044 | .053 | .064 | .131 | .131 | .131 |
| | 21.31 | .003 | .001 | .000 | .021 | .000 | .033 | .043 | .054 | .131 | .131 | .131 |
| | 22.75 | .002 | .001 | .000 | .017 | .000 | .021 | .031 | .041 | .131 | .131 | .131 |
| | 24.19 | .002 | .001 | .000 | .018 | .000 | .021 | .031 | .041 | .131 | .131 | .131 |
| | 25.62 | .002 | .001 | .000 | .018 | .000 | .021 | .031 | .041 | .131 | .131 | .131 |
| 6° | 6.94 | .000 | .000 | .000 | .000 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 8.37 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 9.81 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 11.25 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 12.69 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 14.12 | .000 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 15.56 | .000 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 17.00 | .001 | .001 | .000 | .007 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 18.44 | .019 | .017 | .000 | .017 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 19.87 | .011 | .014 | .000 | .014 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 21.31 | .008 | .009 | .000 | .009 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 22.75 | .007 | .008 | .000 | .008 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 24.19 | .006 | .007 | .000 | .007 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 25.62 | .003 | .004 | .000 | .004 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| 10° | 6.94 | .001 | .000 | .004 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 8.37 | .000 | .000 | .002 | .002 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 9.81 | .000 | .000 | .001 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 11.25 | .000 | .000 | .001 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 12.69 | .000 | .000 | .001 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 14.12 | .002 | .002 | .000 | .002 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 15.56 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 17.00 | .016 | .013 | .004 | .005 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 18.44 | .041 | .041 | .014 | .004 | .004 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 19.87 | .042 | .036 | .017 | .007 | .007 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 21.31 | .037 | .036 | .014 | .006 | .006 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 22.75 | .034 | .036 | .017 | .006 | .005 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 24.19 | .036 | .036 | .017 | .006 | .006 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 25.62 | .033 | .031 | .017 | .006 | .006 | b00 | b00 | b00 | b00 | b00 | b00 |
| 15° | 6.94 | .001 | .001 | .000 | .000 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 8.37 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 9.81 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 11.25 | .000 | .000 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 12.69 | .000 | .000 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 14.12 | .002 | .002 | .000 | .002 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 15.56 | .001 | .001 | .000 | .001 | .000 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 17.00 | .006 | .006 | .004 | .005 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 18.44 | .015 | .013 | .007 | .008 | .005 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 19.87 | .031 | .028 | .017 | .008 | .007 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 21.31 | .057 | .042 | .028 | .011 | .006 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 22.75 | .054 | .041 | .028 | .011 | .006 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 24.19 | .048 | .036 | .017 | .005 | .006 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 25.62 | .058 | .041 | .017 | .002 | .002 | b00 | b00 | b00 | b00 | b00 | b00 |
| 20° | 6.94 | .003 | .003 | .003 | .003 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 8.37 | .002 | .003 | .003 | .003 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 9.81 | .004 | .003 | .003 | .003 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 11.25 | .004 | .003 | .003 | .003 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 12.69 | .002 | .003 | .003 | .003 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 14.12 | .001 | .001 | .001 | .001 | .001 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 15.56 | .003 | .002 | .001 | .001 | .001 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 17.00 | .024 | .023 | .016 | .024 | .011 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 18.44 | .051 | .041 | .024 | .024 | .011 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 19.87 | .079 | .048 | .018 | .018 | .009 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 21.31 | .064 | .063 | .020 | .023 | .010 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 22.75 | .075 | .068 | .023 | .027 | .011 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 24.19 | .040 | .076 | .021 | .011 | .009 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 25.62 | .068 | .088 | .043 | .028 | .011 | b00 | b00 | b00 | b00 | b00 | b00 |
| 25° | 6.94 | .005 | .001 | .006 | .002 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 8.37 | .005 | .001 | .006 | .003 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 9.81 | .005 | .001 | .006 | .003 | .003 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 11.25 | .005 | .003 | .006 | .001 | .002 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 12.69 | .003 | .006 | .001 | .005 | .007 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 14.12 | .003 | .003 | .001 | .002 | .002 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 15.56 | .005 | .001 | .001 | .004 | .004 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 17.00 | .026 | .025 | .015 | .025 | .013 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 18.44 | .065 | .040 | .036 | .032 | .015 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 19.87 | .076 | .039 | .025 | .025 | .012 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 21.31 | .107 | .085 | .045 | .028 | .014 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 22.75 | .110 | .087 | .044 | .025 | .014 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 24.19 | .126 | .094 | .043 | .028 | .014 | b00 | b00 | b00 | b00 | b00 | b00 |
| | 25.62 | .088 | .088 | .043 | .028 | .011 | b00 | b00 | b00 | b00 | b00 | b00 |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(h) A = 2 rectangular wing, r/s = 0.2

| α_B | x/r | δ_w | | | | | | | | | | | |
|------------|-------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| | | 45° | 40° | 35° | 30° | 25° | 20° | 15° | 10° | 6° | 3° | 0° | |
| 0° | 1.134 | .010 | -.016 | -.013 | -.003 | .001 | .061 | | .001 | .001 | .001 | .001 | |
| | 1.259 | .053 | .036 | .009 | .009 | .006 | .005 | | .004 | .004 | .003 | .007 | |
| | 1.384 | .000 | .004 | .000 | .001 | .000 | .000 | | .004 | .004 | .003 | .004 | |
| | 1.509 | .012 | .021 | -.008 | -.006 | .009 | -.007 | | .004 | -.004 | .009 | .004 | |
| | 1.634 | .055 | .060 | .014 | .008 | .011 | .009 | | .009 | .002 | .009 | .002 | |
| | 1.756 | - | .008 | .000 | .000 | .007 | .010 | -.007 | | .015 | -.006 | .002 | |
| | 1.884 | - | .031 | .036 | .025 | .010 | .019 | -.007 | | .000 | .001 | .001 | |
| | 2.009 | .020 | .068 | .003 | .001 | .002 | .000 | | .007 | .004 | .006 | .001 | |
| | 2.134 | .006 | -.014 | -.037 | -.053 | .040 | .000 | | .009 | .006 | .004 | .001 | |
| | 2.259 | .007 | .001 | -.008 | -.031 | .023 | .028 | | .009 | .006 | .006 | .001 | |
| 3° | 1.384 | .035 | .050 | .001 | -.002 | .002 | .001 | | .005 | .006 | .006 | .006 | |
| | 2.059 | -.044 | -.029 | -.058 | .005 | .006 | .014 | | -.003 | -.001 | .001 | .001 | |
| | 1.134 | - | -.001 | -.001 | -.003 | -.003 | .001 | - | .002 | .000 | -.001 | -.001 | |
| | 1.259 | .000 | -.001 | -.001 | -.002 | -.001 | -.002 | - | .001 | -.001 | -.001 | -.001 | |
| | 1.384 | - | .024 | .001 | .001 | .001 | .002 | - | .004 | -.001 | -.001 | -.002 | |
| | 1.509 | .105 | .055 | .006 | -.015 | -.005 | -.004 | - | .002 | -.001 | -.001 | -.002 | |
| | 1.634 | .032 | .147 | .125 | .102 | .047 | .046 | - | .032 | -.025 | -.018 | -.018 | |
| | 1.756 | .264 | .234 | .228 | .178 | .121 | .110 | -.083 | -.058 | -.041 | -.036 | -.036 | |
| | 1.884 | .196 | .225 | .226 | .148 | .187 | .113 | -.080 | -.063 | -.041 | -.045 | -.045 | |
| | 2.009 | .089 | .112 | .135 | .150 | .145 | .098 | -.071 | -.051 | -.042 | -.033 | -.033 | |
| 6° | 1.384 | .103 | .092 | .097 | .127 | .113 | .094 | -.073 | -.057 | -.042 | -.031 | -.023 | |
| | 2.059 | .075 | .046 | .056 | .082 | .084 | .073 | -.053 | -.041 | -.031 | -.027 | -.014 | |
| | 1.134 | .029 | .018 | .021 | .045 | .053 | .037 | -.037 | -.029 | -.021 | -.011 | -.011 | |
| | 2.059 | .017 | .008 | .005 | .027 | .037 | .027 | -.027 | -.019 | -.011 | -.011 | -.011 | |
| | 1.134 | - | -.002 | -.004 | -.001 | -.002 | -.001 | - | .31 | -.002 | -.003 | -.003 | |
| | 1.259 | -.001 | -.002 | -.001 | -.002 | -.001 | -.002 | - | .000 | -.005 | -.004 | -.004 | |
| | 1.384 | -.026 | -.004 | -.005 | -.004 | -.004 | -.004 | - | .004 | -.004 | -.004 | -.004 | |
| | 1.509 | .060 | .021 | -.001 | -.009 | -.009 | -.009 | - | .004 | -.004 | -.004 | -.004 | |
| | 1.634 | .038 | .161 | .161 | .074 | .061 | .040 | -.030 | -.021 | -.016 | -.016 | -.016 | |
| | 1.756 | .310 | .265 | .190 | .174 | .143 | .116 | -.085 | -.056 | -.036 | -.036 | -.036 | |
| 10° | 1.884 | .091 | .270 | .195 | .177 | .151 | .122 | -.091 | -.067 | -.046 | -.046 | -.046 | |
| | 2.009 | .151 | .195 | .199 | .163 | .117 | .091 | -.087 | -.067 | -.046 | -.046 | -.046 | |
| | 2.134 | .106 | .138 | .161 | .141 | .118 | .091 | -.073 | -.062 | -.046 | -.046 | -.046 | |
| | 2.259 | .055 | .088 | .113 | .124 | .097 | .076 | -.061 | -.051 | -.040 | -.029 | -.029 | |
| | 2.384 | .018 | .046 | .059 | .067 | .061 | .049 | -.031 | -.023 | -.014 | -.014 | -.014 | |
| | 2.509 | -.008 | -.004 | .013 | .008 | .037 | .031 | -.023 | -.014 | -.014 | -.014 | -.014 | |
| | 1.134 | - | -.000 | -.001 | -.005 | -.003 | -.003 | - | .005 | -.003 | -.003 | -.003 | |
| | 1.259 | -.001 | -.001 | -.001 | -.001 | -.001 | -.001 | - | .001 | -.001 | -.001 | -.001 | |
| | 1.384 | -.007 | -.007 | -.025 | -.003 | -.003 | -.003 | - | .005 | -.004 | -.004 | -.004 | |
| | 1.509 | .182 | .107 | .059 | .059 | .059 | .059 | -.053 | -.048 | -.036 | -.036 | -.036 | |
| 15° | 1.634 | .301 | .213 | .161 | .161 | .161 | .161 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 1.756 | .339 | .217 | .160 | .160 | .154 | .154 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 1.884 | .228 | .196 | .144 | .144 | .144 | .144 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 2.009 | .082 | .144 | .144 | .144 | .144 | .144 | -.096 | -.074 | -.056 | -.056 | -.056 | |
| | 2.134 | .082 | .144 | .144 | .144 | .144 | .144 | -.096 | -.074 | -.056 | -.056 | -.056 | |
| | 2.259 | .037 | .056 | .065 | .057 | .057 | .057 | -.074 | -.056 | -.047 | -.047 | -.047 | |
| | 2.384 | .034 | .042 | .050 | .051 | .051 | .051 | -.074 | -.056 | -.047 | -.047 | -.047 | |
| | 2.509 | -.003 | .009 | -.010 | -.013 | -.014 | -.014 | -.010 | -.008 | -.003 | -.003 | -.003 | |
| | 1.134 | -.005 | .006 | .006 | .005 | .005 | .005 | -.014 | -.011 | -.004 | -.003 | -.003 | |
| | 1.259 | -.048 | -.006 | -.006 | -.001 | -.001 | -.001 | -.014 | -.011 | -.004 | -.003 | -.003 | |
| 20° | 1.384 | -.011 | -.032 | -.015 | -.007 | -.007 | -.007 | -.014 | -.011 | -.004 | -.003 | -.003 | |
| | 1.509 | .283 | .186 | .173 | .074 | .074 | .064 | -.074 | -.056 | -.048 | -.048 | -.048 | |
| | 1.634 | .409 | .387 | .283 | .168 | .168 | .168 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 1.756 | .350 | .267 | .294 | .165 | .165 | .165 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 1.884 | .234 | .259 | .294 | .142 | .142 | .142 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 2.009 | .113 | .165 | .193 | .181 | .181 | .181 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 2.134 | .066 | .097 | .134 | .146 | .146 | .146 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 2.259 | .028 | .040 | .064 | .084 | .084 | .084 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 2.384 | .026 | .047 | .069 | .096 | .096 | .096 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| | 2.509 | -.006 | .047 | .067 | .087 | .087 | .087 | -.126 | -.104 | -.086 | -.086 | -.086 | |
| 25° | 1.134 | - | -.017 | .020 | .021 | .015 | .024 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.259 | .016 | .018 | .011 | .011 | .006 | .012 | -.017 | -.011 | .012 | -.012 | -.012 | |
| | 1.384 | .012 | .018 | .011 | .002 | .002 | .004 | -.017 | -.011 | .007 | -.007 | -.007 | |
| | 1.509 | .015 | .020 | .015 | .007 | .007 | .011 | -.017 | -.011 | .005 | -.005 | -.005 | |
| | 1.634 | .010 | .010 | .001 | .001 | .000 | .000 | -.017 | -.011 | .005 | -.005 | -.005 | |
| | 1.756 | .018 | .018 | .018 | .018 | .018 | .018 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.884 | .017 | .017 | .017 | .017 | .017 | .017 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 2.009 | .013 | .013 | .013 | .013 | .013 | .013 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 2.134 | .009 | .009 | .009 | .009 | .009 | .009 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 2.259 | .005 | .005 | .005 | .005 | .005 | .005 | -.017 | -.011 | .017 | -.017 | -.017 | |
| 28° | 2.384 | .004 | .004 | .004 | .004 | .004 | .004 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 2.509 | -.004 | .010 | .009 | .009 | .009 | .009 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.134 | -.005 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.259 | .000 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.384 | .000 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.509 | .000 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.634 | .000 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.756 | .000 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 1.884 | .000 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |
| | 2.009 | .000 | .000 | .000 | .000 | .000 | .000 | -.017 | -.011 | .017 | -.017 | -.017 | |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(h) $A = 2$ rectangular wing, $r/s = 0.2$ - Concluded

| a_B | x/r | δ_W | | | | | | | | | |
|-------|-------|------------|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° |
| 0° | 1.134 | - | - | - | - | - | - | - | - | - | - |
| | 1.259 | - | - | - | - | - | - | - | - | - | - |
| | 1.384 | - | - | - | - | - | - | - | - | - | - |
| | 1.509 | - | - | - | - | - | - | - | - | - | - |
| | 1.634 | - | - | - | - | - | - | - | - | - | - |
| | 1.756 | - | - | - | - | - | - | - | - | - | - |
| | 1.884 | - | - | - | - | - | - | - | - | - | - |
| | 2.009 | - | - | - | - | - | - | - | - | - | - |
| | 2.134 | - | - | - | - | - | - | - | - | - | - |
| | 2.259 | - | - | - | - | - | - | - | - | - | - |
| 3° | 1.134 | -0.02 | -0.02 | -0.01 | -0.01 | -0.01 | -0.01 | -0.00 | -0.00 | -0.01 | -0.01 |
| | 1.259 | -0.01 | -0.01 | -0.01 | -0.01 | -0.00 | -0.01 | -0.01 | -0.01 | -0.01 | -0.00 |
| | 1.384 | -0.00 | -0.01 | -0.02 | -0.02 | -0.02 | -0.02 | -0.01 | -0.01 | -0.01 | -0.00 |
| | 1.509 | -0.01 | -0.01 | -0.02 | -0.02 | -0.02 | -0.02 | -0.01 | -0.01 | -0.01 | -0.00 |
| | 1.634 | -0.07 | -0.01 | -0.10 | -0.10 | -0.10 | -0.10 | -0.08 | -0.08 | -0.08 | -0.08 |
| | 1.756 | -0.11 | -0.02 | -0.15 | -0.15 | -0.15 | -0.15 | -0.13 | -0.13 | -0.13 | -0.13 |
| | 1.884 | -0.15 | -0.04 | -0.22 | -0.22 | -0.22 | -0.22 | -0.18 | -0.18 | -0.18 | -0.18 |
| | 2.009 | -0.17 | -0.08 | -0.22 | -0.22 | -0.22 | -0.22 | -0.18 | -0.18 | -0.18 | -0.18 |
| | 2.134 | -0.19 | -0.12 | -0.22 | -0.22 | -0.22 | -0.22 | -0.18 | -0.18 | -0.18 | -0.18 |
| | 2.259 | -0.02 | -0.16 | -0.22 | -0.22 | -0.22 | -0.22 | -0.18 | -0.18 | -0.18 | -0.18 |
| 6° | 1.134 | -0.01 | -0.01 | -0.00 | -0.00 | -0.00 | -0.01 | -0.02 | -0.03 | -0.03 | -0.01 |
| | 1.259 | -0.00 | -0.01 | -0.01 | -0.01 | -0.01 | -0.00 | -0.02 | -0.01 | -0.01 | -0.00 |
| | 1.384 | -0.005 | -0.04 | -0.03 | -0.03 | -0.04 | -0.04 | -0.03 | -0.05 | -0.05 | -0.04 |
| | 1.509 | -0.003 | -0.03 | -0.03 | -0.04 | -0.04 | -0.03 | -0.02 | -0.04 | -0.04 | -0.03 |
| | 1.634 | -0.021 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 1.756 | -0.038 | -0.021 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 1.884 | -0.043 | -0.021 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 |
| | 2.009 | -0.040 | -0.021 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 |
| | 2.134 | -0.040 | -0.021 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 |
| | 2.259 | -0.026 | -0.012 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 | -0.00 |
| 10° | 1.134 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 1.259 | -0.003 | -0.01 | -0.01 | -0.01 | -0.01 | -0.00 | -0.02 | -0.02 | -0.02 | -0.01 |
| | 1.384 | -0.003 | -0.02 | -0.03 | -0.03 | -0.04 | -0.04 | -0.03 | -0.05 | -0.05 | -0.04 |
| | 1.509 | -0.006 | -0.04 | -0.06 | -0.06 | -0.05 | -0.04 | -0.03 | -0.04 | -0.04 | -0.03 |
| | 1.634 | -0.045 | -0.039 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 |
| | 1.756 | -0.051 | -0.031 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 1.884 | -0.060 | -0.046 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 2.009 | -0.071 | -0.044 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 2.134 | -0.058 | -0.037 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 2.259 | -0.051 | -0.033 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| 15° | 1.134 | -0.03 | -0.04 | -0.08 | -0.08 | -0.08 | -0.07 | -0.09 | -0.08 | -0.08 | -0.08 |
| | 1.259 | -0.05 | -0.06 | -0.04 | -0.04 | -0.05 | -0.04 | -0.05 | -0.05 | -0.05 | -0.05 |
| | 1.384 | -0.02 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 |
| | 1.509 | -0.02 | -0.04 | -0.08 | -0.08 | -0.08 | -0.07 | -0.08 | -0.08 | -0.08 | -0.08 |
| | 1.634 | -0.061 | -0.047 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 |
| | 1.756 | -0.069 | -0.057 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 |
| | 1.884 | -0.063 | -0.047 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| | 2.009 | -0.087 | -0.061 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| | 2.134 | -0.094 | -0.069 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| | 2.259 | -0.057 | -0.066 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| 20° | 1.134 | -0.028 | -0.10 | -0.08 | -0.08 | -0.08 | -0.07 | -0.09 | -0.08 | -0.08 | -0.08 |
| | 1.259 | -0.005 | -0.06 | -0.04 | -0.04 | -0.05 | -0.04 | -0.05 | -0.05 | -0.05 | -0.05 |
| | 1.384 | -0.002 | -0.03 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| | 1.509 | -0.002 | -0.04 | -0.08 | -0.08 | -0.08 | -0.07 | -0.08 | -0.08 | -0.08 | -0.08 |
| | 1.634 | -0.061 | -0.047 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 |
| | 1.756 | -0.069 | -0.057 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 | -0.16 |
| | 1.884 | -0.089 | -0.067 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| | 2.009 | -0.187 | -0.085 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| | 2.134 | -1.41 | -1.07 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| | 2.259 | -1.45 | -1.10 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 | -0.22 |
| 25° | 1.134 | -0.29 | -0.31 | -0.16 | -0.16 | -0.06 | -0.08 | -0.01 | -0.40 | -0.03 | -0.15 |
| | 1.259 | -0.11 | -0.13 | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | -0.10 | -0.10 | -0.09 |
| | 1.384 | -0.10 | -0.13 | -0.08 | -0.08 | -0.08 | -0.08 | -0.09 | -0.09 | -0.09 | -0.09 |
| | 1.509 | -0.082 | -0.091 | -0.04 | -0.04 | -0.04 | -0.04 | -0.06 | -0.06 | -0.06 | -0.06 |
| | 1.634 | -0.098 | -0.095 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 | -0.05 |
| | 1.756 | -1.16 | -1.03 | -0.60 | -0.60 | -0.54 | -0.54 | -0.56 | -0.35 | -0.15 | -0.50 |
| | 1.884 | -1.60 | -1.05 | -0.64 | -0.64 | -0.57 | -0.57 | -0.59 | -0.23 | -0.15 | -0.30 |
| | 2.009 | -1.88 | -1.27 | -0.70 | -0.70 | -0.65 | -0.65 | -0.67 | -0.23 | -0.15 | -0.28 |
| | 2.134 | -2.07 | -1.55 | -0.88 | -0.88 | -0.83 | -0.83 | -0.85 | -0.44 | -0.11 | -0.14 |
| | 2.259 | -2.08 | -1.51 | -0.82 | -0.82 | -0.82 | -0.82 | -0.84 | -0.46 | -0.02 | -0.08 |
| 25° | 1.384 | -0.34 | -0.94 | -0.54 | -0.34 | -0.22 | -0.22 | -0.24 | -0.28 | -0.16 | -0.23 |
| | 2.509 | -2.28 | -1.76 | -0.94 | -0.54 | -0.34 | -0.22 | -0.24 | -0.28 | -0.23 | -0.23 |

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(1) $A = 1$ rectangular wing, $r/s = 0.2$

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(i) $A = 1$ rectangular wing, $r/s = 0.2$ - Concluded

TABLE IV.--LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(j) $A = 1$ rectangular wing, $r/s = 0.4$

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Concluded
(j) $A = 1$ rectangular wing, $r/s = 0.4$ - Concluded

| α_B | x/r | δ_w | | | | | | | | | | |
|------------|-------|------------|------|------|------|------|------|------|------|------|------|--|
| | | -3° | -6° | -10° | -15° | -20° | -25° | -30° | -35° | -40° | -45° | |
| 0° | 6.94 | .001 | .001 | .000 | .001 | .002 | .000 | .000 | .001 | .000 | .000 | |
| | 8.37 | .000 | .001 | .000 | .001 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 9.81 | .000 | .001 | .000 | .001 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 11.35 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 12.89 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 14.43 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 15.56 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 17.00 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 18.44 | .001 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 19.87 | .000 | .001 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 21.31 | .000 | .000 | .001 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | |
| 3° | 22.75 | .000 | .000 | .000 | .001 | .000 | .000 | .000 | .001 | .000 | .000 | |
| | 24.19 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | .001 | .000 | .000 | |
| | 25.52 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .001 | .000 | .000 | |
| | 6.94 | .002 | .001 | .000 | .001 | .002 | .000 | .004 | .001 | .002 | .003 | |
| | 8.37 | .002 | .001 | .000 | .002 | .001 | .001 | .005 | .000 | .001 | .003 | |
| | 9.81 | .002 | .001 | .000 | .001 | .001 | .001 | .004 | .000 | .001 | .003 | |
| | 11.35 | .000 | .001 | .000 | .001 | .000 | .001 | .004 | .000 | .001 | .006 | |
| | 12.89 | .006 | .005 | .006 | .007 | .006 | .005 | .010 | .004 | .006 | .001 | |
| | 14.43 | .002 | .000 | .000 | .000 | .000 | .000 | .008 | .004 | .000 | .001 | |
| | 15.56 | .000 | .001 | .000 | .000 | .000 | .000 | .003 | .005 | .000 | .002 | |
| | 17.00 | .000 | .001 | .000 | .000 | .000 | .000 | .005 | .007 | .000 | .002 | |
| | 18.44 | .003 | .004 | .003 | .022 | .027 | .020 | .059 | .051 | .004 | .079 | |
| | 19.87 | .010 | .010 | .011 | .024 | .027 | .020 | .054 | .051 | .004 | .074 | |
| | 21.31 | .010 | .010 | .010 | .024 | .027 | .020 | .053 | .051 | .004 | .073 | |
| 6° | 22.75 | .010 | .010 | .010 | .025 | .027 | .020 | .053 | .051 | .004 | .073 | |
| | 24.19 | .010 | .010 | .010 | .025 | .027 | .020 | .053 | .051 | .004 | .071 | |
| | 25.52 | .008 | .007 | .005 | .002 | .007 | .016 | .016 | .001 | .012 | .010 | |
| | 6.94 | .000 | .000 | .001 | .002 | .000 | .001 | .001 | .001 | .001 | .000 | |
| | 8.37 | .002 | .002 | .000 | .000 | .001 | .001 | .001 | .001 | .001 | .003 | |
| | 9.81 | .000 | .001 | .001 | .000 | .000 | .000 | .001 | .001 | .001 | .000 | |
| | 11.35 | .000 | .001 | .001 | .000 | .000 | .000 | .006 | .000 | .000 | .004 | |
| | 12.89 | .001 | .001 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .001 | |
| | 14.43 | .000 | .001 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .006 | |
| | 15.56 | .001 | .001 | .000 | .000 | .000 | .000 | .000 | .000 | .001 | .053 | |
| | 17.00 | .005 | .000 | .000 | .000 | .000 | .000 | .001 | .000 | .000 | .058 | |
| | 18.44 | .035 | .018 | .001 | .029 | .046 | .051 | .054 | .078 | .078 | .075 | |
| | 19.87 | .036 | .016 | .004 | .029 | .041 | .045 | .051 | .078 | .078 | .073 | |
| 10° | 21.31 | .036 | .016 | .006 | .029 | .040 | .040 | .050 | .078 | .078 | .070 | |
| | 22.75 | .012 | .012 | .014 | .023 | .021 | .013 | .016 | .013 | .012 | .007 | |
| | 24.19 | .011 | .012 | .012 | .021 | .020 | .016 | .016 | .013 | .012 | .007 | |
| | 25.52 | .010 | .012 | .006 | .000 | .003 | .006 | .000 | .003 | .001 | .003 | |
| | 6.94 | .003 | .003 | .003 | .001 | .001 | .002 | .000 | .000 | .004 | .000 | |
| | 8.37 | .003 | .002 | .003 | .000 | .001 | .003 | .001 | .001 | .005 | .001 | |
| | 9.81 | .001 | .001 | .001 | .000 | .001 | .000 | .000 | .001 | .001 | .002 | |
| | 11.35 | .000 | .001 | .001 | .000 | .001 | .000 | .004 | .000 | .001 | .001 | |
| | 12.89 | .001 | .001 | .001 | .000 | .000 | .000 | .000 | .001 | .001 | .001 | |
| | 14.43 | .000 | .001 | .000 | .000 | .000 | .000 | .000 | .001 | .001 | .010 | |
| | 15.56 | .000 | .001 | .000 | .000 | .000 | .000 | .000 | .001 | .001 | .058 | |
| 15° | 17.00 | .006 | .006 | .006 | .005 | .004 | .003 | .006 | .004 | .004 | .005 | |
| | 18.44 | .006 | .006 | .006 | .005 | .004 | .003 | .006 | .004 | .004 | .005 | |
| | 19.87 | .009 | .006 | .006 | .006 | .005 | .004 | .006 | .004 | .004 | .005 | |
| | 21.31 | .037 | .016 | .016 | .033 | .047 | .047 | .049 | .078 | .078 | .069 | |
| | 22.75 | .026 | .023 | .014 | .021 | .027 | .013 | .016 | .013 | .012 | .009 | |
| | 24.19 | .011 | .012 | .012 | .021 | .020 | .016 | .016 | .012 | .011 | .009 | |
| | 25.52 | .010 | .012 | .006 | .000 | .003 | .006 | .000 | .003 | .001 | .009 | |
| | 6.94 | .005 | .003 | .002 | .004 | .004 | .002 | .002 | .001 | .004 | .001 | |
| | 8.37 | .002 | .001 | .001 | .003 | .001 | .001 | .001 | .001 | .001 | .001 | |
| | 9.81 | .004 | .001 | .001 | .002 | .003 | .001 | .001 | .001 | .001 | .001 | |
| | 11.35 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | .001 | |
| 20° | 12.89 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | |
| | 14.43 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | |
| | 15.56 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | .005 | |
| | 17.00 | .035 | .035 | .035 | .035 | .035 | .035 | .035 | .035 | .035 | .035 | |
| | 18.44 | .077 | .061 | .058 | .099 | .015 | .015 | .015 | .015 | .014 | .014 | |
| | 19.87 | .085 | .068 | .058 | .098 | .011 | .011 | .011 | .011 | .011 | .011 | |
| | 21.31 | .078 | .065 | .059 | .097 | .011 | .011 | .011 | .011 | .011 | .011 | |
| | 22.75 | .065 | .058 | .057 | .095 | .015 | .015 | .015 | .015 | .015 | .015 | |
| | 24.19 | .060 | .056 | .054 | .095 | .010 | .010 | .010 | .010 | .010 | .010 | |
| | 25.52 | .040 | .039 | .026 | .055 | .005 | .004 | .004 | .004 | .014 | .015 | |
| 25° | 6.94 | .014 | .005 | .004 | .004 | .002 | .000 | .000 | .000 | .000 | .000 | |
| | 8.37 | .009 | .000 | .000 | .003 | .004 | .000 | .001 | .001 | .001 | .001 | |
| | 9.81 | .010 | .000 | .000 | .003 | .005 | .000 | .001 | .001 | .001 | .001 | |
| | 11.35 | .009 | .000 | .000 | .003 | .004 | .000 | .001 | .001 | .001 | .001 | |
| | 12.89 | .009 | .000 | .000 | .003 | .004 | .000 | .001 | .001 | .001 | .001 | |
| | 14.43 | .006 | .000 | .000 | .003 | .003 | .000 | .001 | .001 | .001 | .001 | |
| | 15.56 | .011 | .000 | .000 | .003 | .007 | .000 | .002 | .002 | .001 | .001 | |
| | 17.00 | .034 | .014 | .014 | .033 | .003 | .003 | .002 | .002 | .001 | .001 | |
| | 18.44 | .034 | .014 | .014 | .033 | .003 | .003 | .002 | .002 | .001 | .001 | |
| | 19.87 | .030 | .024 | .024 | .033 | .003 | .003 | .002 | .002 | .001 | .001 | |
| | 21.31 | .021 | .026 | .024 | .033 | .003 | .003 | .002 | .002 | .001 | .001 | |
| | 22.75 | .016 | .024 | .021 | .025 | .002 | .001 | .001 | .002 | .001 | .001 | |
| | 24.19 | .018 | .024 | .021 | .025 | .002 | .001 | .001 | .002 | .001 | .001 | |
| | 25.52 | .015 | .028 | .026 | .014 | .003 | .001 | .005 | .005 | .004 | .007 | |

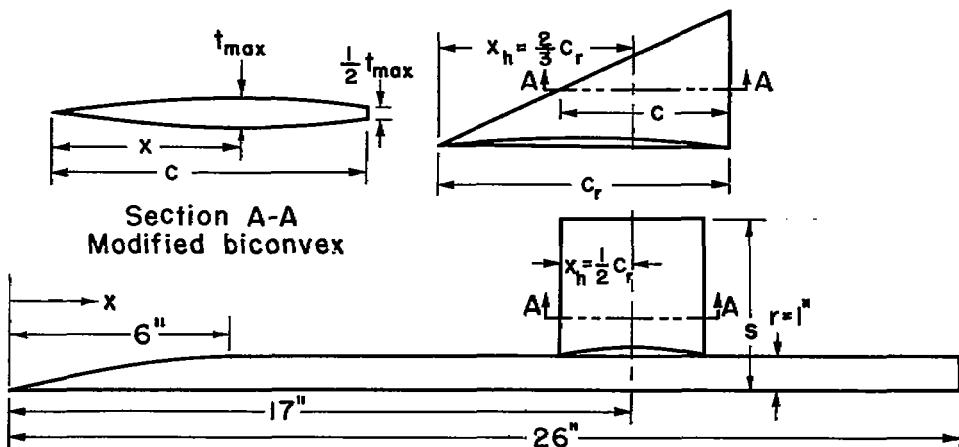
TABLE V.- PRESSURE COEFFICIENTS OF THE BODY ALONE
(a) Model I

| θ | x/r | a_B | | | | | | |
|----------|-------|--------|--------|--------|--------|--------|--------|-----|
| | | 0° | 3° | 6° | 10° | 15° | 20° | 25° |
| 7.22 | .027 | - .034 | - .040 | - .047 | - .058 | - .079 | - .086 | |
| 8.56 | .022 | - .036 | - .033 | - .038 | - .051 | - .079 | - .084 | |
| 9.94 | .018 | - .024 | - .027 | - .028 | - .059 | - .076 | - .083 | |
| 11.34 | .020 | - .022 | - .021 | - .023 | - .061 | - .076 | - .086 | |
| 12.59 | .015 | - .017 | - .017 | - .021 | - .064 | - .078 | - .081 | |
| 13.84 | .011 | - .010 | - .011 | - .028 | - .064 | - .077 | - .081 | |
| 15.09 | .007 | - .007 | - .009 | - .023 | - .066 | - .079 | - .083 | |
| 16.34 | .006 | - .006 | - .006 | - .031 | - .066 | - .079 | - .080 | |
| 17.56 | .004 | - .004 | - .008 | - .027 | - .064 | - .078 | - .074 | |
| 18.84 | .002 | - .002 | - .005 | - .029 | - .068 | - .067 | - .069 | |
| 20.09 | .001 | - .001 | - .004 | - .031 | - .058 | - .064 | - .065 | |
| 21.34 | .005 | - .005 | - .005 | - .026 | - .057 | - .056 | - .062 | |
| 22.59 | .004 | - .004 | - .006 | - .020 | - .056 | - .056 | - .066 | |
| 23.84 | .019 | - .011 | - .009 | - .023 | - .059 | - .058 | - .064 | |
| 25.09 | .019 | - .011 | - .009 | - .023 | - .059 | - .058 | - .064 | |
| 6° | | | | | | | | |
| 7.22 | .027 | - .033 | - .038 | - .048 | - .070 | - .081 | - .084 | |
| 8.56 | .021 | - .026 | - .034 | - .049 | - .073 | - .083 | - .084 | |
| 9.94 | .019 | - .024 | - .029 | - .048 | - .074 | - .083 | - .085 | |
| 11.34 | .020 | - .023 | - .025 | - .047 | - .078 | - .078 | - .086 | |
| 12.59 | .015 | - .017 | - .029 | - .041 | - .070 | - .071 | - .081 | |
| 13.84 | .010 | - .018 | - .037 | - .067 | - .078 | - .079 | - .089 | |
| 15.09 | .008 | - .011 | - .019 | - .038 | - .066 | - .077 | - .089 | |
| 16.34 | .005 | - .016 | - .042 | - .063 | - .079 | - .080 | - .090 | |
| 17.56 | .005 | - .014 | - .041 | - .064 | - .082 | - .077 | - .077 | |
| 18.84 | .006 | - .013 | - .037 | - .060 | - .077 | - .072 | - .072 | |
| 20.09 | .009 | - .015 | - .040 | - .068 | - .078 | - .070 | - .070 | |
| 21.34 | .004 | - .004 | - .011 | - .039 | - .063 | - .068 | - .067 | |
| 22.59 | .018 | - .005 | - .009 | - .028 | - .063 | - .064 | - .063 | |
| 23.84 | .018 | - .005 | - .007 | - .026 | - .068 | - .063 | - .059 | |
| 25.09 | .018 | - .007 | - .005 | - .026 | - .061 | - .057 | - .047 | |
| 15° | | | | | | | | |
| 7.22 | .029 | - .037 | - .044 | - .067 | - .066 | - .086 | - .087 | |
| 8.56 | .024 | - .030 | - .037 | - .084 | - .084 | - .086 | - .086 | |
| 9.94 | .021 | - .027 | - .034 | - .069 | - .078 | - .081 | - .086 | |
| 11.34 | .028 | - .028 | - .029 | - .070 | - .070 | - .075 | - .082 | |
| 12.59 | .019 | - .019 | - .026 | - .071 | - .068 | - .075 | - .081 | |
| 13.84 | .016 | - .013 | - .021 | - .061 | - .061 | - .079 | - .079 | |
| 15.09 | .010 | - .018 | - .025 | - .060 | - .065 | - .069 | - .081 | |
| 16.34 | .008 | - .008 | - .023 | - .037 | - .061 | - .068 | - .076 | |
| 17.56 | .008 | - .008 | - .023 | - .037 | - .060 | - .066 | - .071 | |
| 18.84 | .009 | - .007 | - .024 | - .034 | - .057 | - .065 | - .067 | |
| 20.09 | .014 | - .006 | - .019 | - .031 | - .059 | - .061 | - .064 | |
| 21.34 | .005 | - .005 | - .015 | - .027 | - .035 | - .057 | - .059 | |
| 22.59 | .005 | - .005 | - .013 | - .026 | - .033 | - .054 | - .056 | |
| 23.84 | .014 | - .006 | - .018 | - .025 | - .033 | - .048 | - .047 | |
| 30° | | | | | | | | |
| 7.22 | .029 | - .037 | - .044 | - .067 | - .066 | - .086 | - .087 | |
| 8.56 | .024 | - .030 | - .037 | - .084 | - .084 | - .086 | - .086 | |
| 9.94 | .021 | - .027 | - .034 | - .069 | - .078 | - .081 | - .086 | |
| 11.34 | .028 | - .028 | - .029 | - .070 | - .070 | - .075 | - .082 | |
| 12.59 | .019 | - .019 | - .026 | - .071 | - .068 | - .075 | - .081 | |
| 13.84 | .016 | - .013 | - .021 | - .061 | - .061 | - .079 | - .079 | |
| 15.09 | .010 | - .018 | - .025 | - .060 | - .065 | - .069 | - .081 | |
| 16.34 | .008 | - .008 | - .023 | - .037 | - .061 | - .068 | - .076 | |
| 17.56 | .008 | - .008 | - .023 | - .037 | - .060 | - .066 | - .071 | |
| 18.84 | .009 | - .007 | - .024 | - .034 | - .057 | - .065 | - .067 | |
| 20.09 | .014 | - .006 | - .019 | - .031 | - .059 | - .061 | - .064 | |
| 21.34 | .005 | - .005 | - .015 | - .027 | - .035 | - .057 | - .059 | |
| 22.59 | .005 | - .005 | - .013 | - .026 | - .033 | - .054 | - .056 | |
| 23.84 | .014 | - .006 | - .018 | - .025 | - .033 | - .048 | - .047 | |
| 60° | | | | | | | | |
| 7.22 | .031 | - .040 | - .053 | - .076 | - .079 | - .083 | - .087 | |
| 8.56 | .029 | - .037 | - .052 | - .069 | - .074 | - .082 | - .085 | |
| 9.94 | .028 | - .032 | - .045 | - .058 | - .069 | - .076 | - .082 | |
| 11.34 | .019 | - .027 | - .037 | - .054 | - .068 | - .076 | - .081 | |
| 12.59 | .014 | - .019 | - .030 | - .049 | - .065 | - .073 | - .079 | |
| 13.84 | .014 | - .019 | - .030 | - .044 | - .060 | - .069 | - .077 | |
| 15.09 | .012 | - .015 | - .031 | - .048 | - .061 | - .071 | - .078 | |
| 16.34 | .006 | - .011 | - .021 | - .041 | - .089 | - .067 | - .075 | |
| 17.56 | .005 | - .010 | - .018 | - .036 | - .087 | - .063 | - .073 | |
| 18.84 | .004 | - .006 | - .013 | - .032 | - .085 | - .063 | - .073 | |
| 20.09 | .002 | - .003 | - .011 | - .028 | - .080 | - .061 | - .068 | |
| 21.34 | .003 | - .003 | - .009 | - .025 | - .047 | - .065 | - .065 | |
| 22.59 | .003 | - .003 | - .007 | - .021 | - .042 | - .054 | - .060 | |
| 23.84 | .007 | - .004 | - .003 | - .021 | - .029 | - .043 | - .055 | |
| 25.09 | .007 | - .004 | - .003 | - .021 | - .029 | - .043 | - .055 | |

| θ | x/r | a_B | | | | | | |
|----------|-------|--------|--------|--------|------|------|------|-----|
| | | 0° | 3° | 6° | 10° | 15° | 20° | 25° |
| 7.22 | .030 | - .026 | - .031 | - .014 | .018 | .047 | .110 | |
| 8.56 | .028 | - .026 | - .033 | - .021 | .007 | .047 | .101 | |
| 9.94 | .028 | - .028 | - .026 | - .028 | .021 | .047 | .112 | |
| 11.34 | .023 | - .023 | - .023 | - .023 | .021 | .043 | .109 | |
| 12.59 | .018 | - .018 | - .018 | - .021 | .024 | .048 | .115 | |
| 13.84 | .018 | - .018 | - .018 | - .019 | .019 | .048 | .115 | |
| 15.09 | .013 | - .013 | - .013 | - .015 | .015 | .040 | .128 | |
| 16.34 | .013 | - .013 | - .013 | - .013 | .013 | .040 | .140 | |
| 17.56 | .005 | - .005 | - .005 | - .011 | .011 | .047 | .156 | |
| 18.84 | .005 | - .005 | - .005 | - .010 | .010 | .048 | .161 | |
| 20.09 | .008 | - .008 | - .008 | - .008 | .008 | .049 | .159 | |
| 21.34 | .001 | - .001 | - .001 | - .001 | .001 | .049 | .156 | |
| 22.59 | .001 | - .001 | - .001 | - .001 | .001 | .049 | .157 | |
| 23.84 | .004 | - .004 | - .004 | - .004 | .004 | .049 | .151 | |
| 25.09 | .009 | - .009 | - .009 | - .009 | .009 | .049 | .155 | |
| 120° | | | | | | | | |
| 7.22 | .031 | - .021 | - .004 | .028 | .066 | .164 | .309 | |
| 8.56 | .024 | - .015 | .003 | .028 | .068 | .173 | .279 | |
| 9.94 | .019 | - .017 | .006 | .028 | .065 | .161 | .264 | |
| 11.34 | .018 | - .018 | .006 | .028 | .065 | .150 | .234 | |
| 12.59 | .018 | - .018 | .005 | .028 | .060 | .144 | .198 | |
| 13.84 | .018 | - .018 | .005 | .028 | .060 | .144 | .196 | |
| 15.09 | .010 | - .010 | .005 | .028 | .060 | .144 | .196 | |
| 16.34 | .008 | - .008 | .004 | .028 | .060 | .144 | .196 | |
| 17.56 | .004 | - .004 | .004 | .028 | .060 | .144 | .196 | |
| 18.84 | .004 | - .004 | .004 | .028 | .060 | .144 | .196 | |
| 20.09 | .009 | - .009 | .004 | .028 | .060 | .144 | .196 | |
| 21.34 | .001 | - .001 | .001 | .028 | .060 | .144 | .196 | |
| 22.59 | .001 | - .001 | .001 | .028 | .060 | .144 | .196 | |
| 23.84 | .004 | - .004 | .001 | .028 | .060 | .144 | .196 | |
| 25.09 | .009 | - .009 | .001 | .028 | .060 | .144 | .196 | |
| 165° | | | | | | | | |
| 7.22 | .030 | - .015 | .003 | .028 | .066 | .164 | .315 | |
| 8.56 | .020 | - .012 | .002 | .028 | .065 | .163 | .311 | |
| 9.94 | .019 | - .019 | .002 | .028 | .065 | .161 | .311 | |
| 11.34 | .018 | - .018 | .002 | .028 | .065 | .161 | .311 | |
| 12.59 | .018 | - .018 | .002 | .028 | .065 | .161 | .311 | |
| 13.84 | .018 | - .018 | .002 | .028 | .065 | .161 | .311 | |
| 15.09 | .010 | - .010 | .002 | .028 | .065 | .161 | .311 | |
| 16.34 | .008 | - .008 | .002 | .028 | .065 | .161 | .311 | |
| 17.56 | .004 | - .004 | .002 | .028 | .065 | .161 | .311 | |
| 18.84 | .004 | - .004 | .002 | .028 | .065 | .161 | .311 | |
| 20.09 | .009 | - .009 | .002 | .028 | .065 | .161 | .311 | |
| 21.34 | .001 | - .001 | .001 | .028 | .065 | .161 | .311 | |
| 22.59 | .001 | - .001 | .001 | .028 | .065 | .161 | .311 | |
| 23.84 | .004 | - .004 | .001 | .028 | .065 | .161 | .311 | |
| 25.09 | .009 | - .009 | .001 | .028 | .065 | .161 | .311 | |
| 174° | | | | | | | | |
| 7.22 | .030 | - .013 | .001 | .028 | .066 | .163 | .313 | |
| 8.56 | .020 | - .011 | .001 | .028 | .066 | .163 | .313 | |
| 9.94 | .019 | - .010 | .001 | .028 | .066 | .163 | .313 | |
| 11.34 | .018 | - .010 | .001 | .028 | .066 | .163 | .313 | |
| 12.59 | .018 | - .010 | .001 | .028 | .066 | .163 | .313 | |
| 13.84 | .018 | - .010 | .001 | .028 | .066 | .163 | .313 | |
| 15.09 | .010 | - .010 | .001 | .028 | .066 | .163 | .313 | |
| 16.34 | .008 | - .008 | .001 | .028 | .066 | .163 | .313 | |
| 17.56 | .004 | - .004 | .001 | .028 | .066 | .163 | .313 | |
| 18.84 | .004 | - .004 | .001 | .028 | .066 | .163 | .313 | |
| 20.09 | .009 | - .009 | .001 | .028 | .066 | .163 | .313 | |
| 21.34 | .001 | - .001 | .001 | .028 | .066 | .163 | .313 | |
| 22.59 | .001 | - .001 | .001 | .028 | .066 | .163 | .313 | |
| 23.84 | .004 | - .004 | .001 | .028 | .066 | .163 | .313 | |
| 25.09 | .009 | - .009 | .001 | .028 | .066 | .163 | .313 | |

TABLE V.- PRESSURE COEFFICIENTS OF THE BODY ALONE - Concluded
 (b) Model II

| θ | x/r | a _B | | | | | | | θ | x/r | a _B | | | | | | |
|-----|-------|----------------|--------|--------|--------|--------|--------|--------|------|-------|----------------|--------|--------|--------|-------|-------|-------|
| | | 0° | 3° | 6° | 10° | 15° | 20° | 25° | | | 0° | 3° | 6° | 10° | 15° | 20° | 25° |
| 6° | 6.94 | -0.026 | 0.36 | -0.048 | -0.049 | -0.059 | -0.069 | -0.086 | 120° | 6.94 | -0.031 | -0.026 | -0.021 | -0.014 | 0.018 | 0.047 | 0.13 |
| | 8.37 | -0.028 | -0.027 | -0.034 | -0.040 | -0.050 | -0.069 | -0.084 | | 8.37 | -0.028 | -0.026 | -0.023 | -0.016 | 0.007 | 0.047 | 0.101 |
| | 9.81 | -0.019 | -0.024 | -0.027 | -0.031 | -0.039 | -0.059 | -0.086 | | 9.81 | -0.028 | -0.023 | -0.021 | -0.016 | 0.004 | 0.047 | 0.108 |
| | 11.25 | -0.020 | -0.021 | -0.027 | -0.031 | -0.039 | -0.061 | -0.086 | | 11.25 | -0.021 | -0.021 | -0.021 | -0.016 | 0.004 | 0.047 | 0.108 |
| | 12.69 | -0.018 | -0.017 | -0.021 | -0.026 | -0.039 | -0.061 | -0.085 | | 12.69 | -0.017 | -0.016 | -0.016 | -0.011 | 0.003 | 0.047 | 0.108 |
| | 14.13 | -0.016 | -0.017 | -0.021 | -0.026 | -0.039 | -0.065 | -0.086 | | 14.13 | -0.016 | -0.016 | -0.016 | -0.011 | 0.003 | 0.047 | 0.108 |
| | 15.56 | -0.005 | -0.006 | -0.016 | -0.026 | -0.039 | -0.065 | -0.086 | | 15.56 | -0.004 | -0.004 | -0.004 | -0.003 | 0.003 | 0.047 | 0.108 |
| | 17.00 | -0.007 | -0.008 | -0.009 | -0.016 | -0.038 | -0.065 | -0.086 | | 17.00 | -0.003 | -0.003 | -0.003 | -0.002 | 0.006 | 0.047 | 0.108 |
| 15° | 6.94 | -0.089 | -0.034 | -0.038 | -0.047 | -0.069 | -0.080 | -0.083 | 150° | 6.94 | -0.032 | -0.028 | -0.023 | -0.018 | 0.005 | 0.047 | 0.17 |
| | 8.37 | -0.089 | -0.026 | -0.034 | -0.049 | -0.072 | -0.083 | -0.083 | | 8.37 | -0.024 | -0.016 | -0.009 | -0.005 | 0.000 | 0.047 | 0.161 |
| | 9.81 | -0.019 | -0.024 | -0.030 | -0.046 | -0.074 | -0.083 | -0.084 | | 9.81 | -0.019 | -0.016 | -0.006 | -0.003 | 0.000 | 0.047 | 0.161 |
| | 11.25 | -0.020 | -0.024 | -0.030 | -0.046 | -0.075 | -0.078 | -0.086 | | 11.25 | -0.019 | -0.016 | -0.006 | -0.003 | 0.000 | 0.047 | 0.161 |
| | 12.69 | -0.016 | -0.016 | -0.020 | -0.040 | -0.069 | -0.078 | -0.086 | | 12.69 | -0.016 | -0.016 | -0.006 | -0.003 | 0.000 | 0.047 | 0.161 |
| | 14.13 | -0.010 | -0.010 | -0.019 | -0.016 | -0.067 | -0.074 | -0.078 | | 14.13 | -0.010 | -0.010 | -0.006 | -0.003 | 0.000 | 0.047 | 0.161 |
| | 15.56 | -0.007 | -0.007 | -0.010 | -0.019 | -0.080 | -0.085 | -0.081 | | 15.56 | -0.005 | -0.005 | -0.004 | -0.003 | 0.000 | 0.047 | 0.161 |
| | 17.00 | -0.004 | -0.005 | -0.015 | -0.027 | -0.083 | -0.083 | -0.083 | | 17.00 | -0.003 | -0.003 | -0.003 | -0.002 | 0.006 | 0.047 | 0.161 |
| 30° | 6.94 | -0.30 | -0.030 | -0.046 | -0.056 | -0.086 | -0.087 | -0.087 | 165° | 6.94 | -0.032 | -0.028 | -0.023 | -0.018 | 0.003 | 0.047 | 0.23 |
| | 8.37 | -0.28 | -0.028 | -0.034 | -0.056 | -0.084 | -0.083 | -0.086 | | 8.37 | -0.023 | -0.019 | -0.013 | -0.008 | 0.000 | 0.047 | 0.23 |
| | 9.81 | -0.28 | -0.028 | -0.034 | -0.056 | -0.079 | -0.082 | -0.086 | | 9.81 | -0.020 | -0.016 | -0.010 | -0.005 | 0.000 | 0.047 | 0.23 |
| | 11.25 | -0.16 | -0.016 | -0.029 | -0.071 | -0.061 | -0.076 | -0.088 | | 11.25 | -0.017 | -0.016 | -0.011 | -0.006 | 0.000 | 0.047 | 0.23 |
| | 12.69 | -0.16 | -0.016 | -0.026 | -0.071 | -0.066 | -0.074 | -0.088 | | 12.69 | -0.017 | -0.016 | -0.011 | -0.006 | 0.000 | 0.047 | 0.23 |
| | 14.13 | -0.10 | -0.010 | -0.028 | -0.066 | -0.068 | -0.070 | -0.080 | | 14.13 | -0.017 | -0.017 | -0.011 | -0.006 | 0.000 | 0.047 | 0.23 |
| | 15.56 | -0.09 | -0.009 | -0.021 | -0.059 | -0.064 | -0.069 | -0.079 | | 15.56 | -0.007 | -0.007 | -0.004 | -0.003 | 0.000 | 0.047 | 0.23 |
| | 17.00 | -0.006 | -0.006 | -0.024 | -0.039 | -0.058 | -0.065 | -0.074 | | 17.00 | -0.003 | -0.003 | -0.003 | -0.002 | 0.006 | 0.047 | 0.23 |
| 60° | 6.94 | -0.31 | -0.41 | -0.54 | -0.78 | -0.80 | -0.84 | -0.87 | 174° | 6.94 | -0.031 | -0.14 | 0.03 | 0.36 | 1.14 | 1.64 | 1.94 |
| | 8.37 | -0.29 | -0.37 | -0.54 | -0.70 | -0.88 | -0.84 | -0.86 | | 8.37 | -0.023 | -0.16 | 0.09 | 0.40 | 1.04 | 1.56 | 1.70 |
| | 9.81 | -0.26 | -0.32 | -0.46 | -0.59 | -0.70 | -0.76 | -0.88 | | 9.81 | -0.018 | -0.16 | 0.09 | 0.39 | 1.04 | 1.55 | 1.63 |
| | 11.25 | -0.19 | -0.28 | -0.38 | -0.55 | -0.67 | -0.76 | -0.80 | | 11.25 | -0.015 | -0.16 | 0.09 | 0.38 | 1.04 | 1.55 | 1.63 |
| | 12.69 | -0.16 | -0.26 | -0.30 | -0.48 | -0.64 | -0.73 | -0.79 | | 12.69 | -0.015 | -0.16 | 0.09 | 0.38 | 1.04 | 1.55 | 1.63 |
| | 14.13 | -0.13 | -0.19 | -0.26 | -0.44 | -0.60 | -0.70 | -0.76 | | 14.13 | -0.014 | -0.16 | 0.09 | 0.38 | 1.04 | 1.55 | 1.63 |
| | 15.56 | -0.09 | -0.14 | -0.23 | -0.33 | -0.58 | -0.64 | -0.74 | | 15.56 | -0.008 | -0.16 | 0.09 | 0.37 | 1.04 | 1.54 | 1.62 |
| | 17.00 | -0.04 | -0.07 | -0.17 | -0.33 | -0.58 | -0.63 | -0.74 | | 17.00 | -0.004 | -0.16 | 0.09 | 0.37 | 1.04 | 1.54 | 1.62 |
| 90° | 6.94 | -0.31 | -0.41 | -0.54 | -0.78 | -0.80 | -0.84 | -0.87 | 90° | 6.94 | -0.031 | -0.14 | 0.03 | 0.36 | 1.14 | 1.64 | 1.94 |
| | 8.37 | -0.29 | -0.37 | -0.54 | -0.70 | -0.88 | -0.84 | -0.86 | | 8.37 | -0.023 | -0.16 | 0.09 | 0.40 | 1.04 | 1.56 | 1.70 |
| | 9.81 | -0.26 | -0.32 | -0.46 | -0.59 | -0.70 | -0.76 | -0.88 | | 9.81 | -0.018 | -0.16 | 0.09 | 0.39 | 1.04 | 1.55 | 1.63 |
| | 11.25 | -0.19 | -0.28 | -0.38 | -0.55 | -0.67 | -0.76 | -0.80 | | 11.25 | -0.015 | -0.16 | 0.09 | 0.38 | 1.04 | 1.55 | 1.63 |
| | 12.69 | -0.16 | -0.26 | -0.30 | -0.48 | -0.64 | -0.73 | -0.79 | | 12.69 | -0.015 | -0.16 | 0.09 | 0.38 | 1.04 | 1.55 | 1.63 |
| | 14.13 | -0.13 | -0.19 | -0.26 | -0.44 | -0.60 | -0.70 | -0.76 | | 14.13 | -0.014 | -0.16 | 0.09 | 0.38 | 1.04 | 1.55 | 1.63 |
| | 15.56 | -0.09 | -0.14 | -0.23 | -0.33 | -0.58 | -0.64 | -0.74 | | 15.56 | -0.008 | -0.16 | 0.09 | 0.37 | 1.04 | 1.54 | 1.62 |
| | 17.00 | -0.04 | -0.07 | -0.14 | -0.29 | -0.47 | -0.61 | -0.65 | | 17.00 | -0.004 | -0.16 | 0.09 | 0.37 | 1.04 | 1.54 | 1.62 |



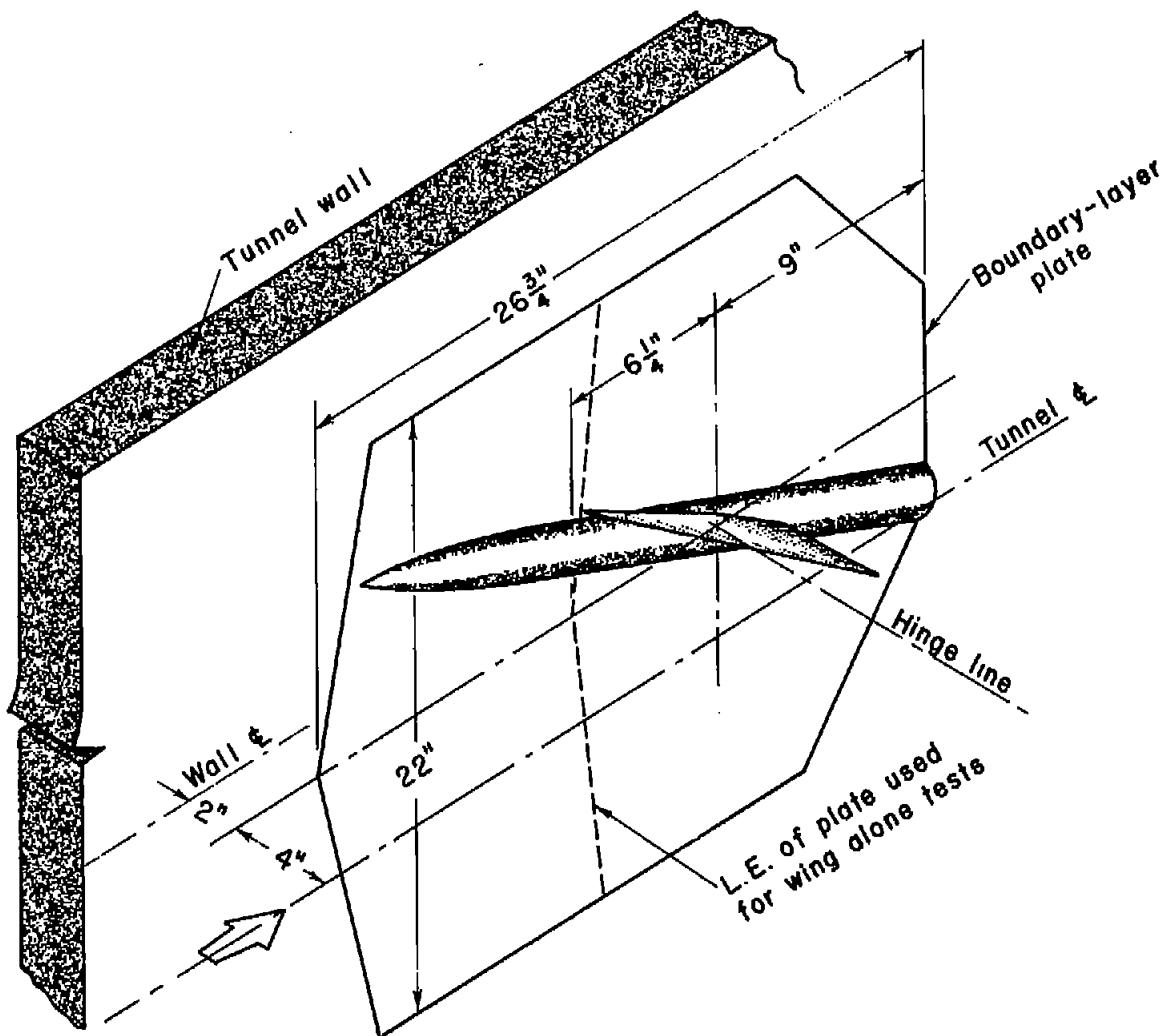
| Triangular plan forms | | | | | | | | |
|-----------------------|---------------|-----|------|----------|-------------------|-------------|---------------|-----------|
| Model | A | r/s | s in | c_r in | S in ² | t/c_{max} | $x/c@t_{max}$ | Wing test |
| | 4 | .2 | 5 | 4 | 8 | .05 | .50 | press. |
| | 2 | .2 | 5 | 8 | 16 | .05 | .50 | press. |
| | 1 | .2 | 5 | 16 | 32 | .04 | .59 | force |
| | 1 | .4 | 2.5 | 6 | 4.5 | .04 | .59 | force |
| | $\frac{2}{3}$ | .4 | 2.5 | 9 | 6.75 | .04 | .59 | force |
| | $\frac{3}{8}$ | .4 | 2.5 | 16 | 12 | .04 | .59 | force |

| Rectangular plan forms | | | | | | | | |
|------------------------|---|----|-----|------|--------|-----|-----|--------|
| | 3 | .2 | 5 | 2667 | 10.667 | .04 | .59 | force |
| | 2 | .2 | 5 | 4 | 16 | .05 | .50 | press. |
| | 1 | .2 | 5 | 8 | 32 | .04 | .59 | force |
| | 1 | .4 | 2.5 | 3 | 4.5 | .04 | .59 | force |

* Plan form for $7/16$ scale full-span models.

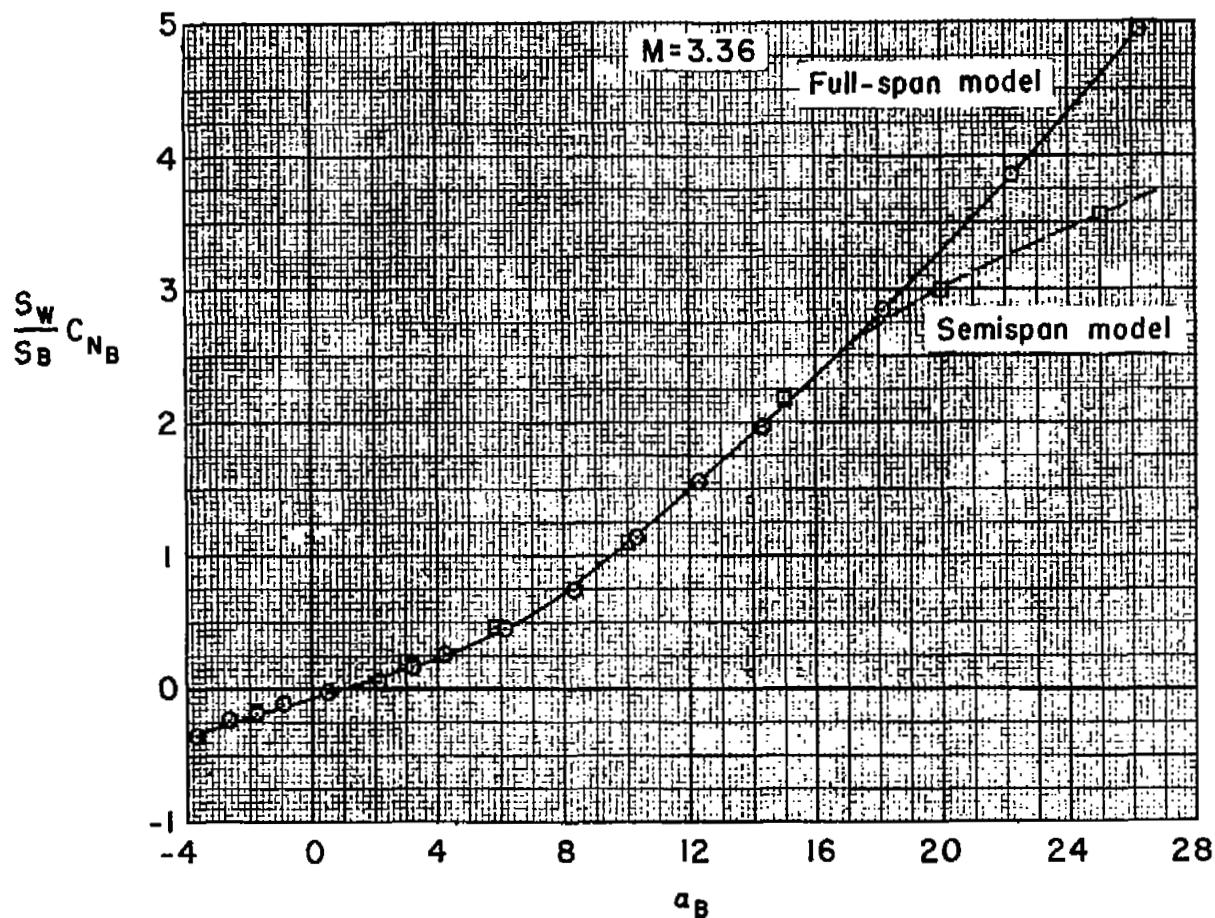
(a) Summary of model geometry and dimensions.

Figure 1.- Models and semispan supports.



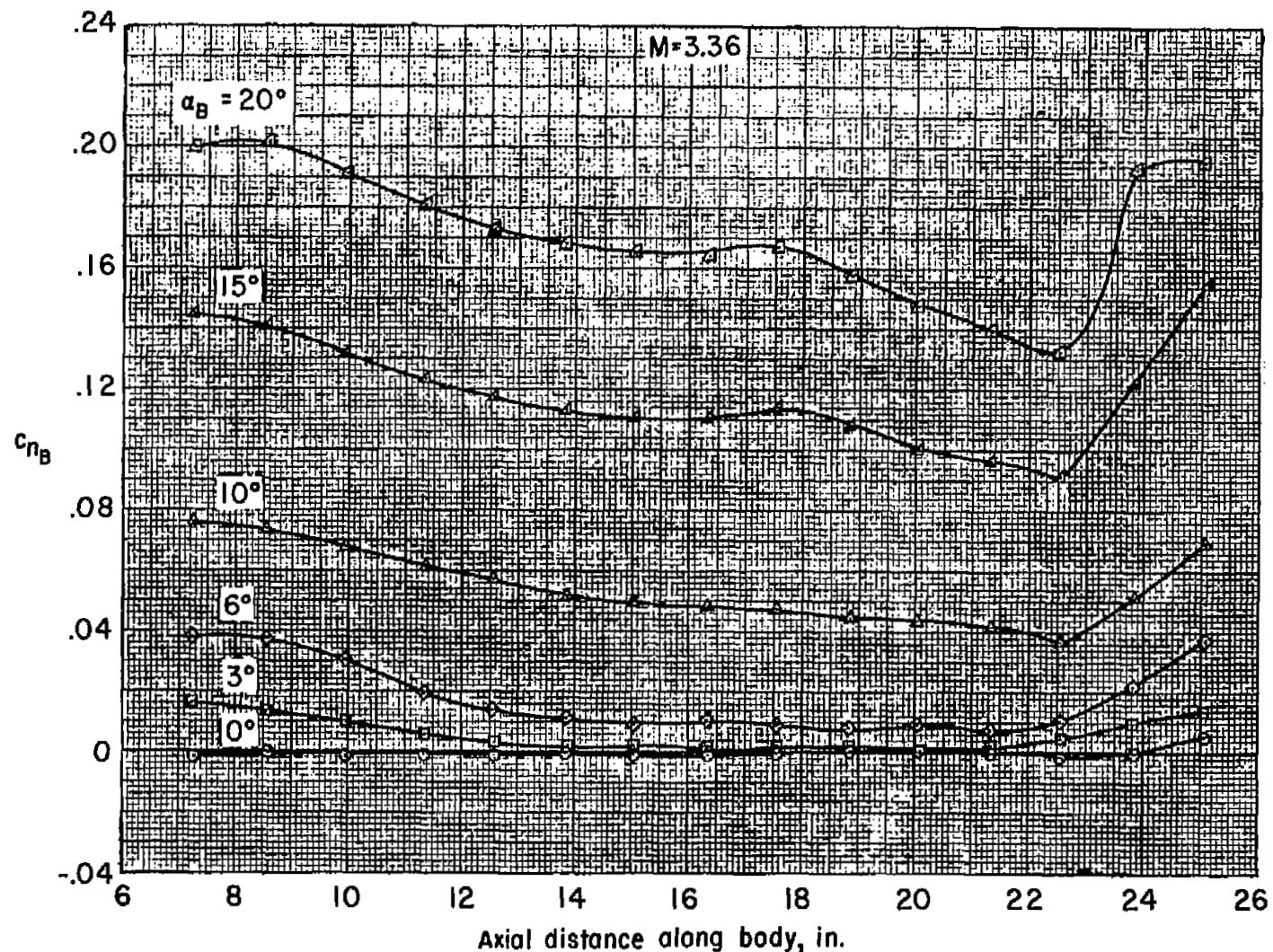
(b) Semispan model installation.

Figure 1.- Concluded.



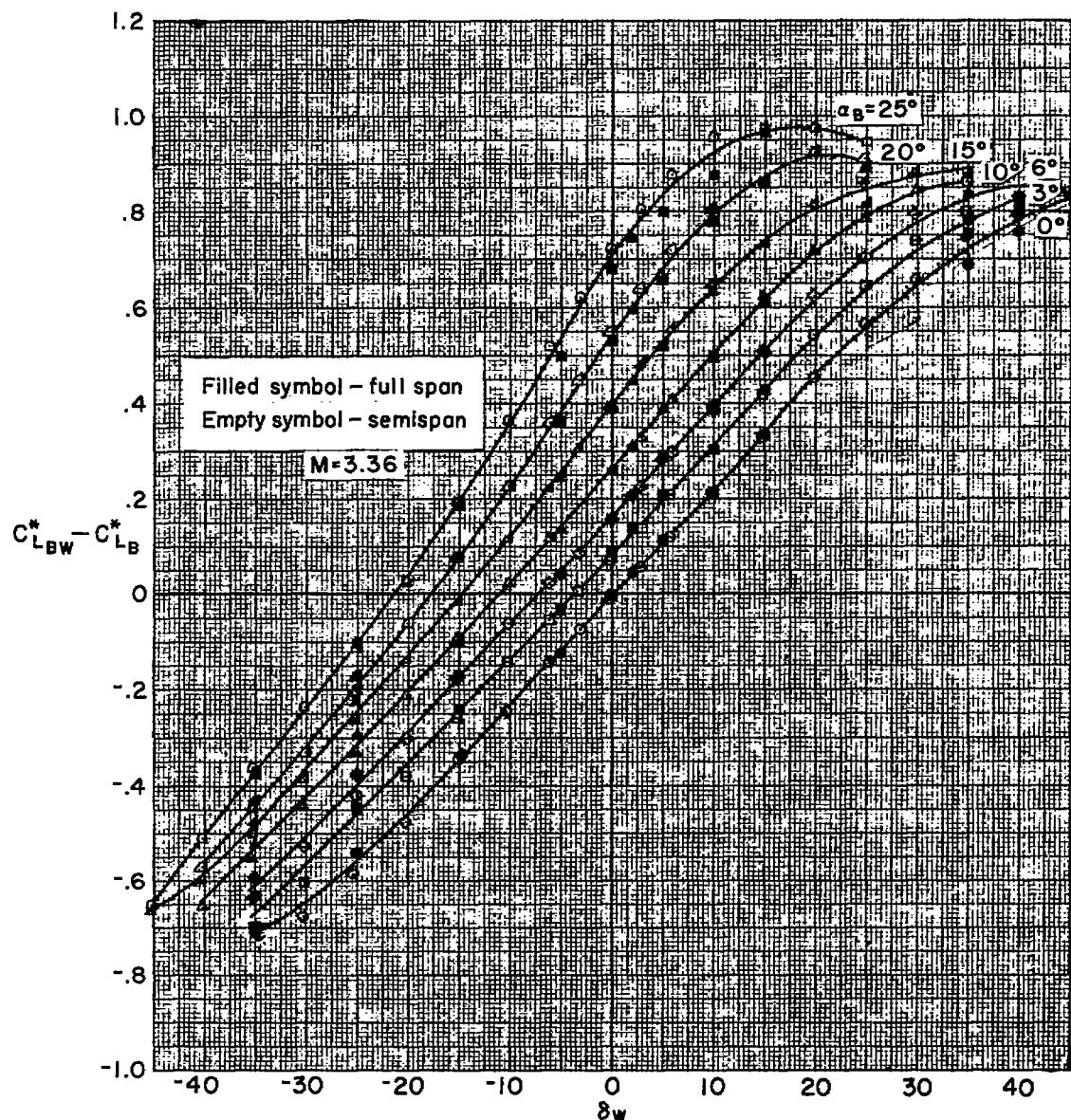
(a) Comparison of the variation of normal-force coefficient with angle of attack for the half body and full body.

Figure 2.- Body alone characteristics.



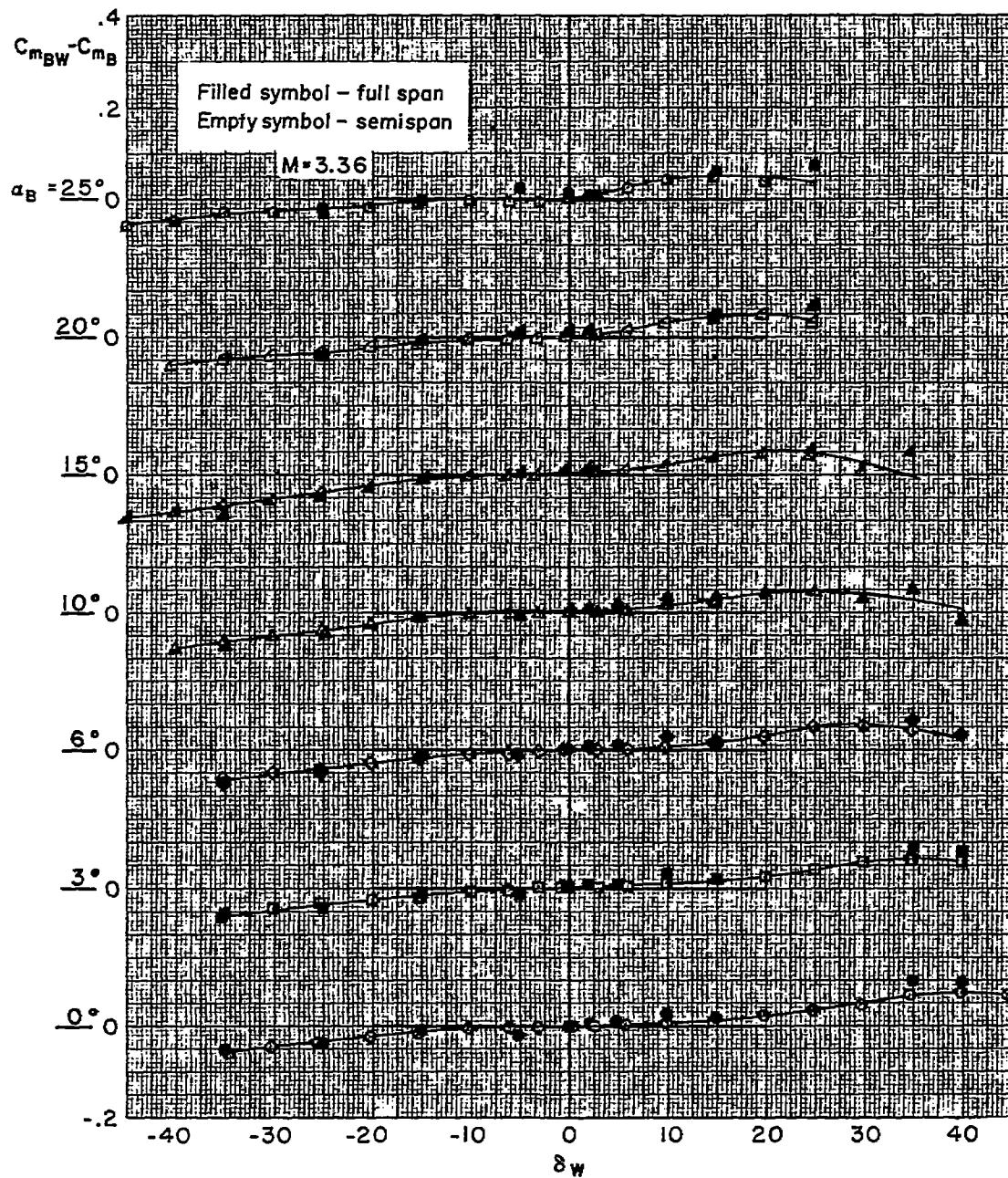
(b) Local normal-force coefficients at several angles of attack for half body.

Figure 2.- Concluded.



- (a) Variation with wing deflection angle of normal-force coefficient for the $A = 1$ rectangular wing and body combination minus that for body alone.

Figure 3.- Comparison of semispan and full-span model data.



- (b) Variation with wing deflection angle of the pitching-moment coefficient for the $A = 1$ rectangular wing and body combination minus that for the body alone.

Figure 3.- Concluded.

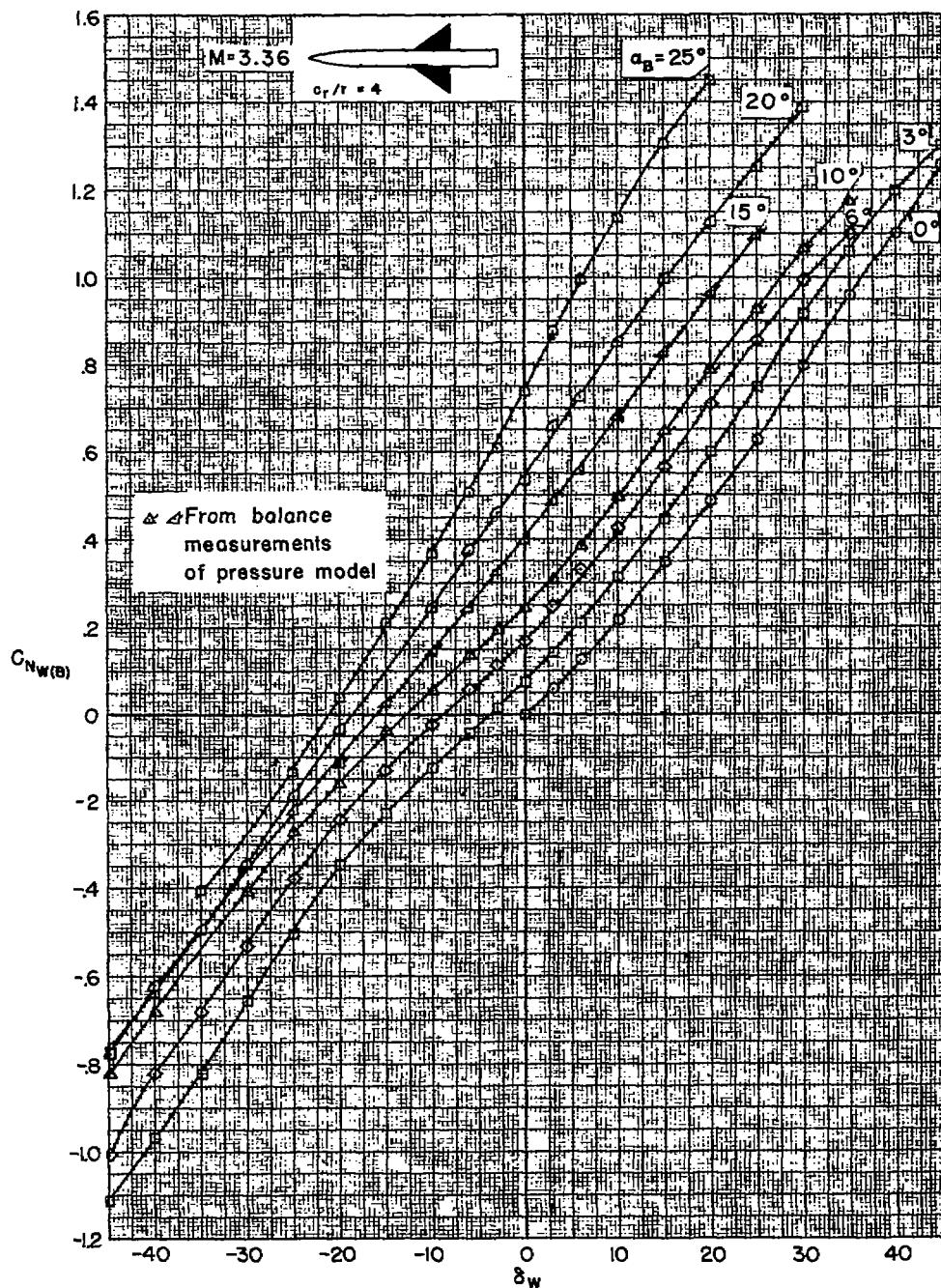
(a) $A = 4$ triangular wing, $r/s = 0.2$.

Figure 4.- Variation with deflection angle of normal-force coefficient for the wings in the presence of the body.

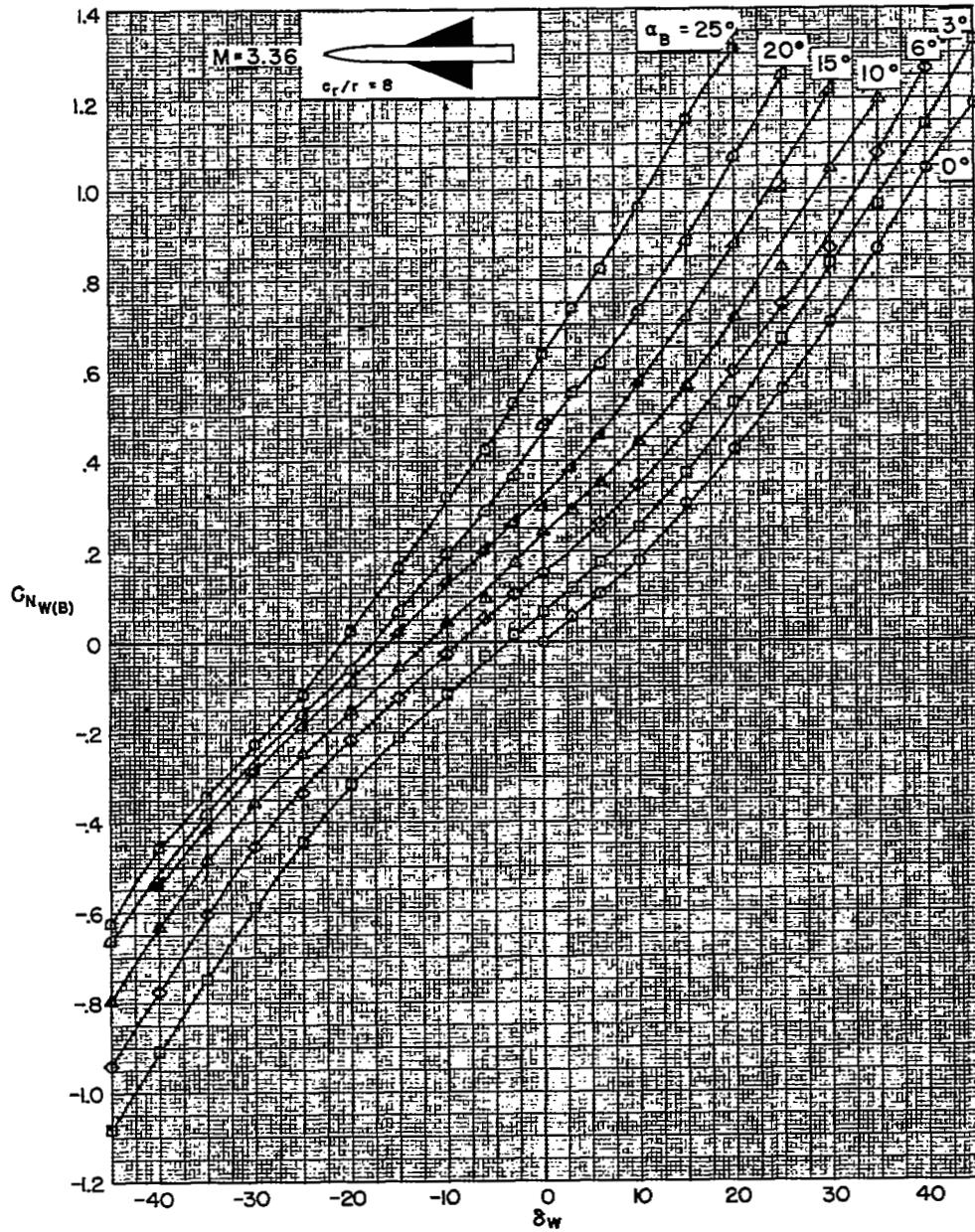
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 4.- Continued.

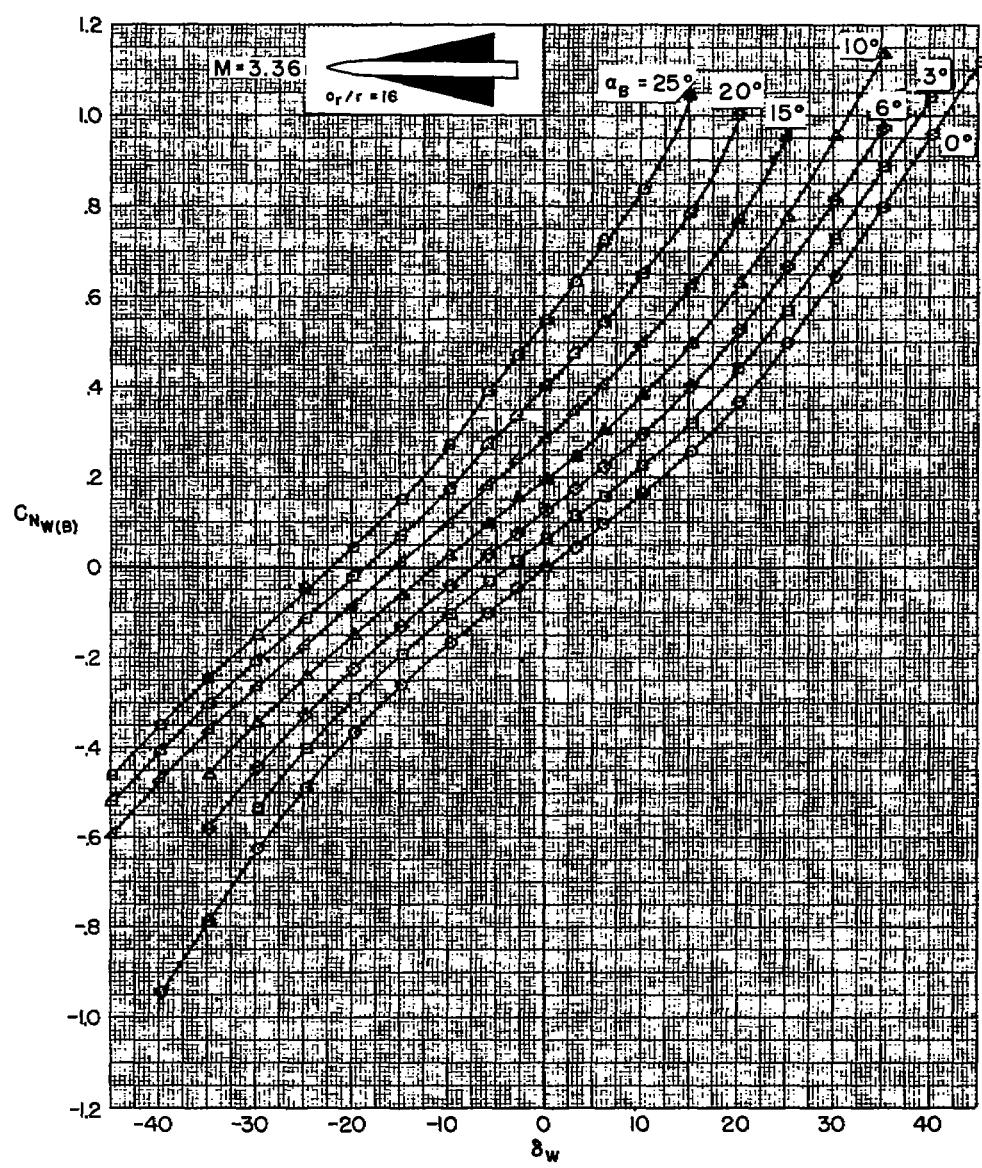
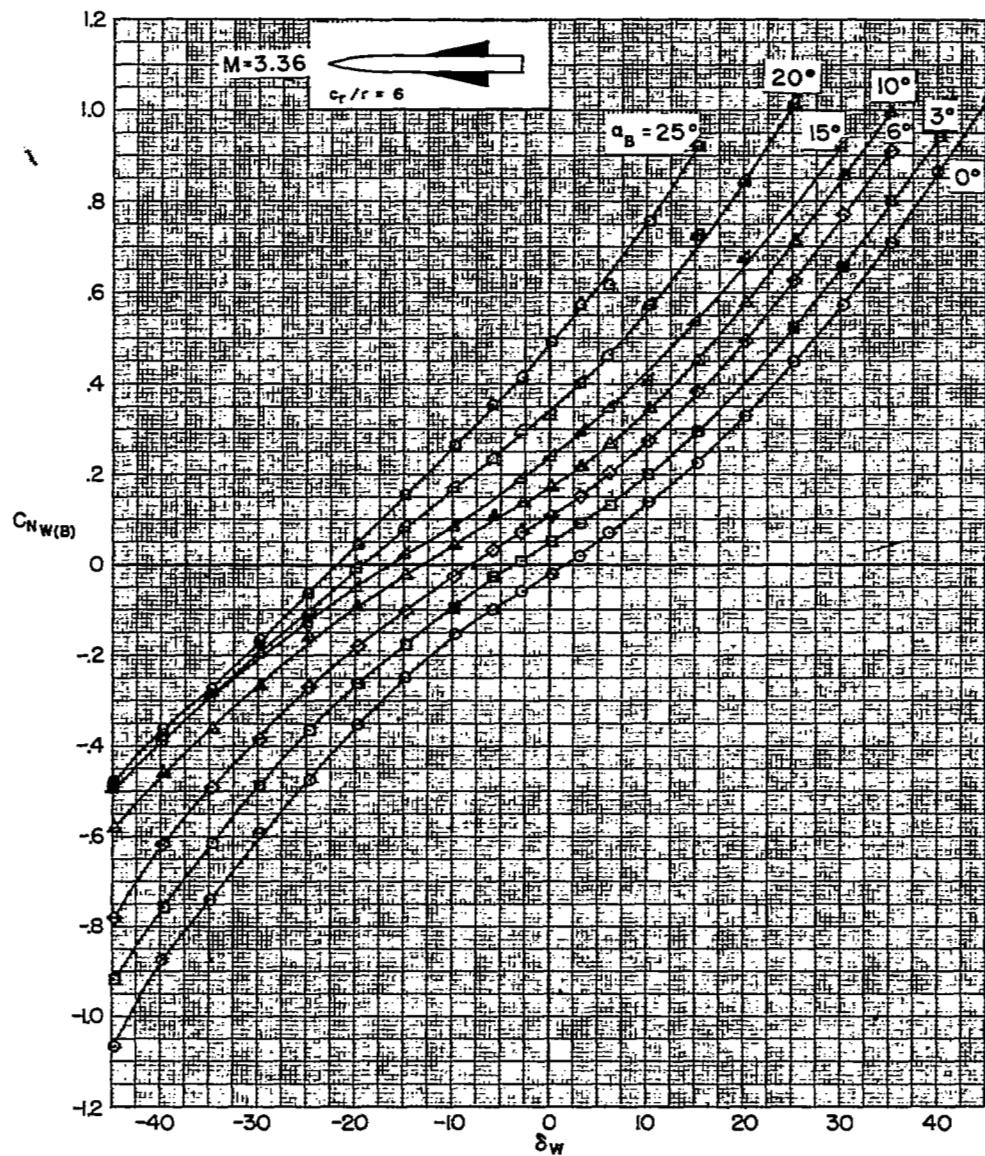
(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 4.- Continued.



(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 4.- Continued.

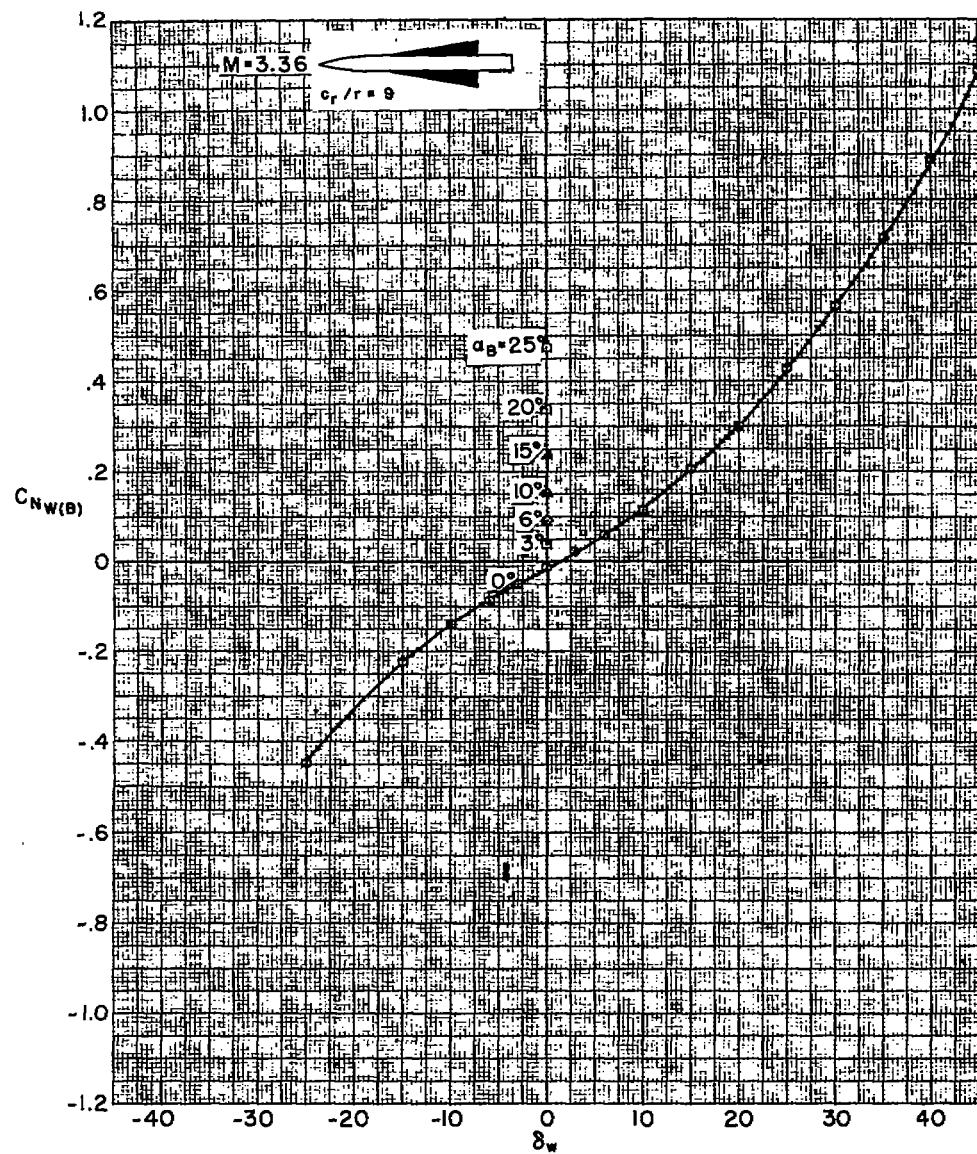
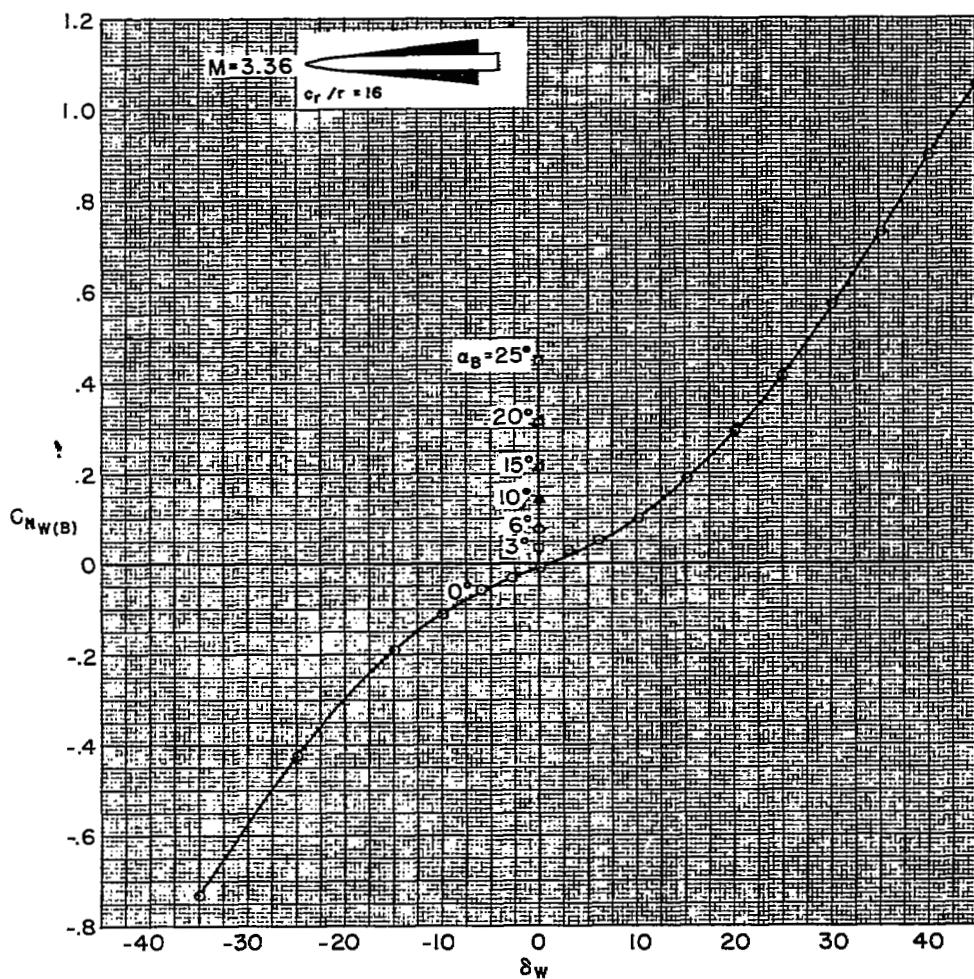
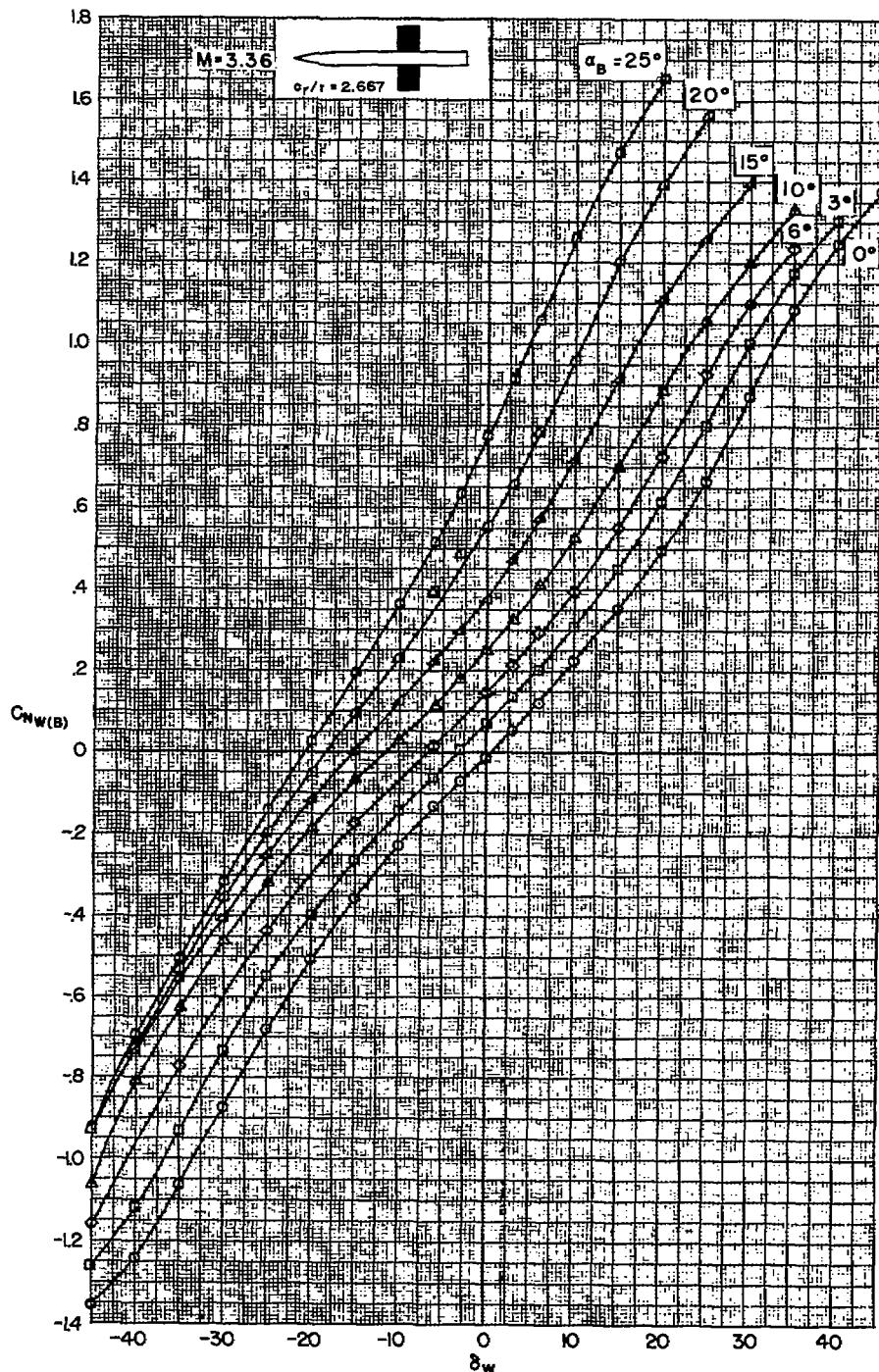
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.

Figure 4.- Continued.



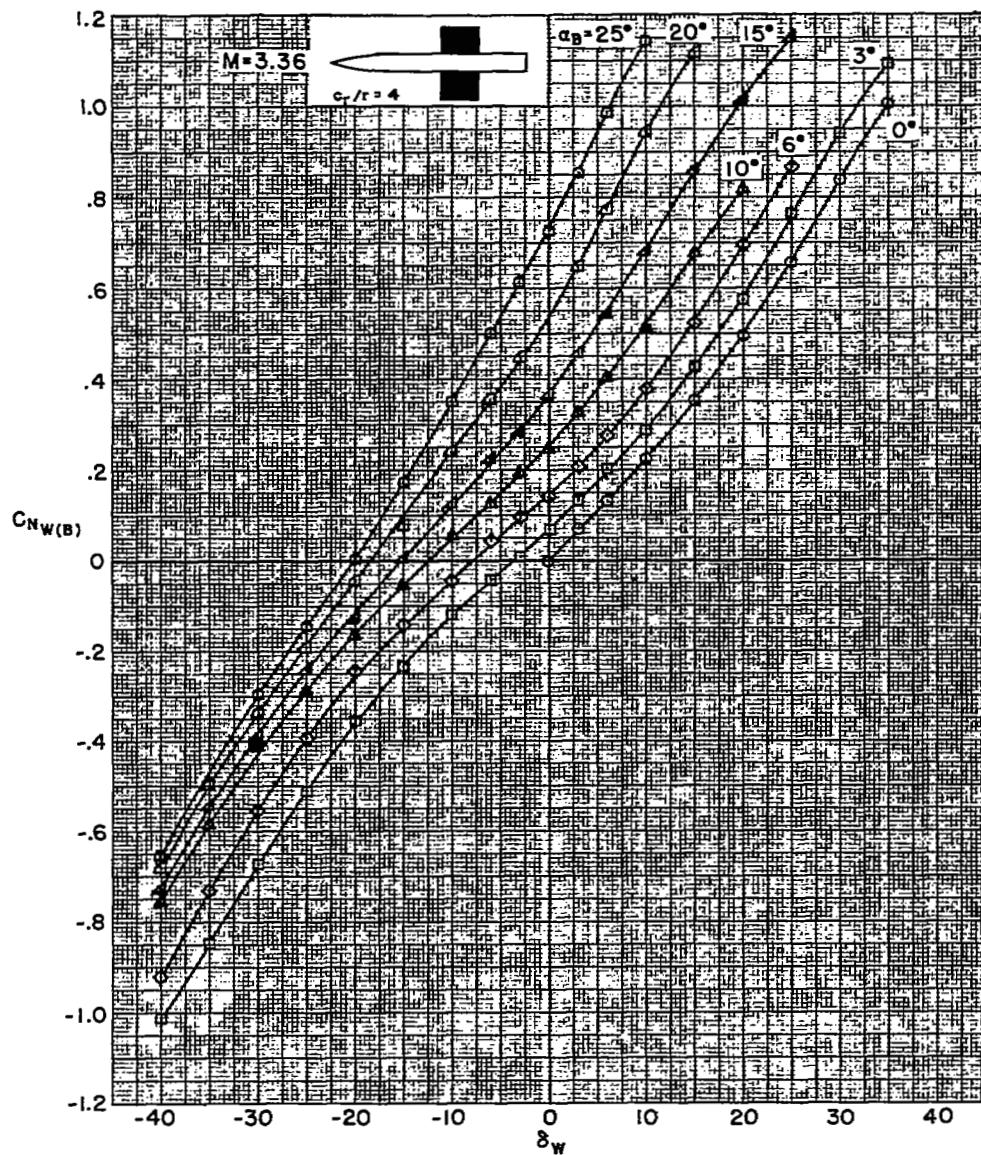
(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 4.- Continued.



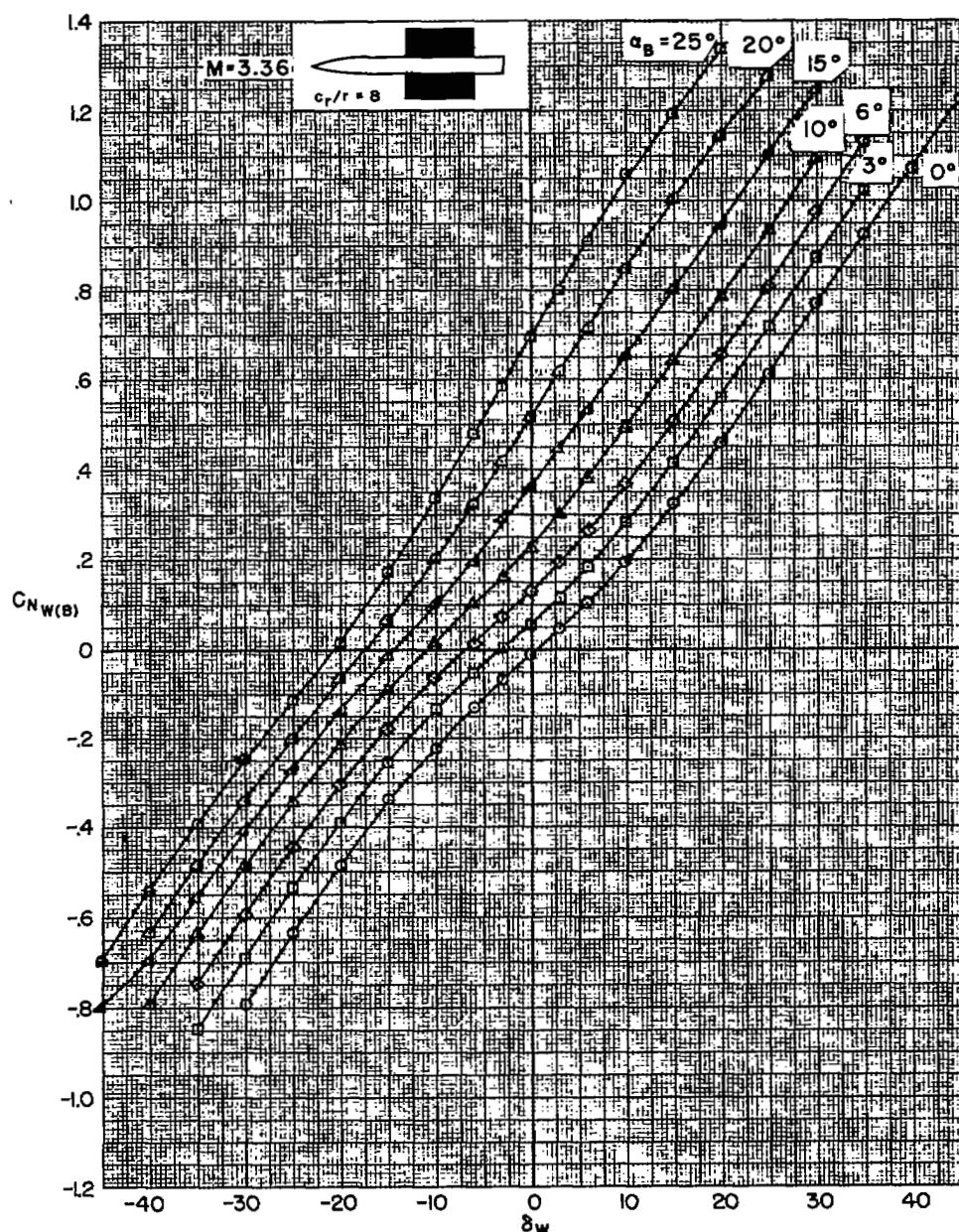
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 4.- Continued.



(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 4.- Continued.



(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 4.- Continued.

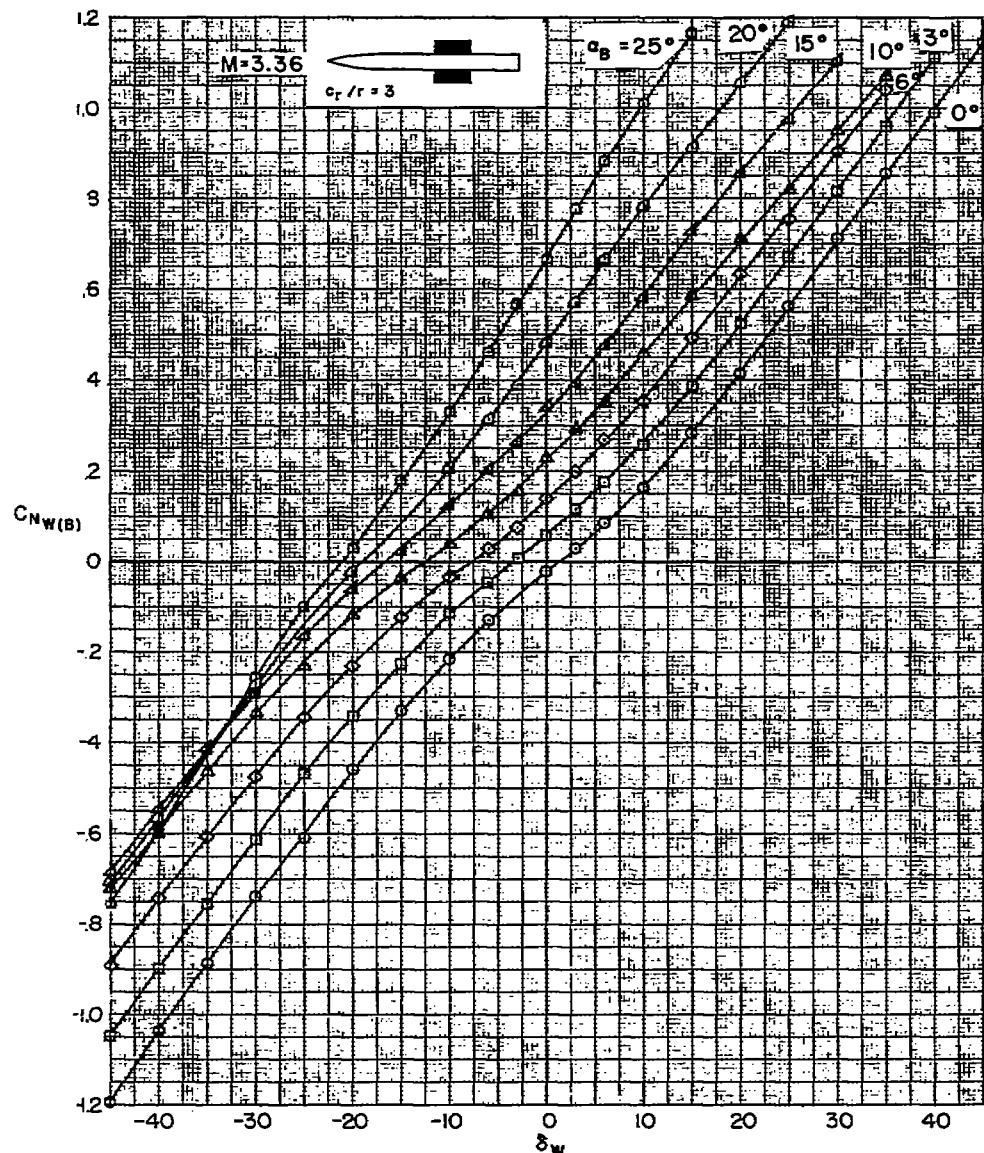
(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 4.- Concluded.

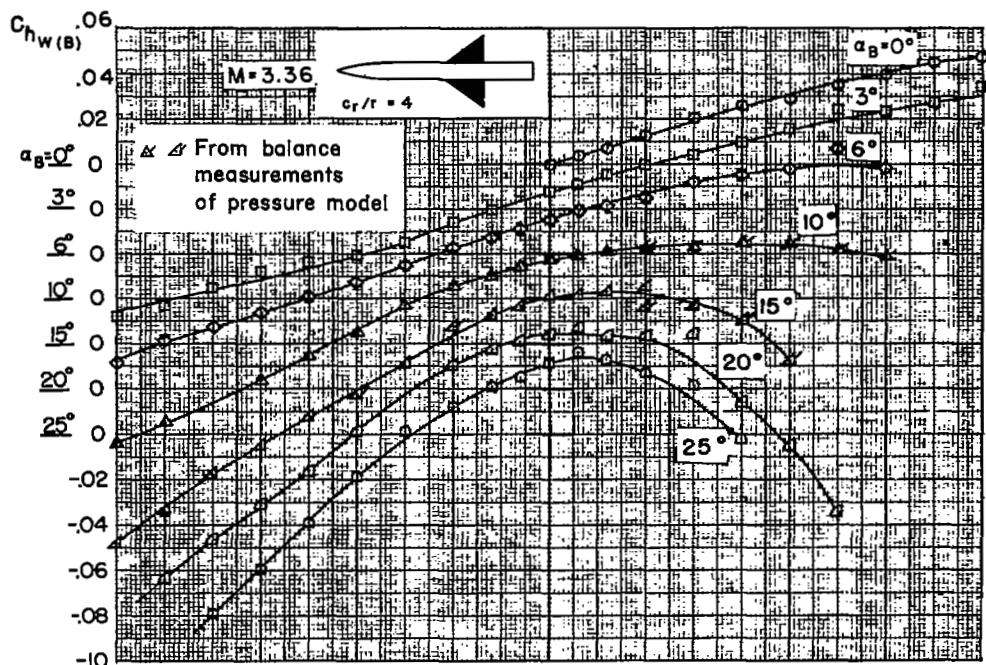
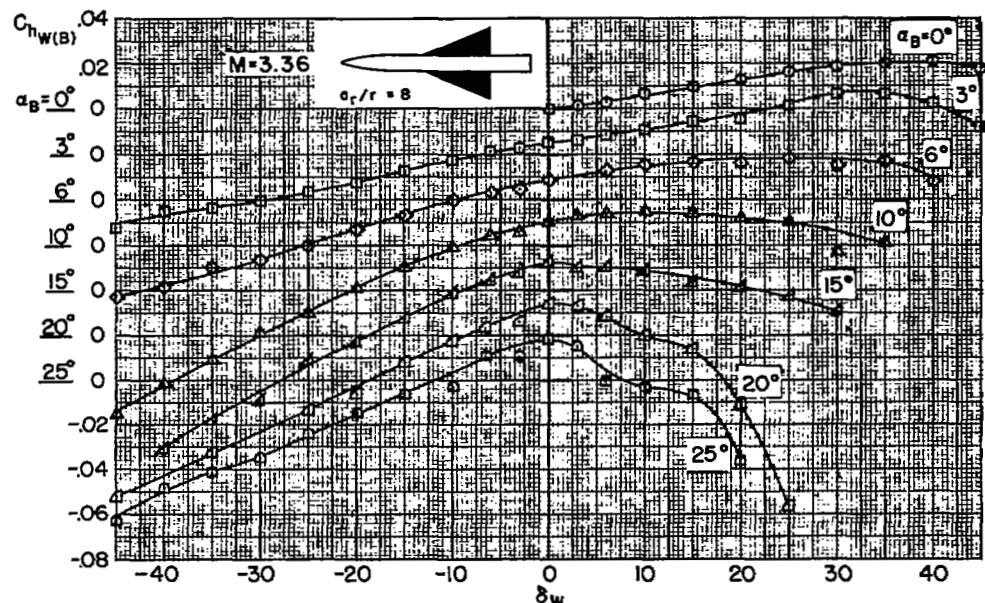
(a) $A = 4$ triangular wing, $r/s = 0.2$.(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 5.- Variation with deflection angle of hinge-moment coefficient for the wings in the presence of the body.

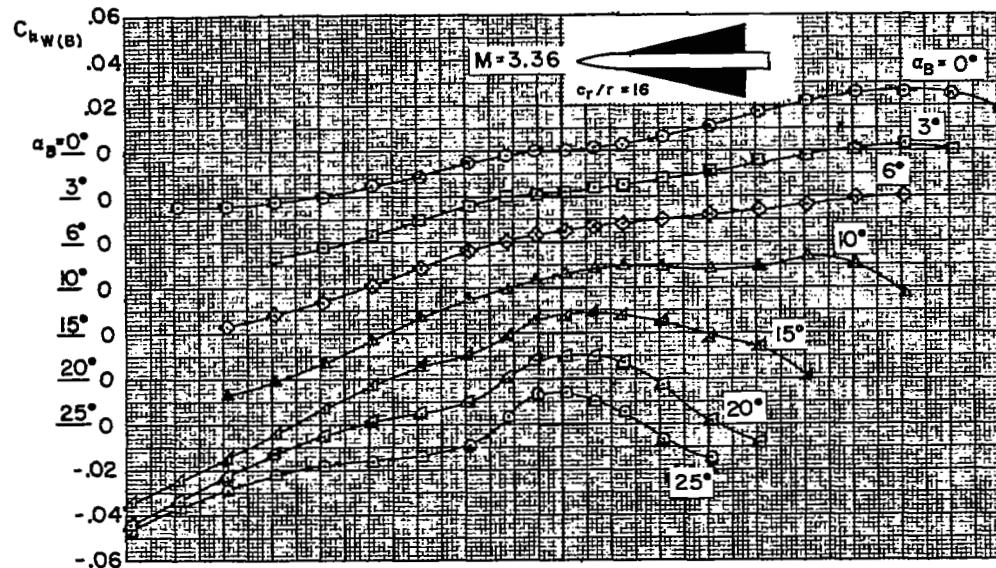
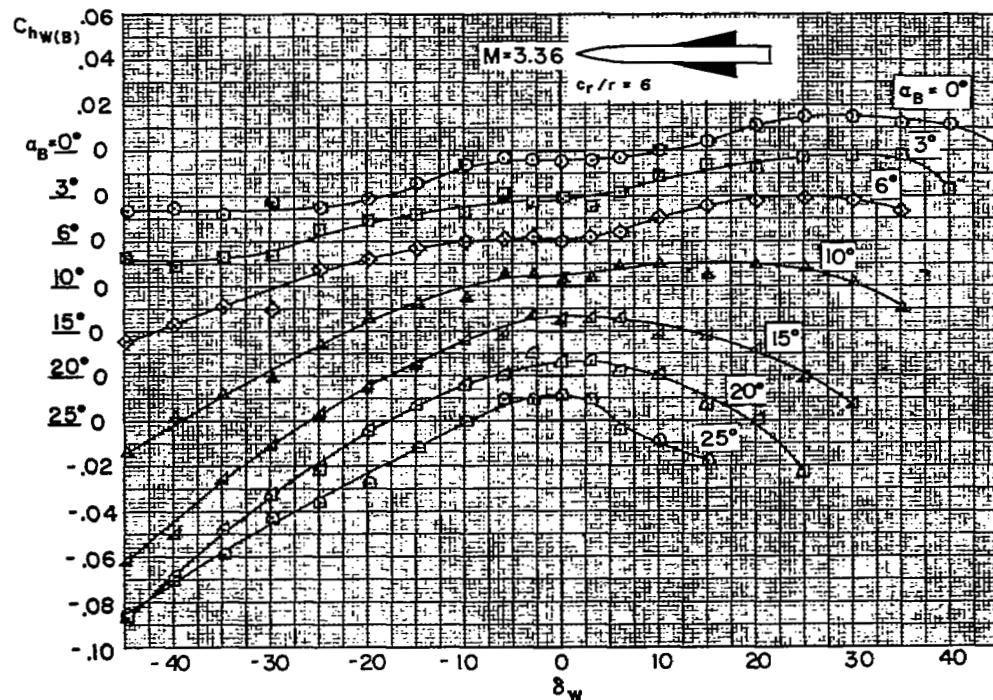
(c) $A = 1$ triangular wing, $r/s = 0.2$.(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 5.- Continued.

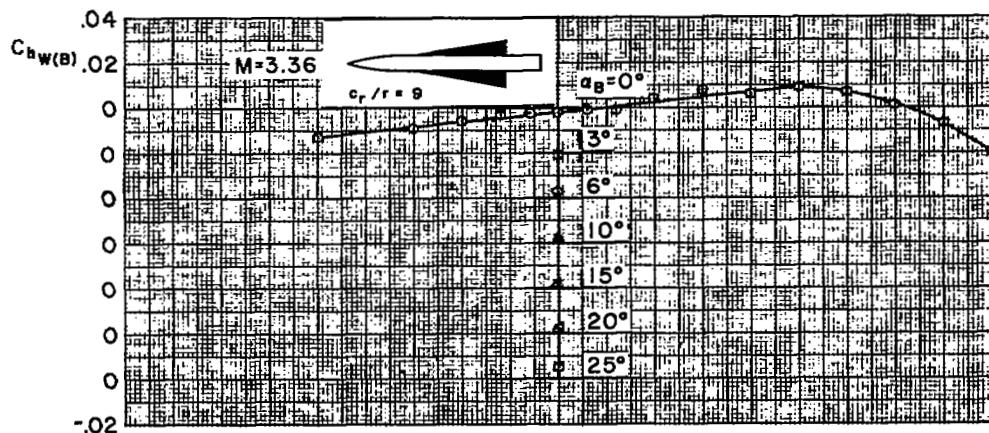
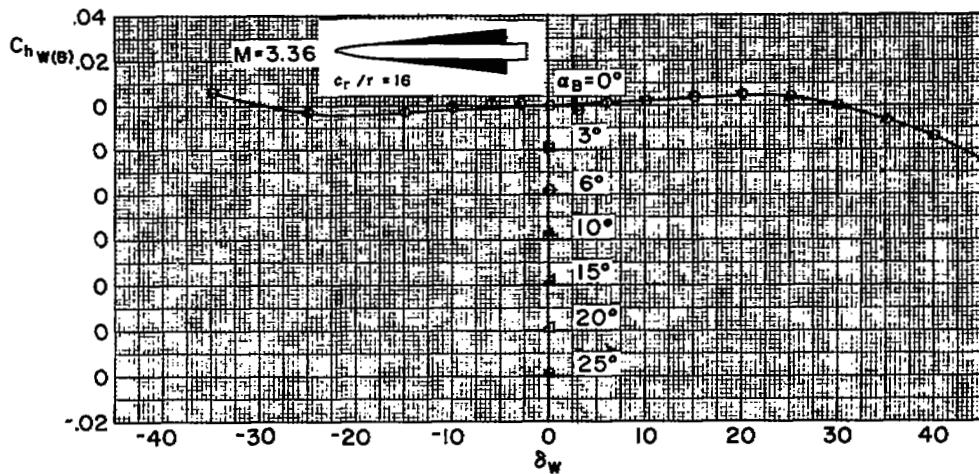
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 5.- Continued.

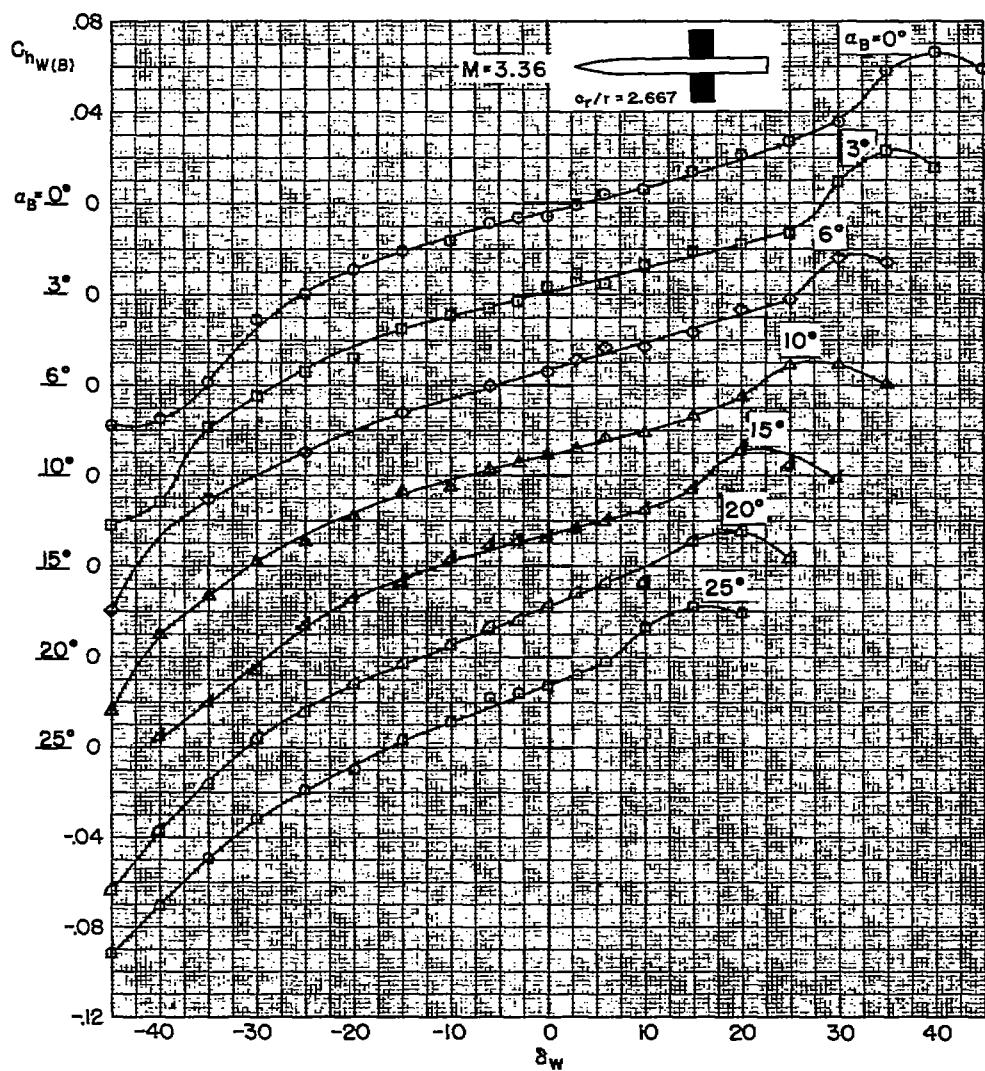
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 5.- Continued.

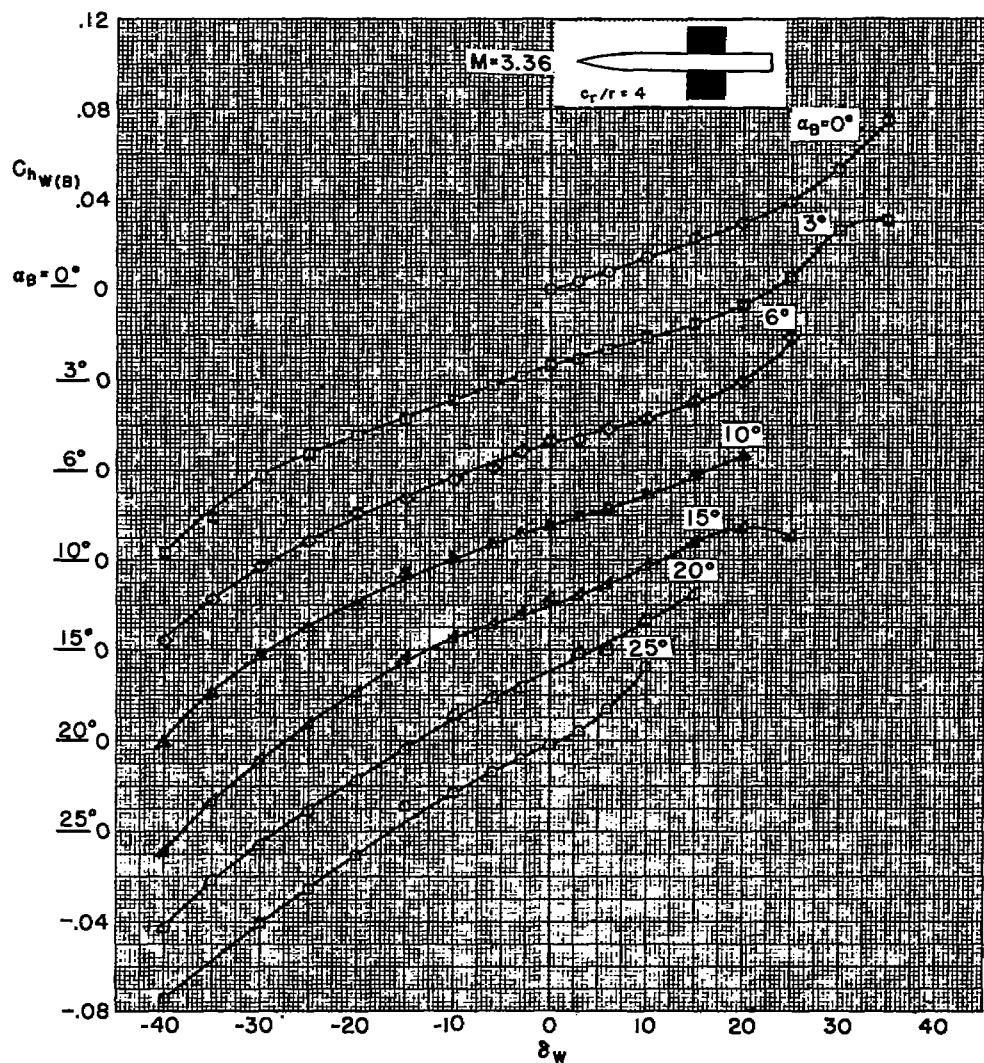
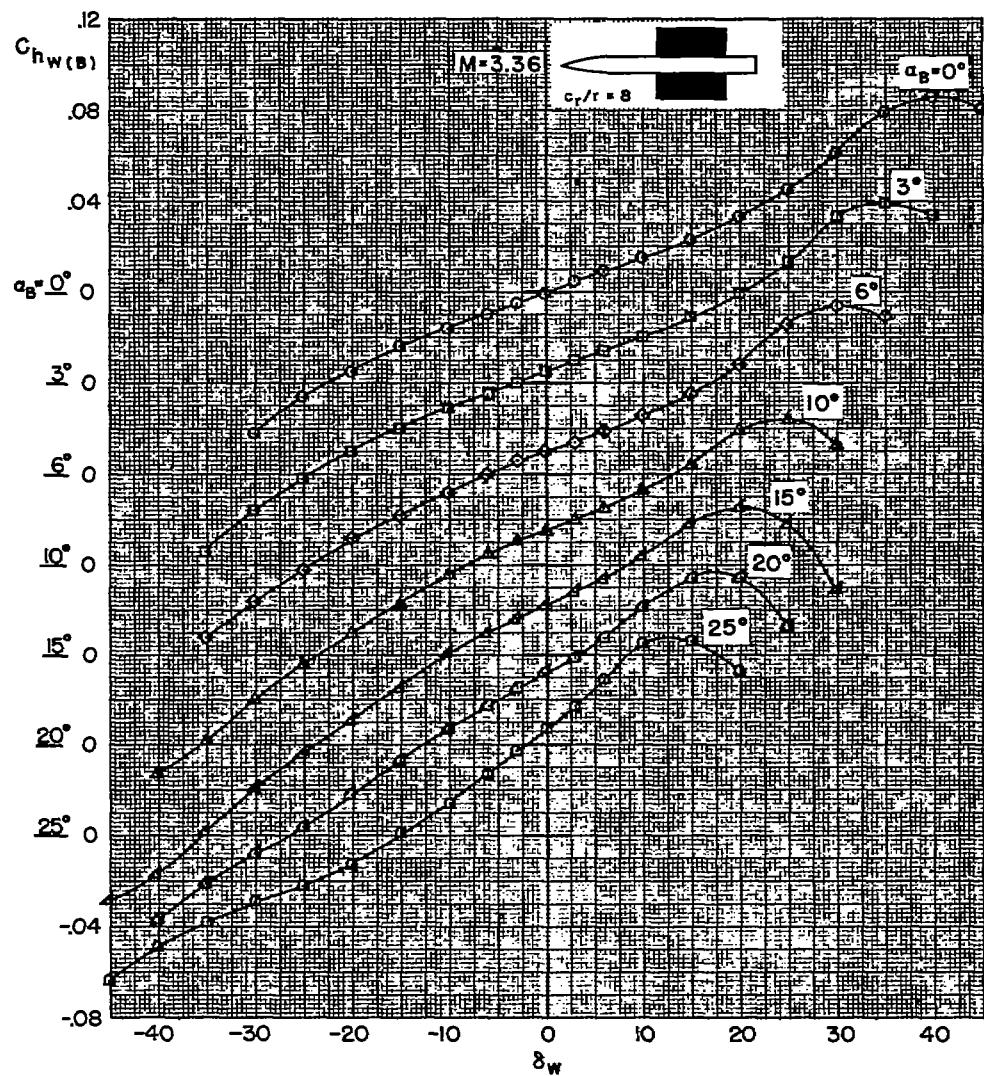
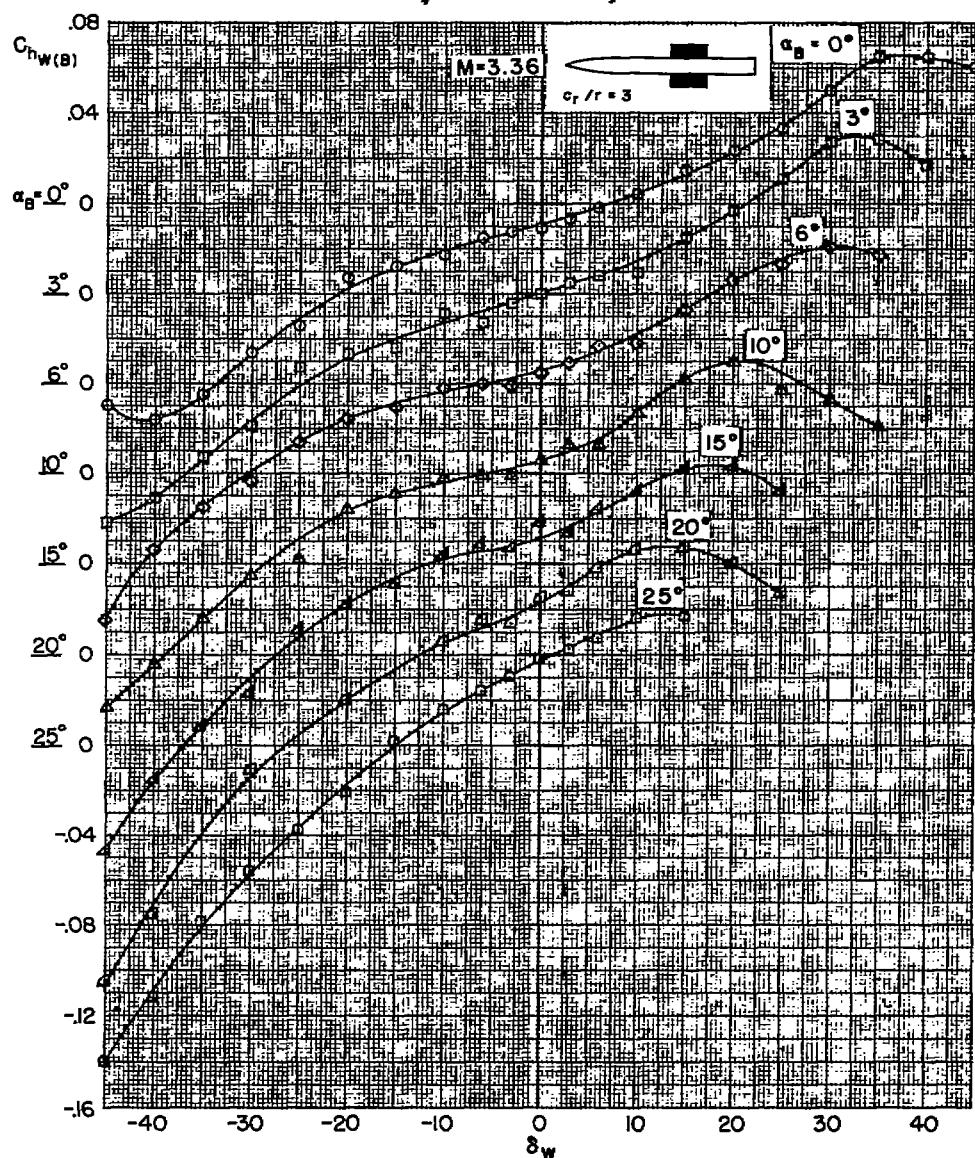
(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 5.- Continued.



(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 5.- Continued.



(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 5.- Concluded.

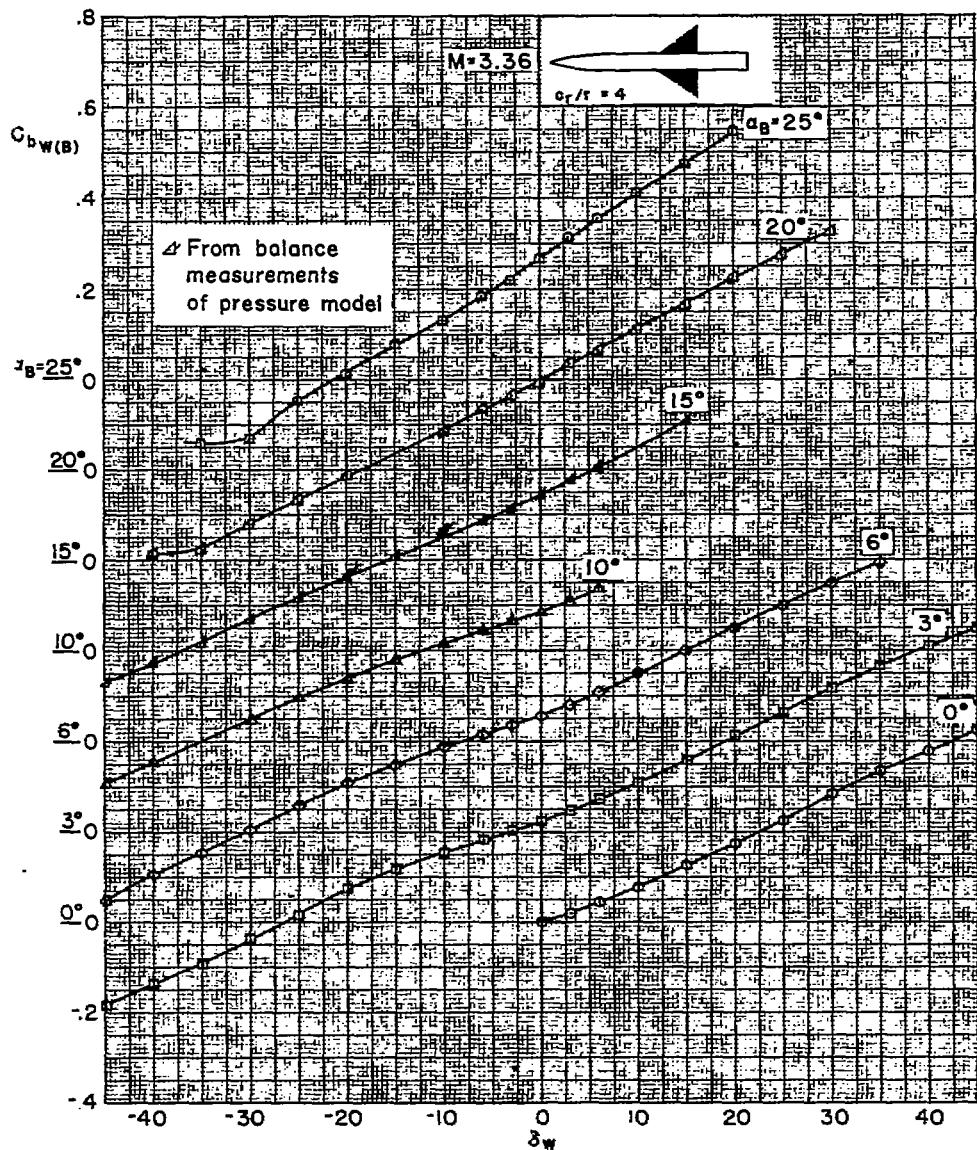
(a) $A = 4$ triangular wing, $r/s 0.2$.

Figure 6.- Variation with deflection angle of bending-moment coefficient for the wings in the presence of the body.

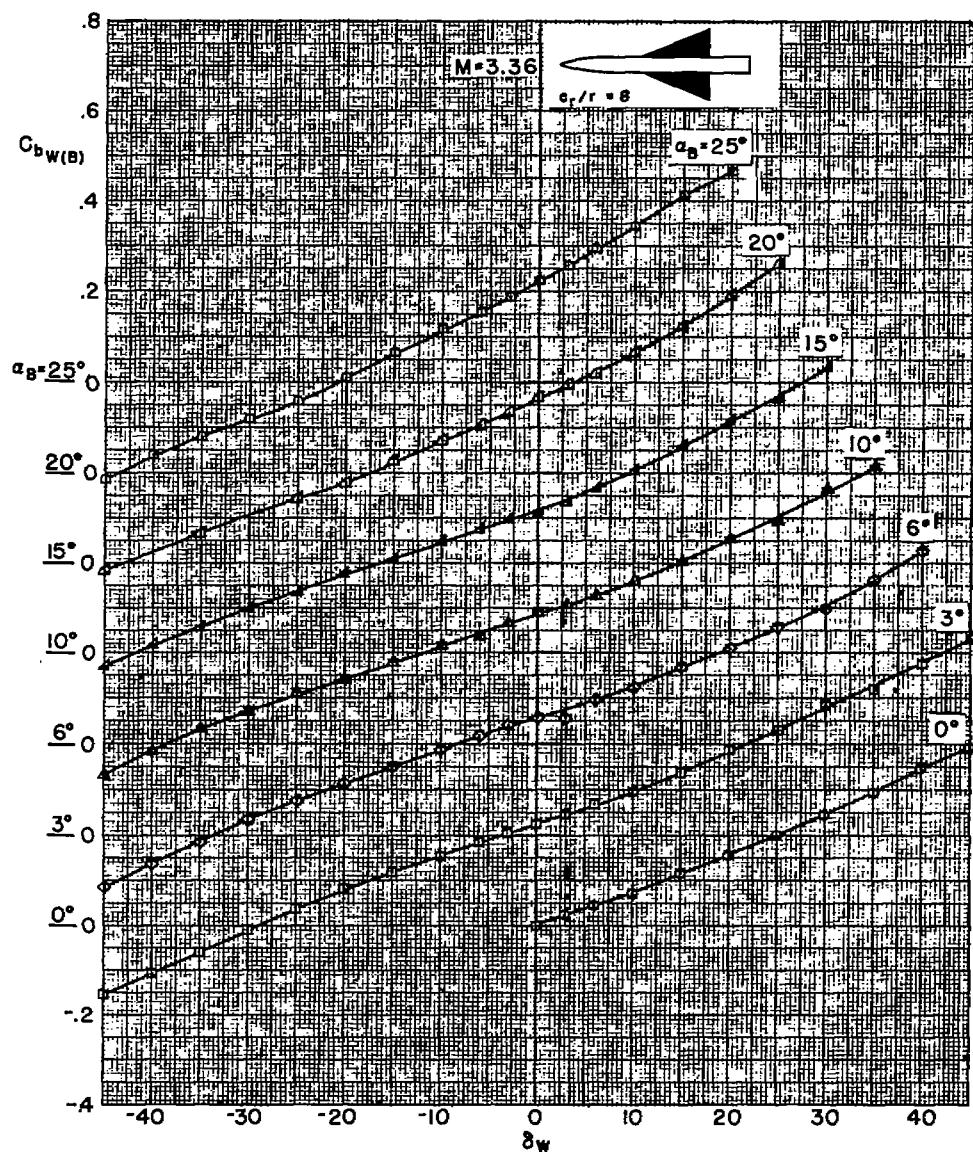
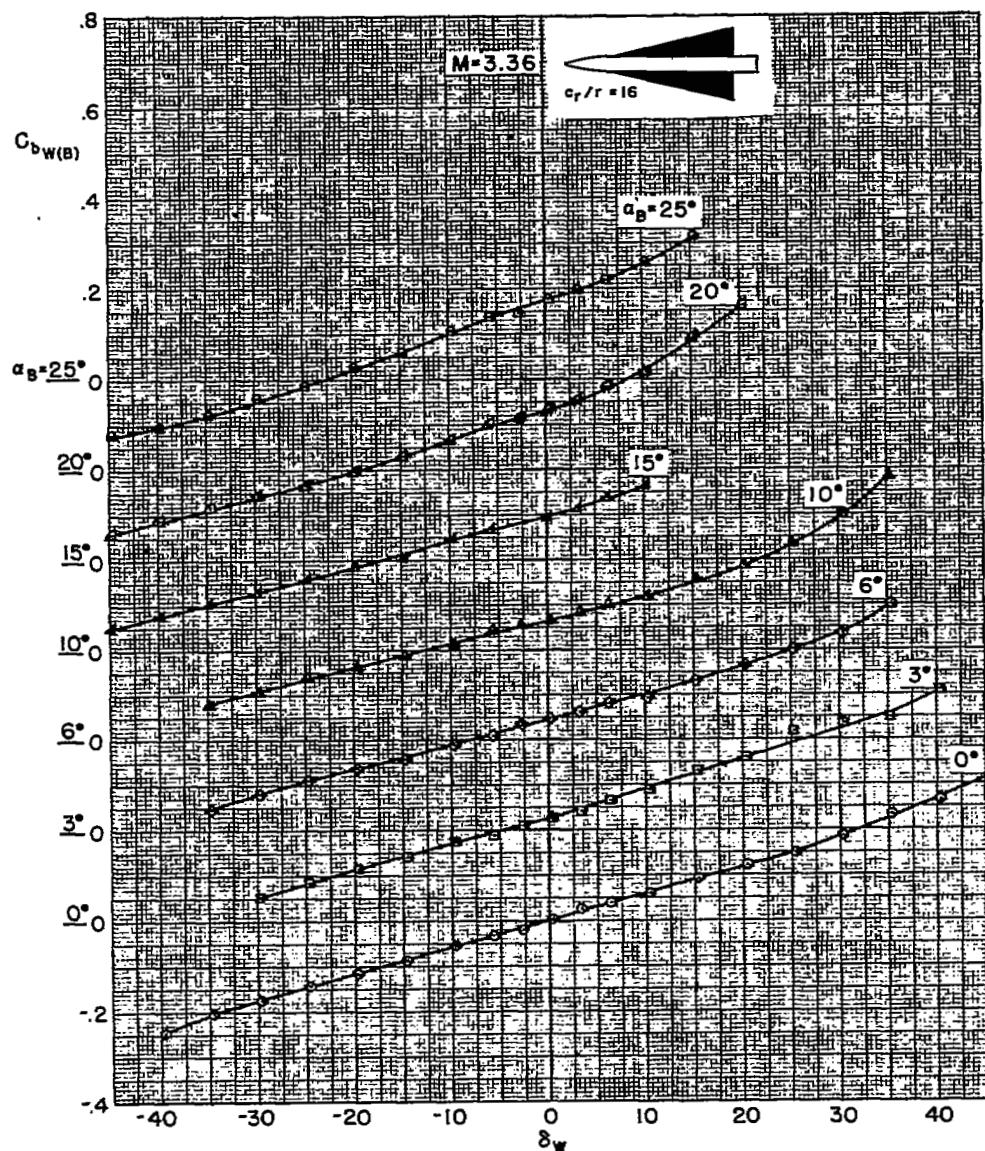
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 6.- Continued.



(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 6.- Continued.

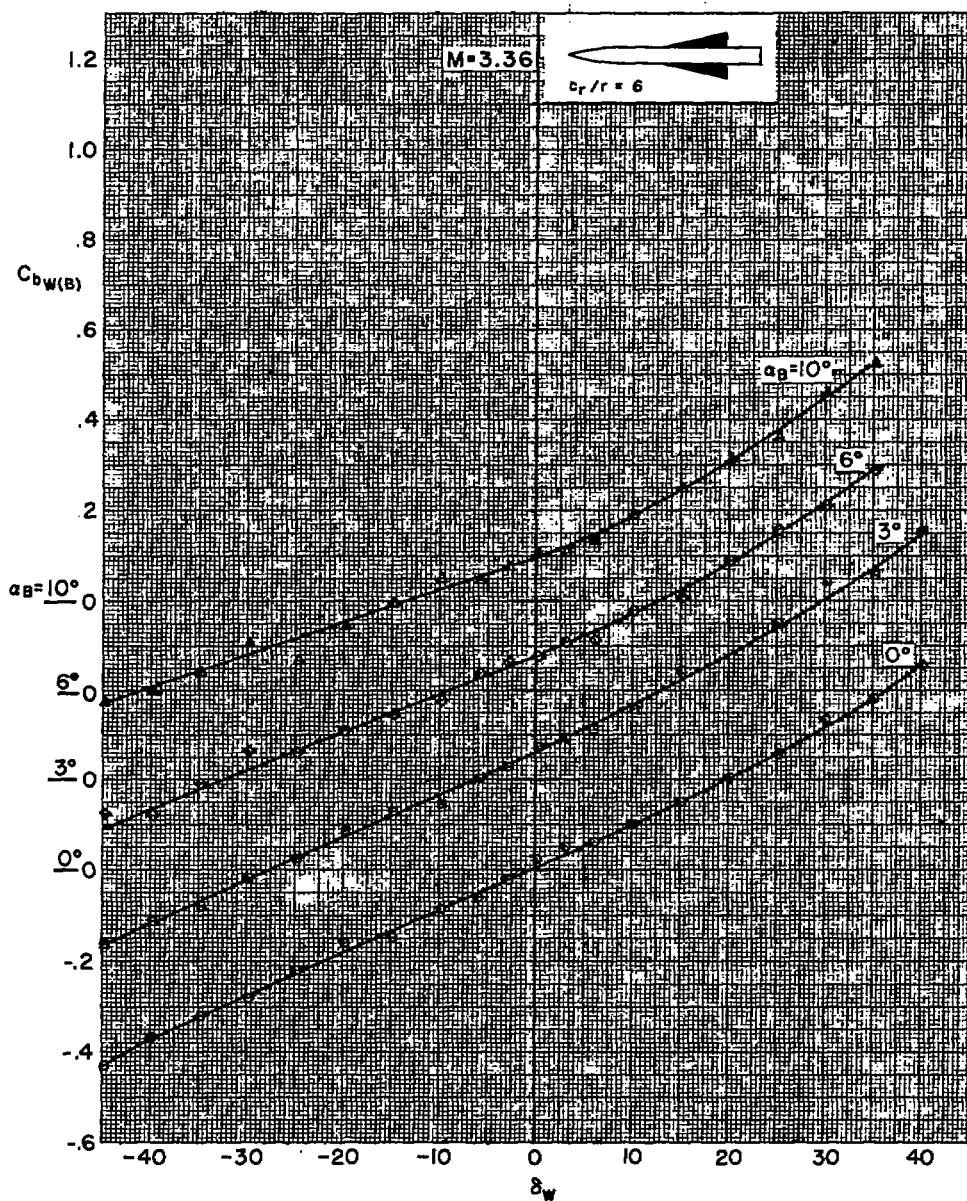
(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 6.- Continued.

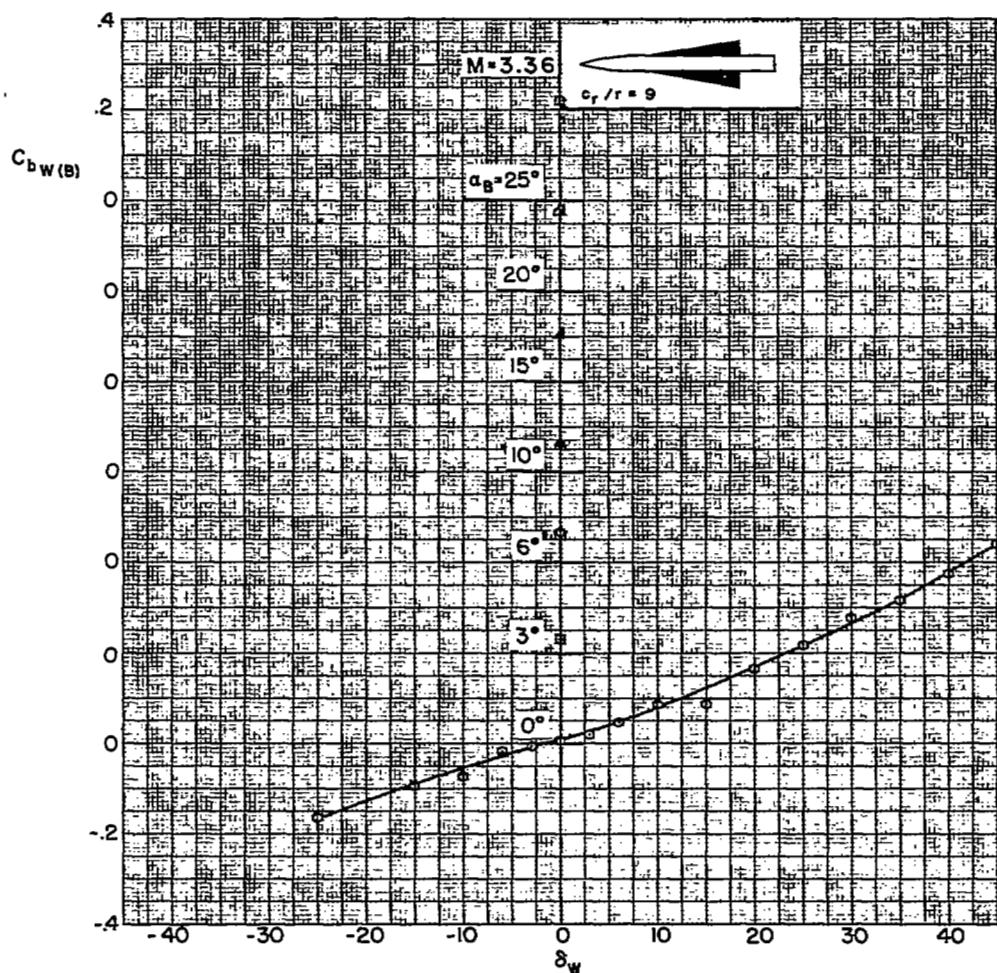
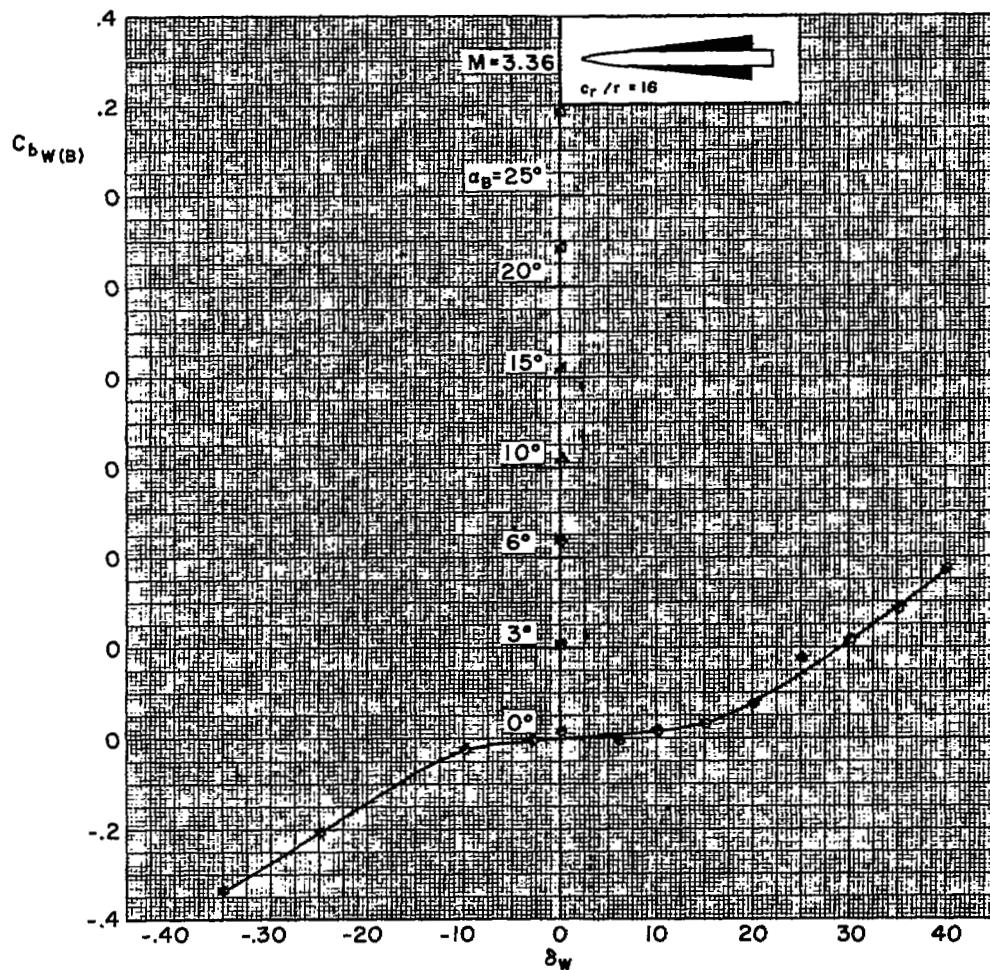
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.

Figure 6.- Continued.



(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 6.- Continued.

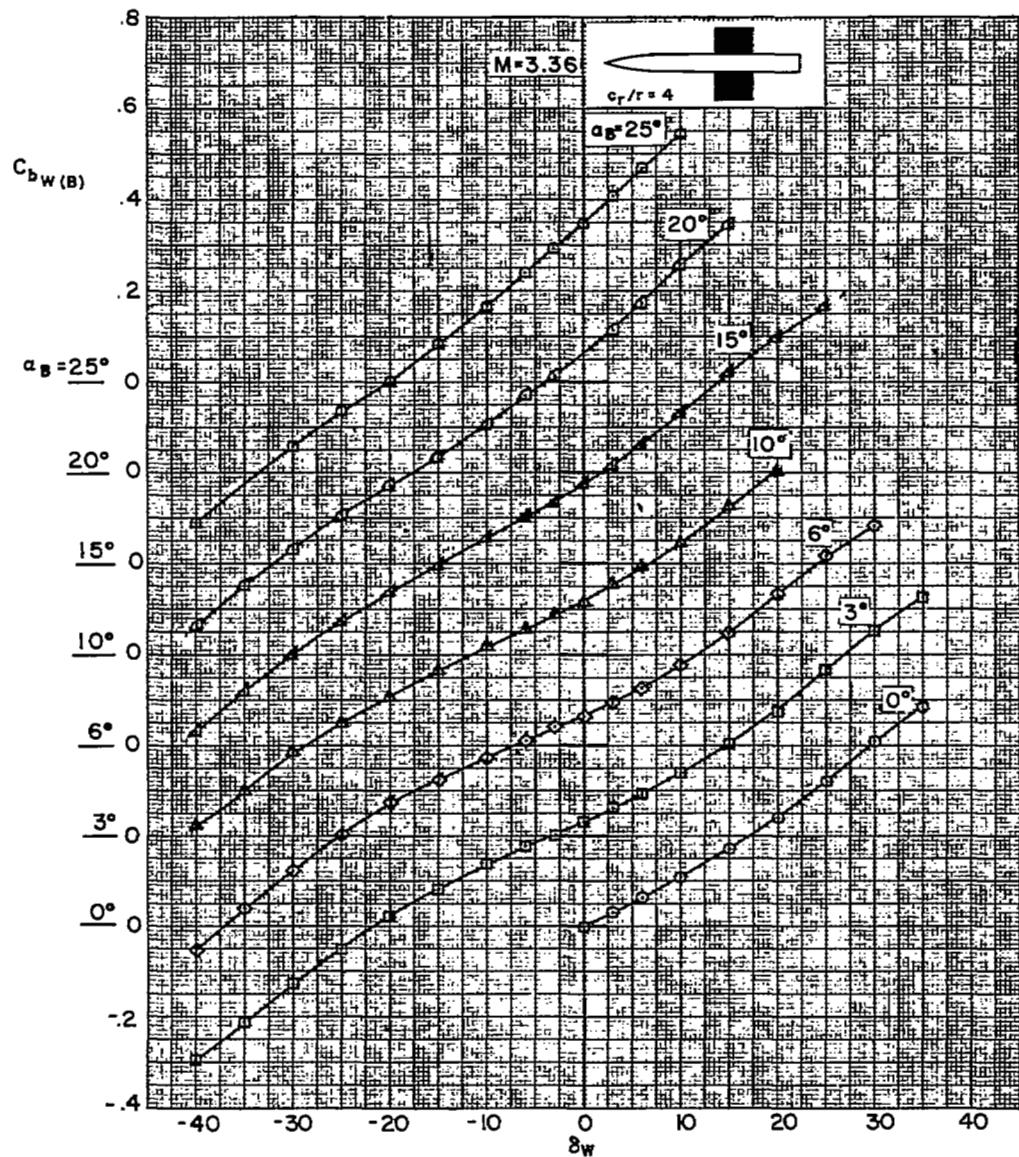
(g) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 6.- Continued.

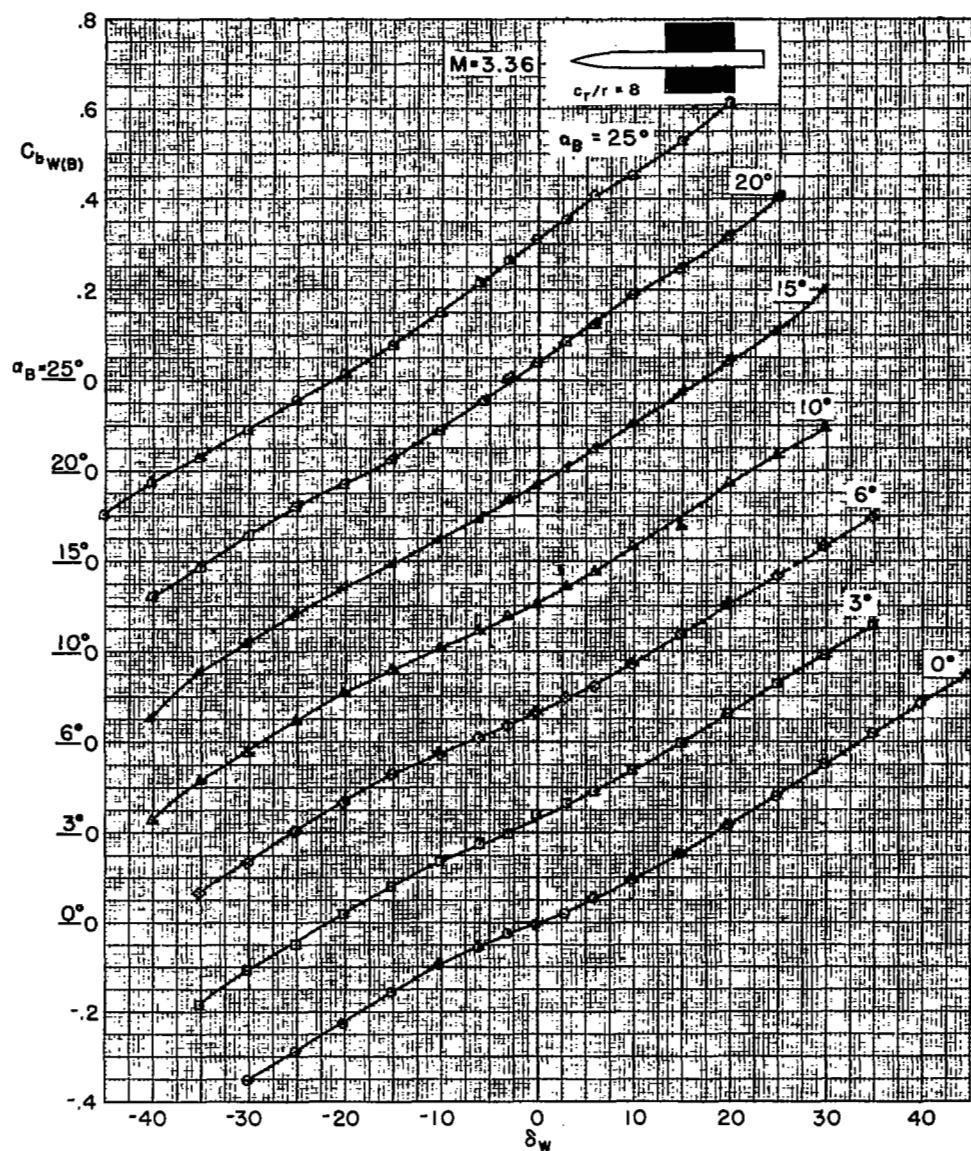
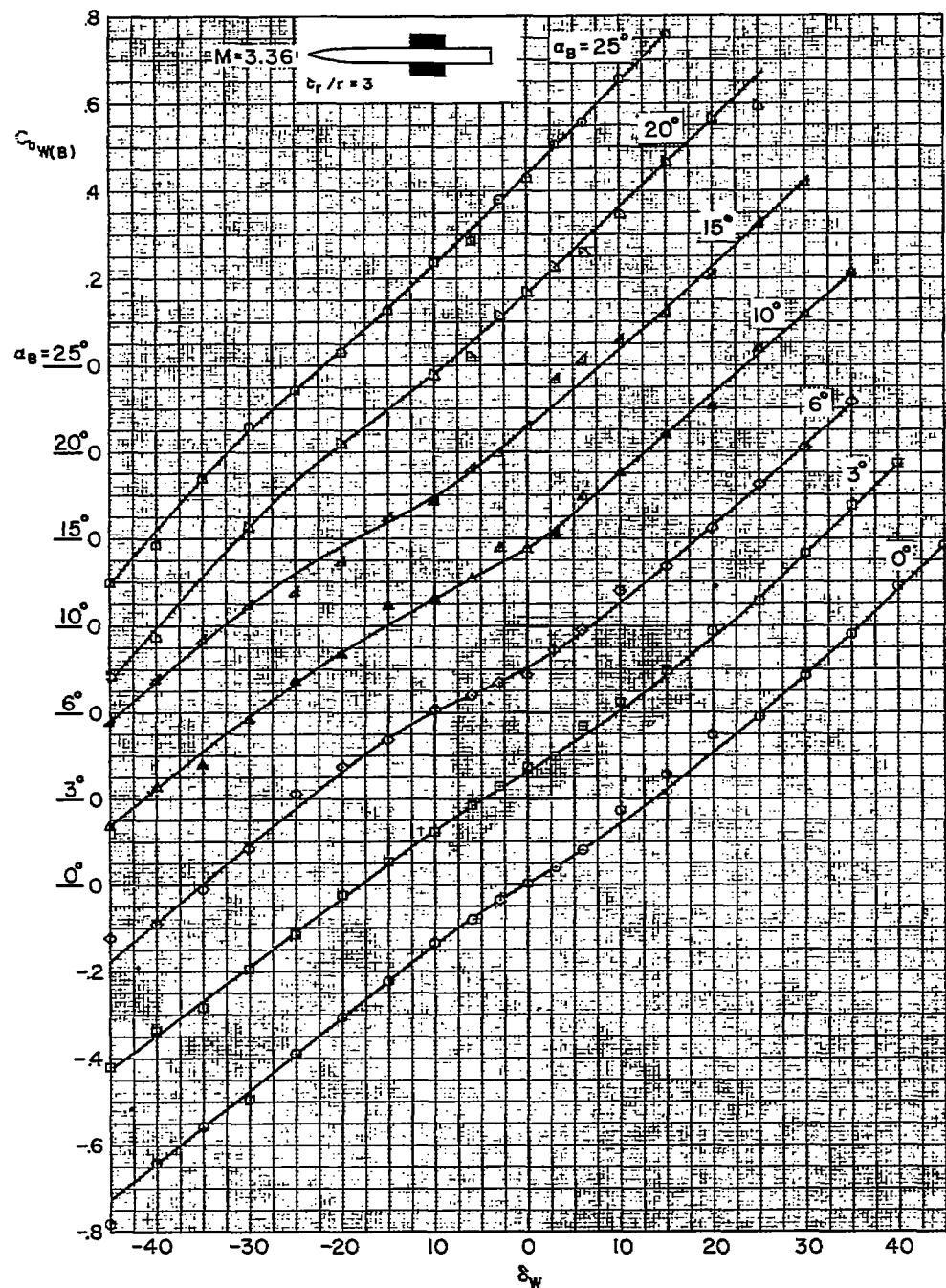
(h) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 6.- Continued.



(i) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 6.- Concluded.

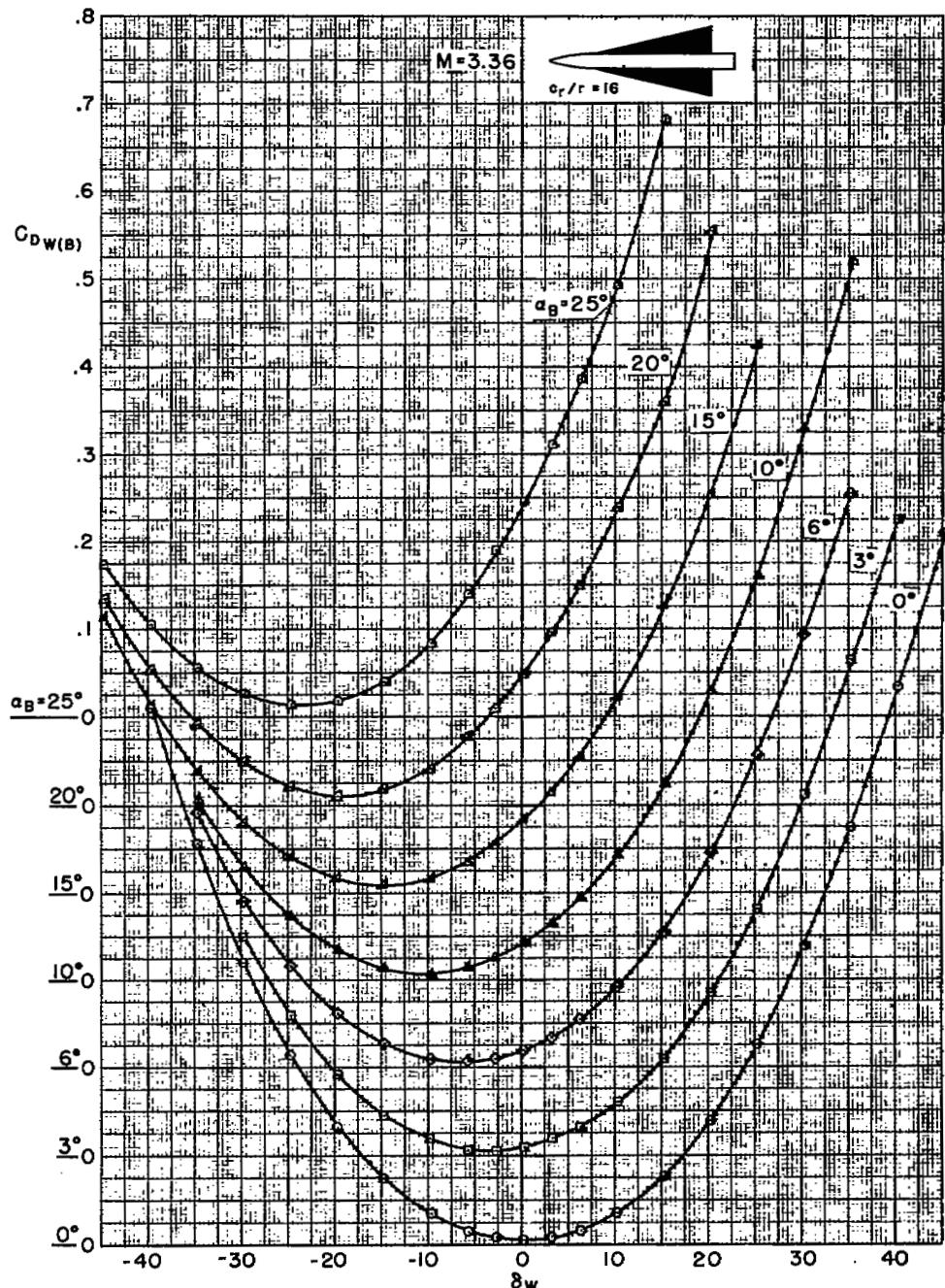
(a) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 7.- Variation with deflection angle of drag coefficient for the wings in the presence of the body.

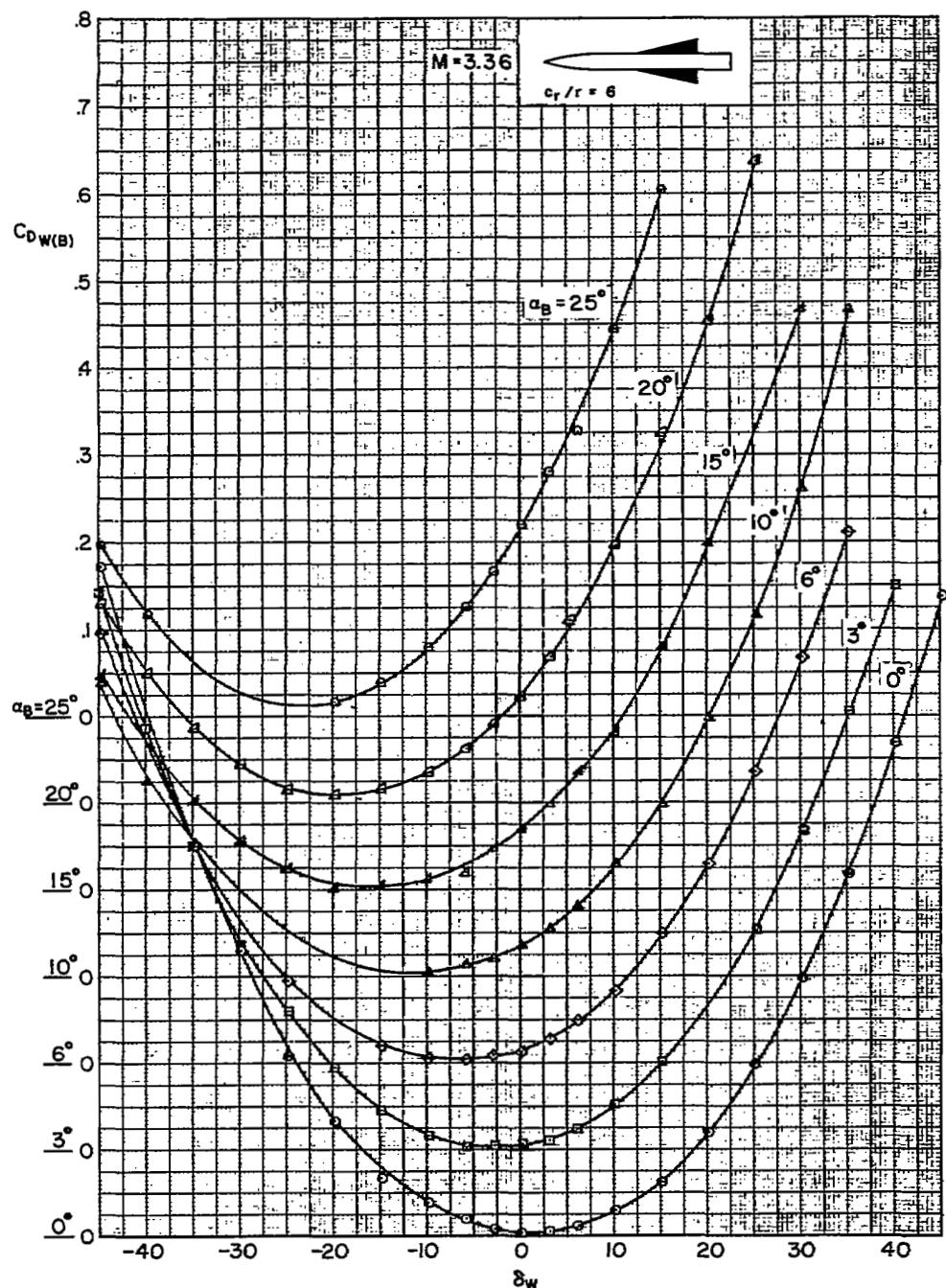
(b) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 7.- Continued.

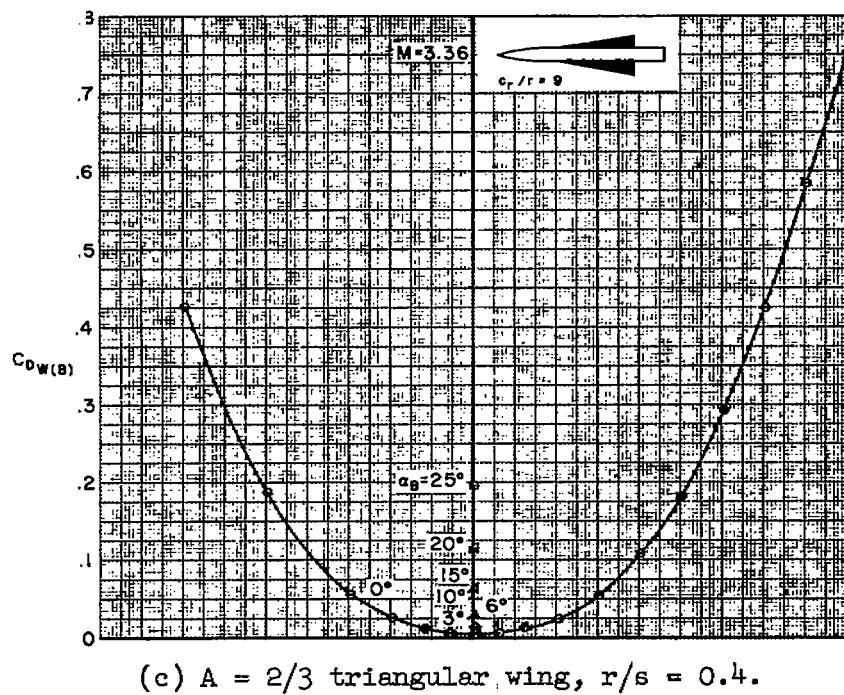
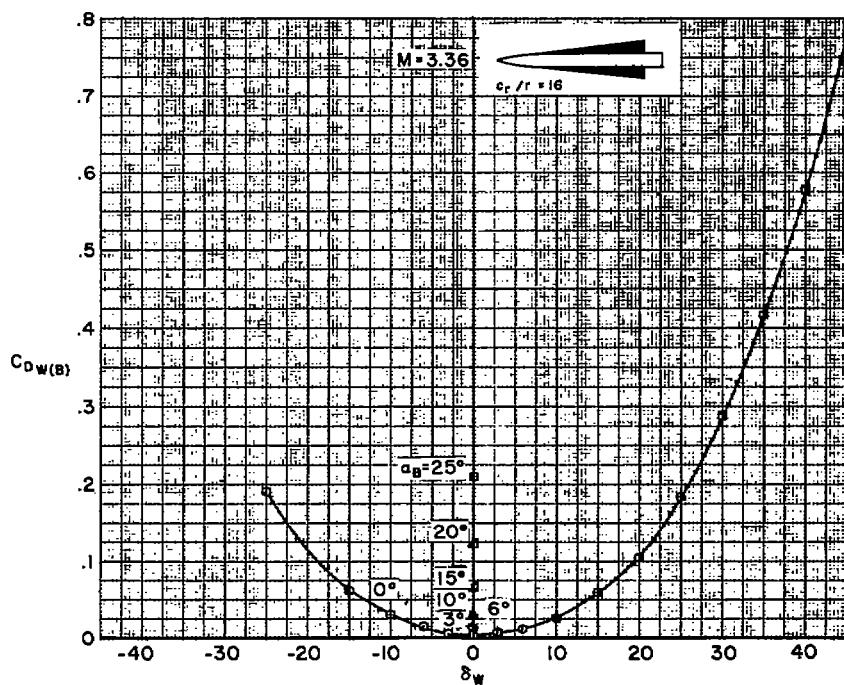
(c) $A = 2/3$ triangular wing, $r/s = 0.4$.(d) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 7.- Continued.

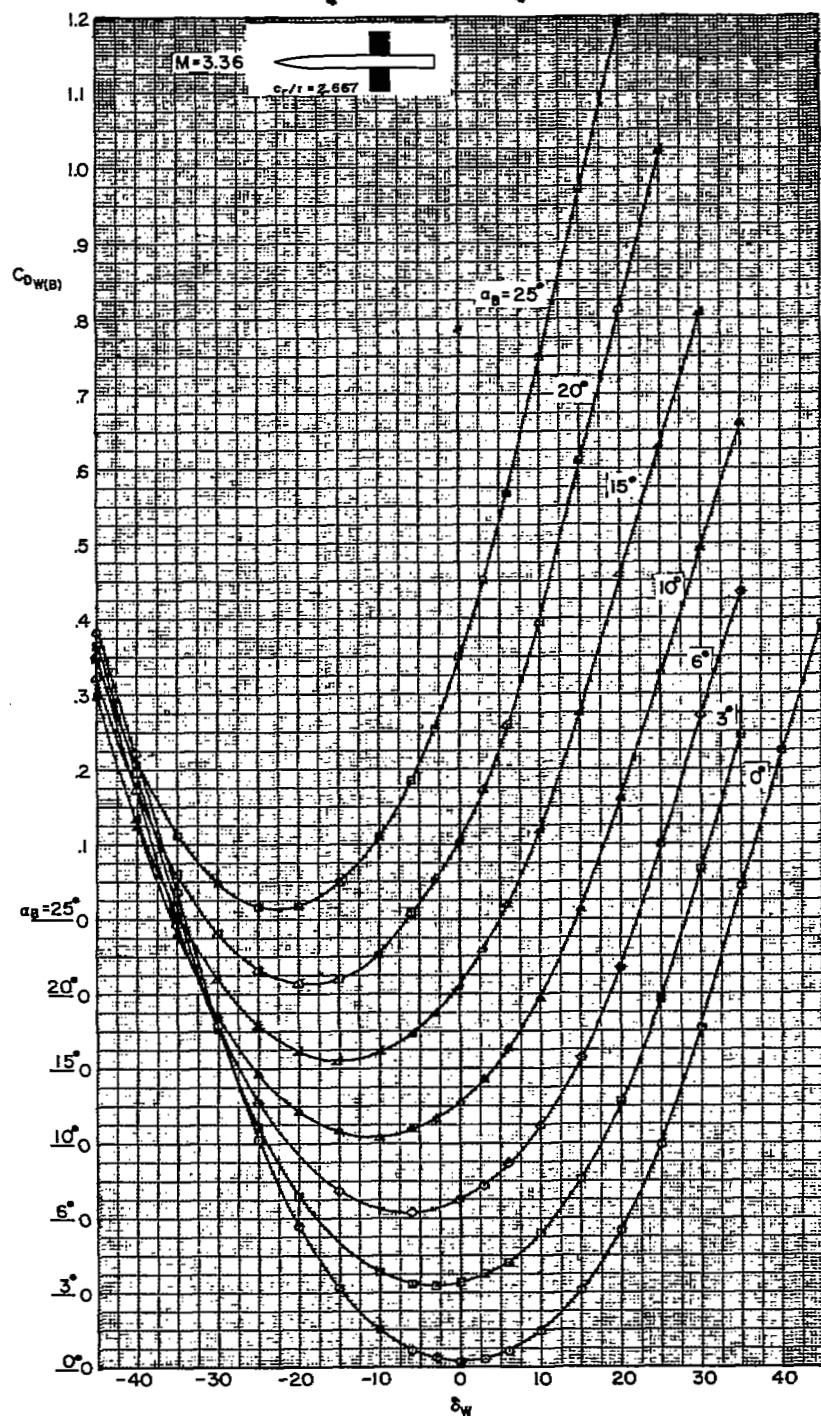
(e) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 7.- Continued.

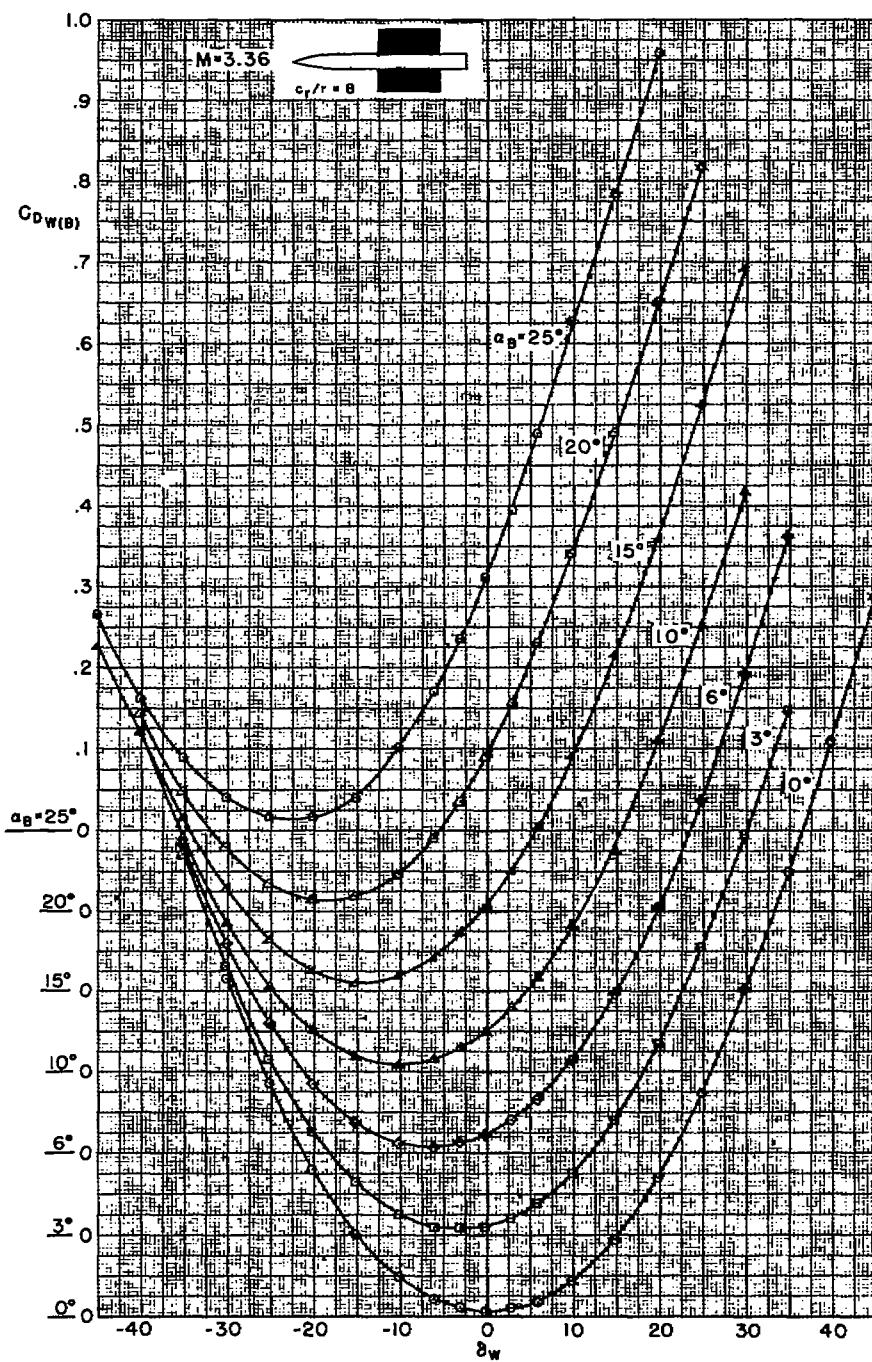
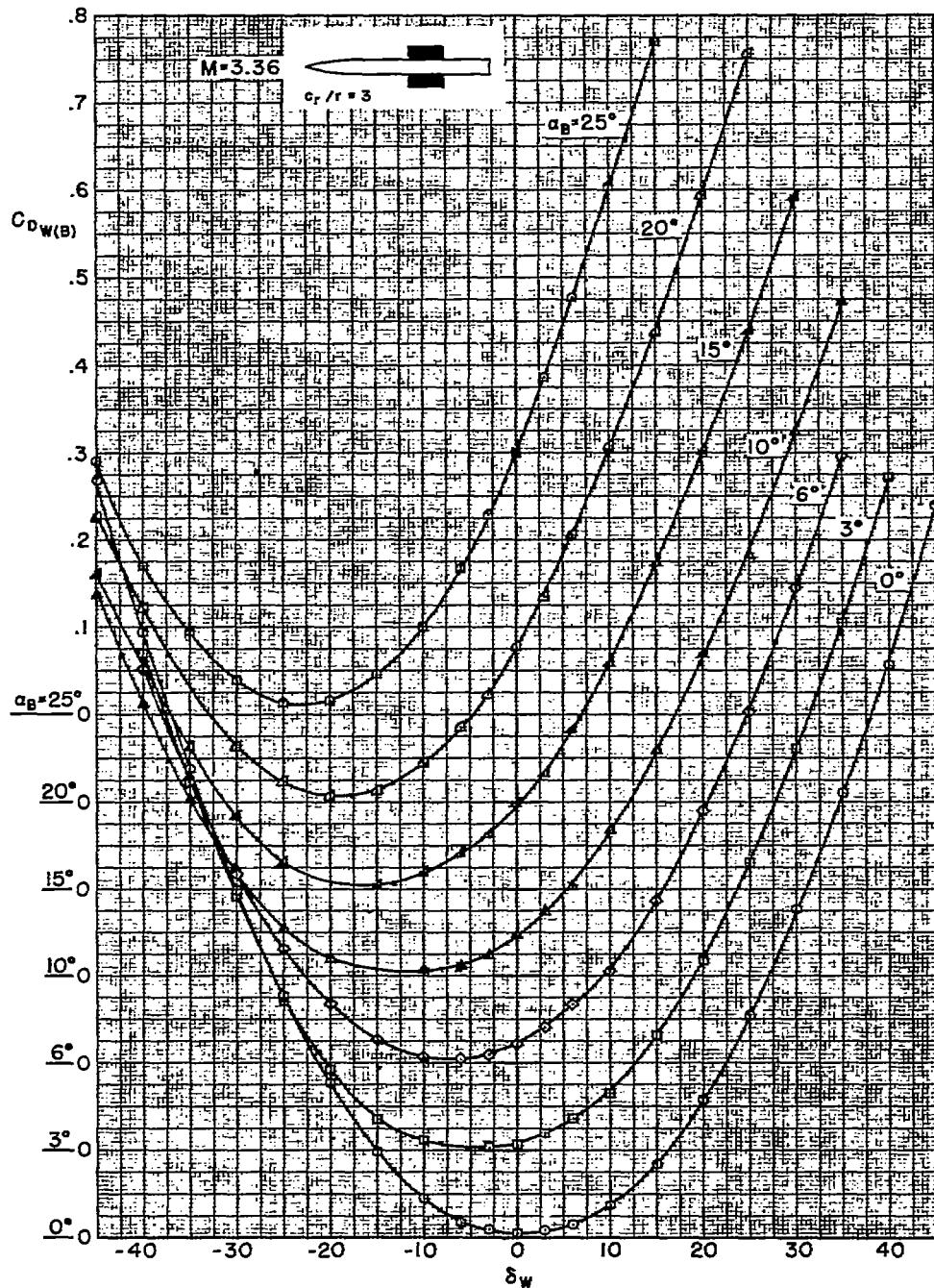
(f) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 7.- Continued.



(g) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 7.- Concluded.

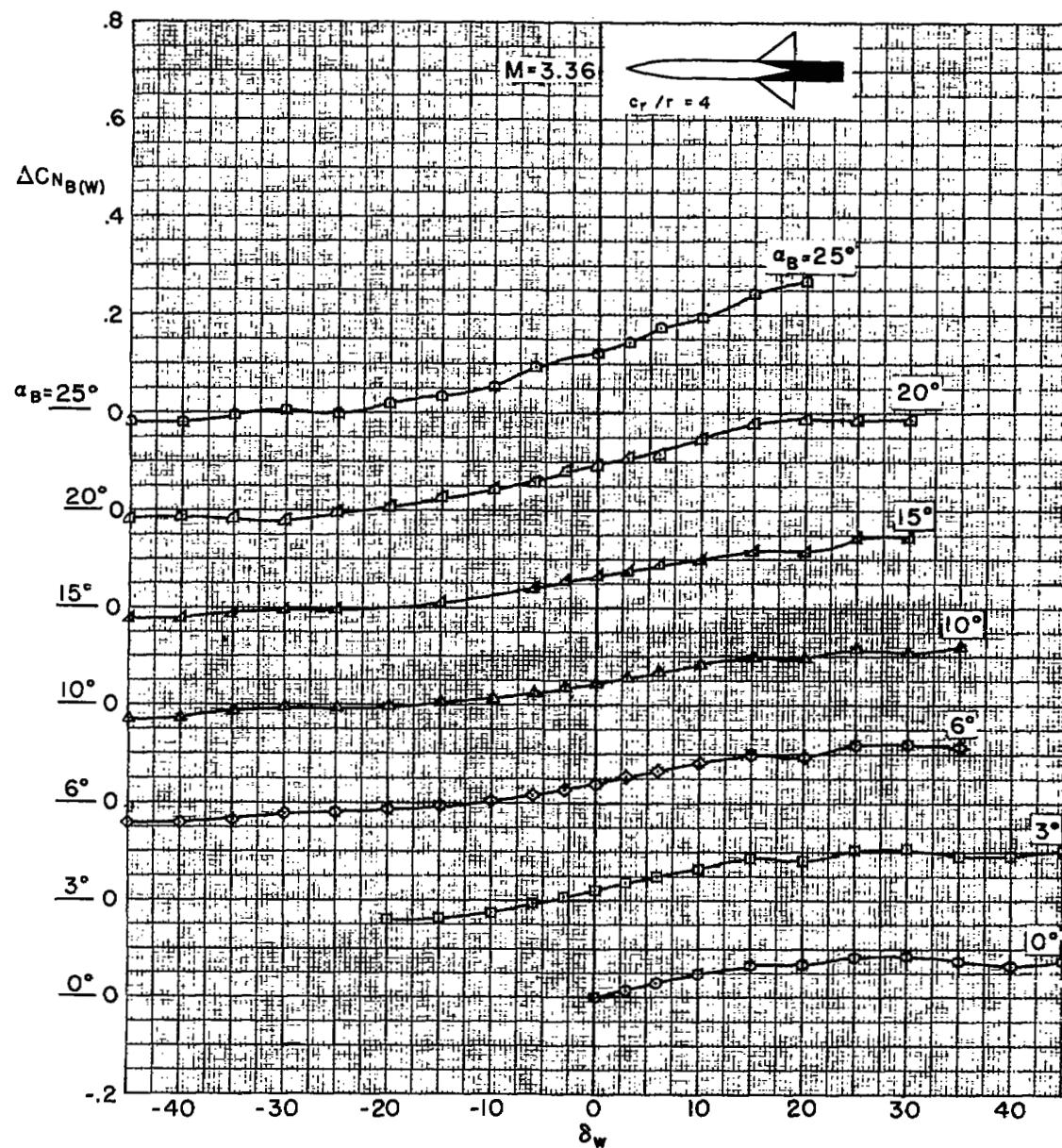
(a) $A = 4$ triangular wing, $r/s = 0.2$.

Figure 8.- Variation with deflection angle of interference normal-force coefficient for the body in the presence of the wings.

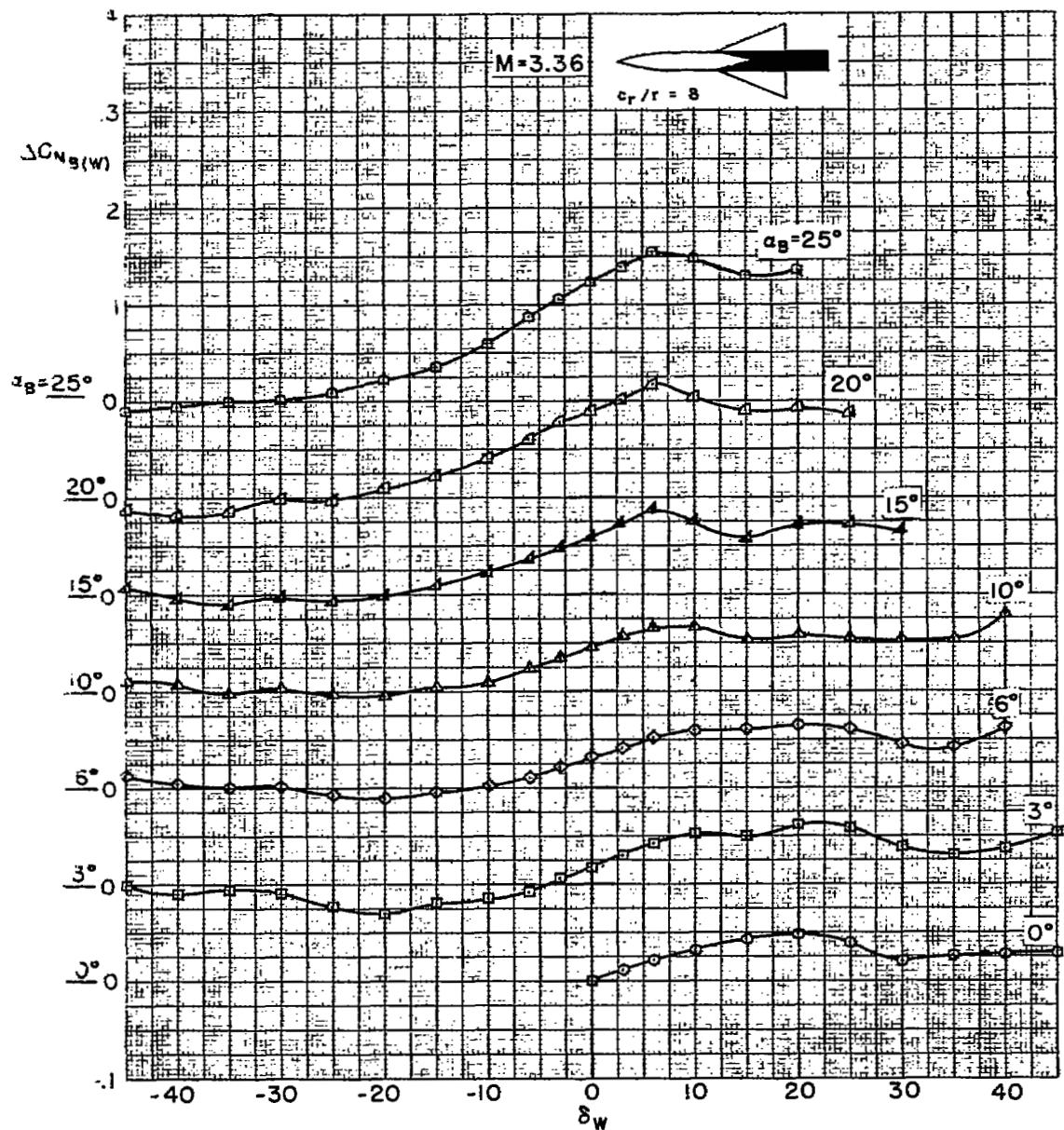
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 8.- Continued.

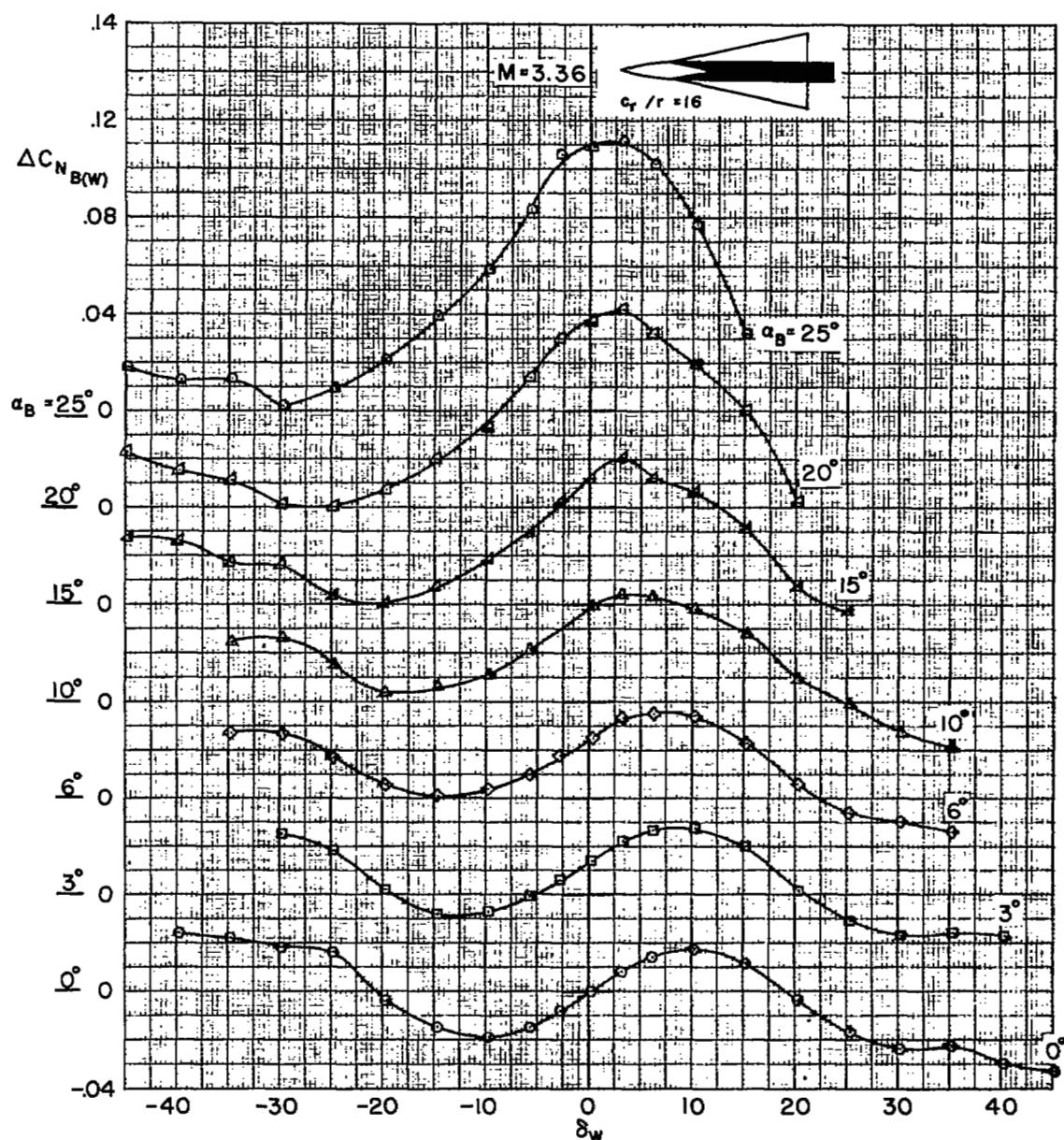
(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 8.- Continued.

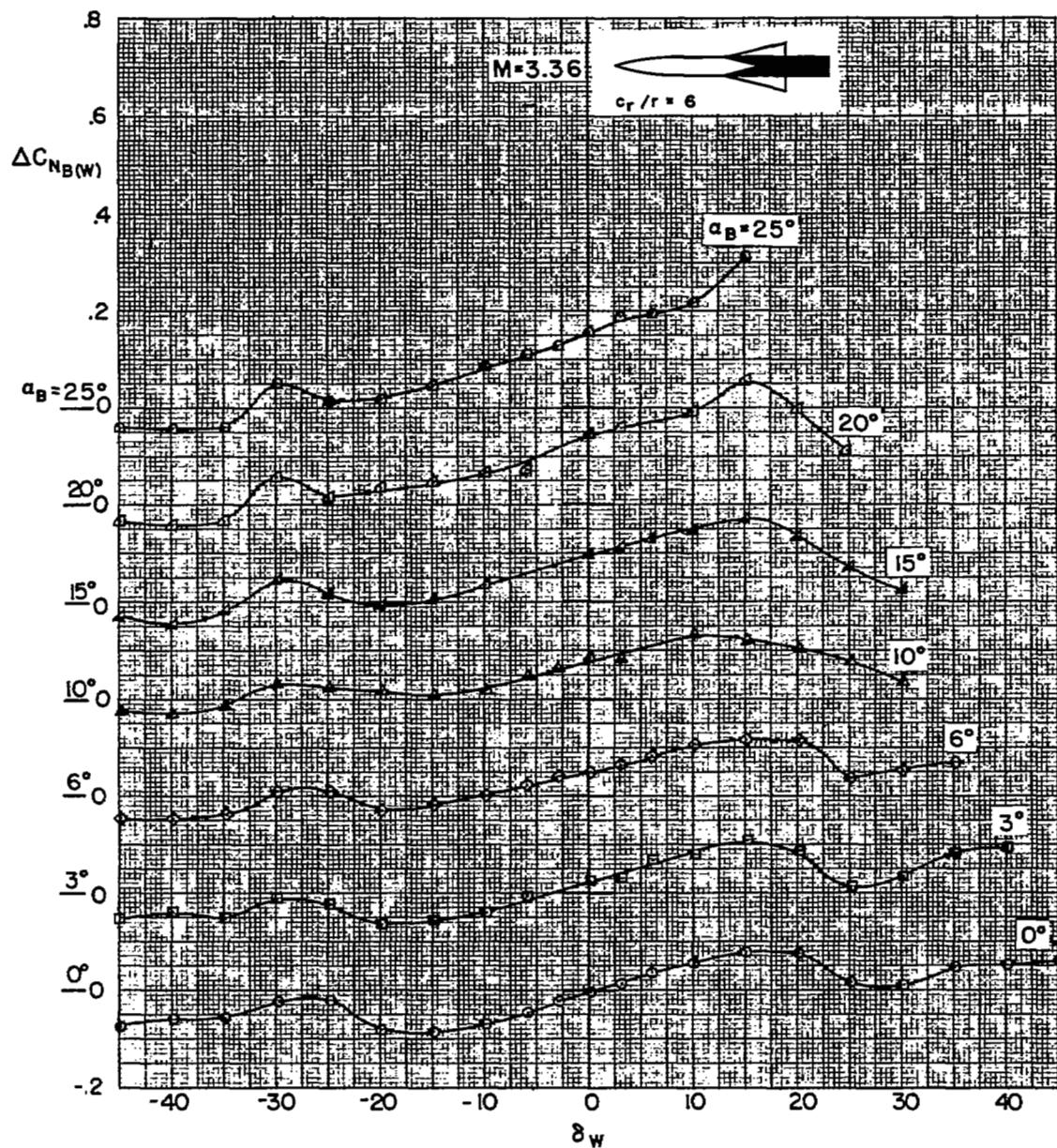
(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 8.- Continued.

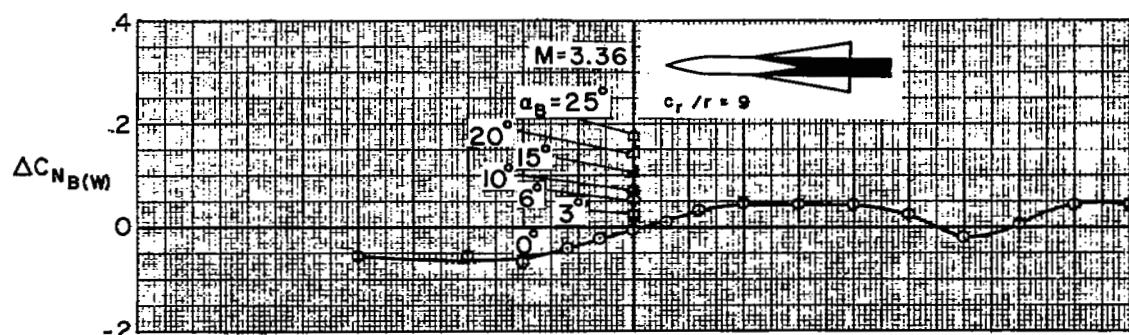
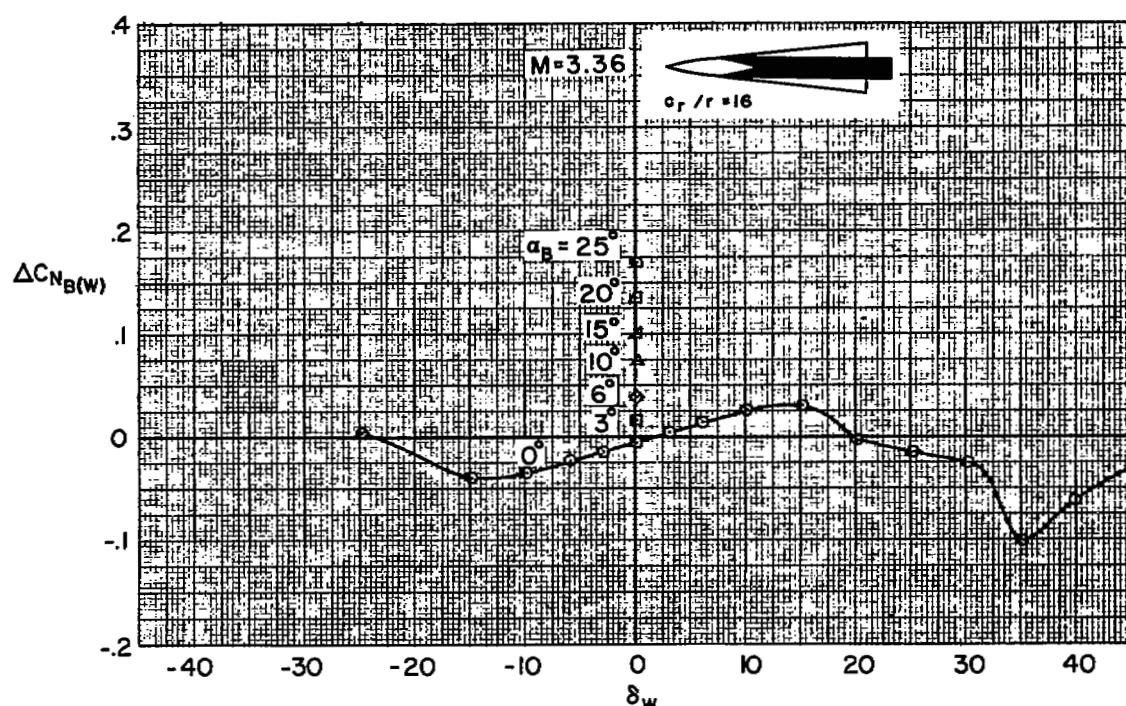
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 8.- Continued.

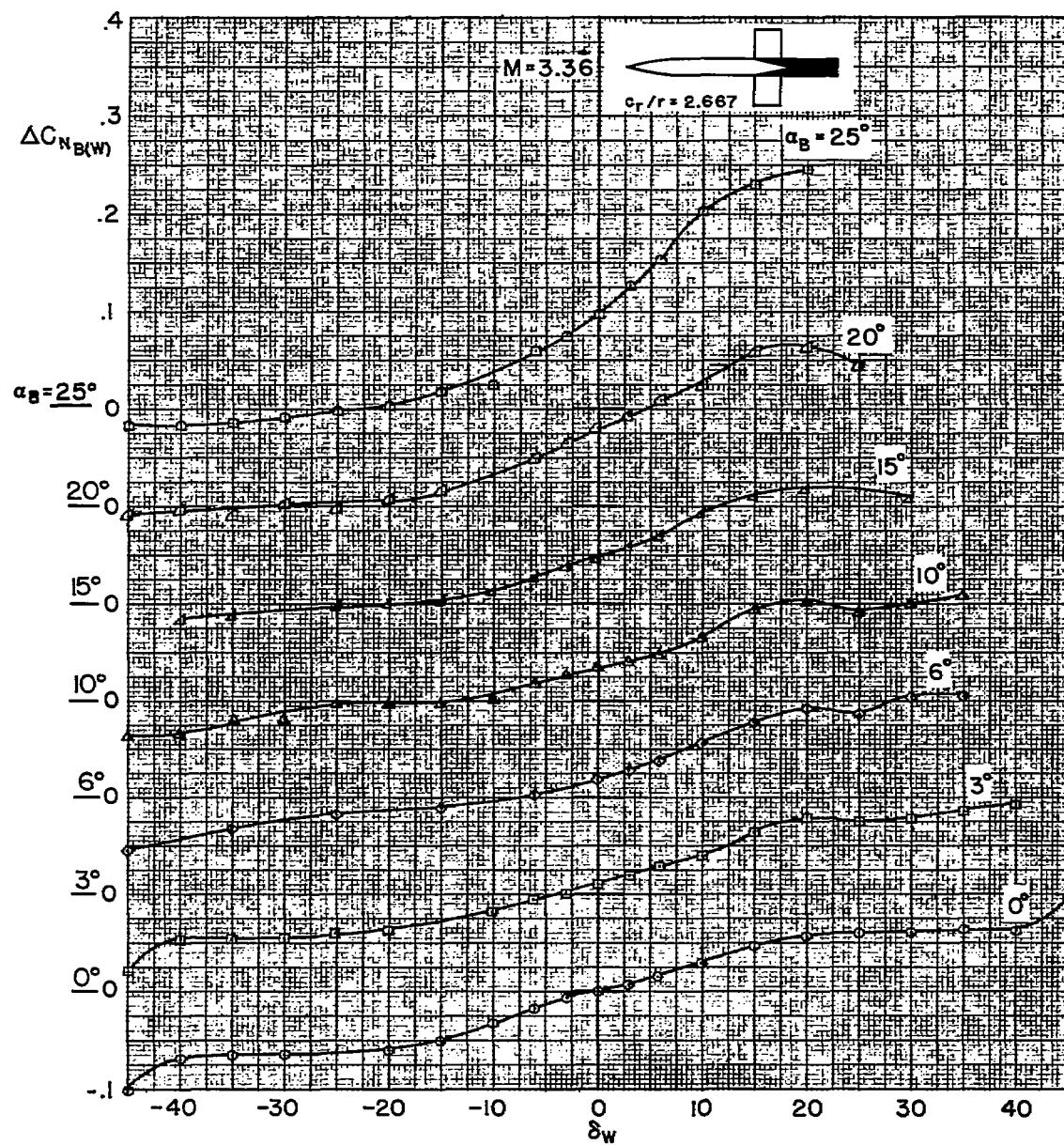
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 8.- Continued.

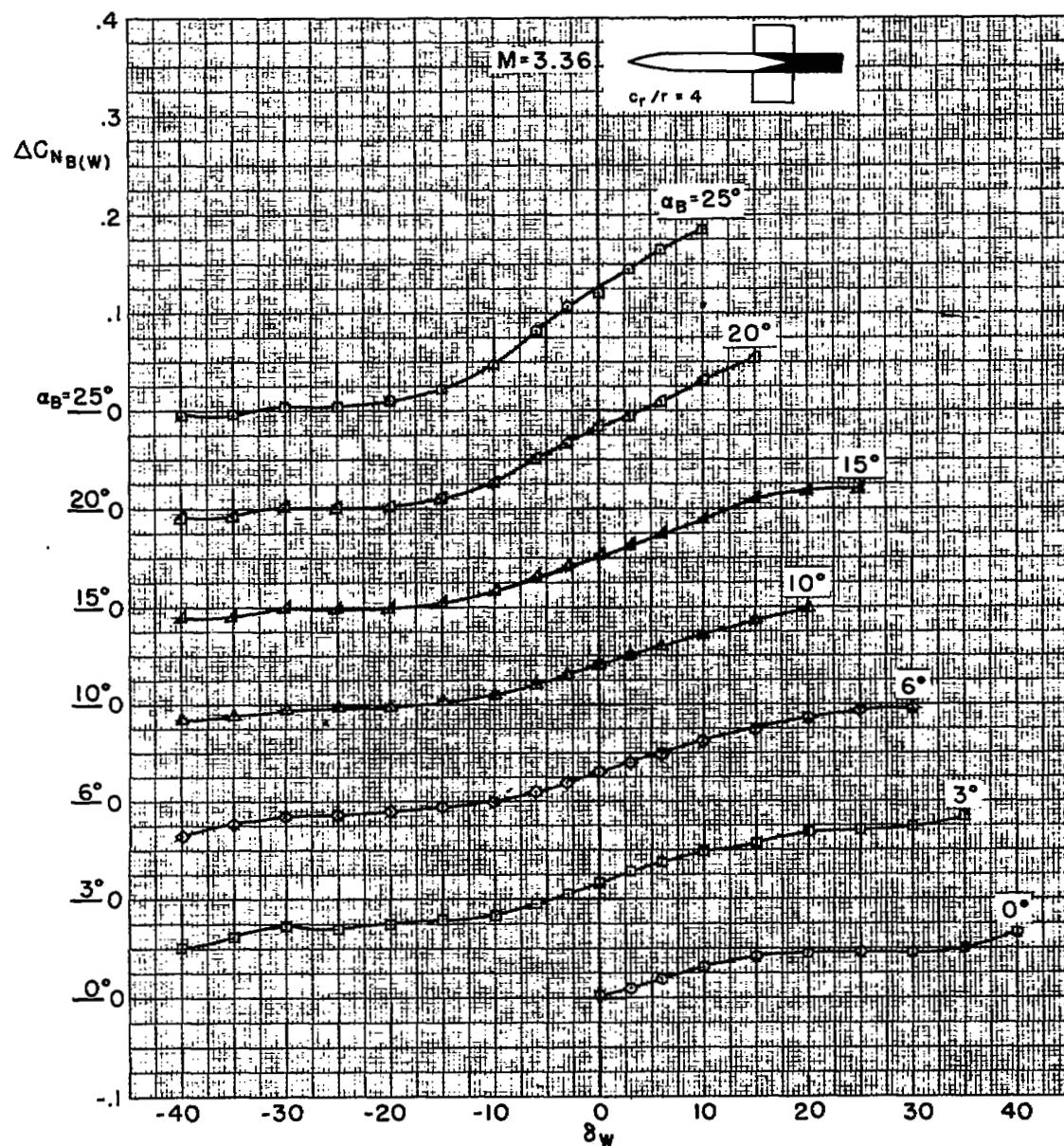
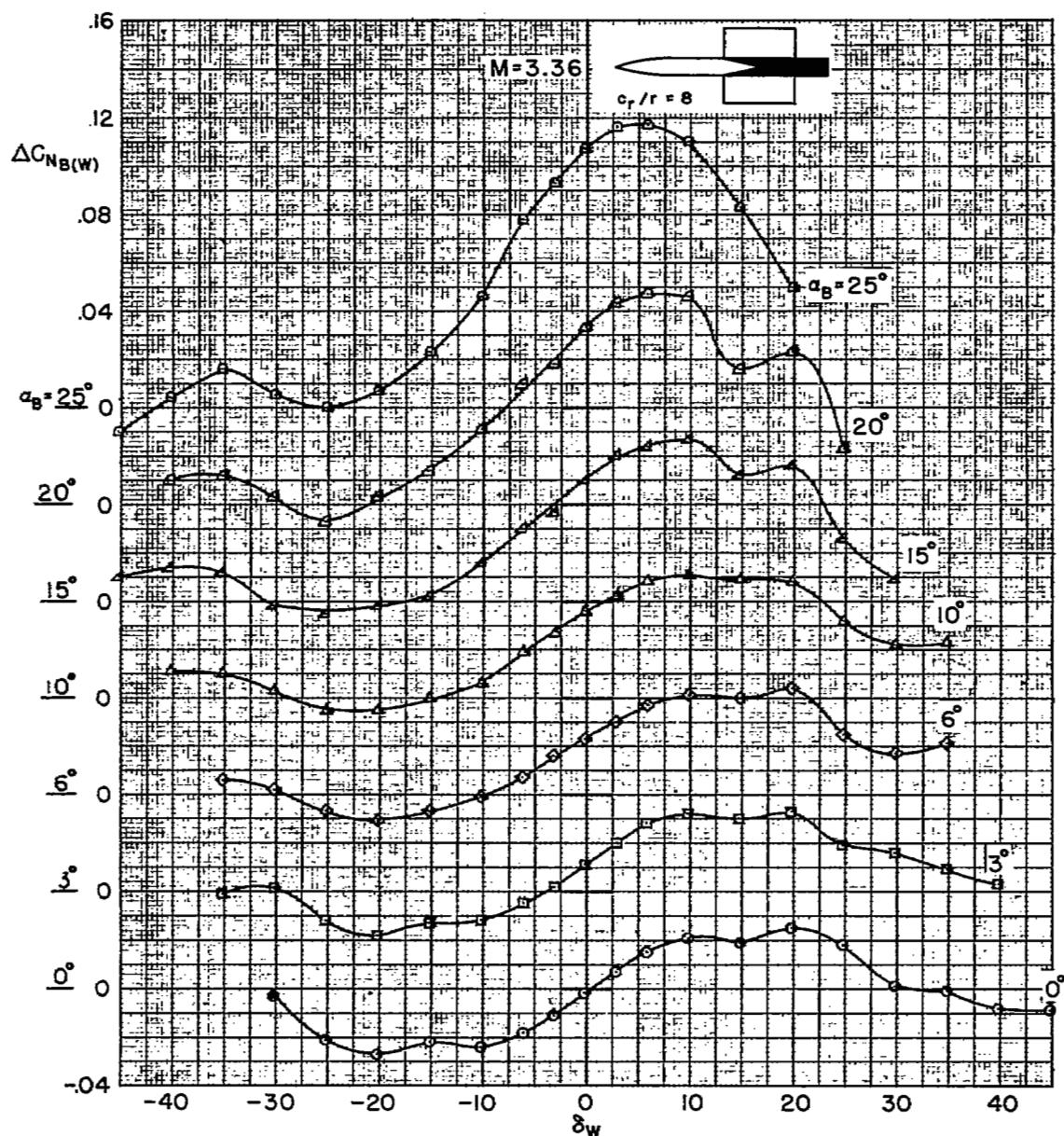
(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 8.- Continued.



(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 8.- Continued.

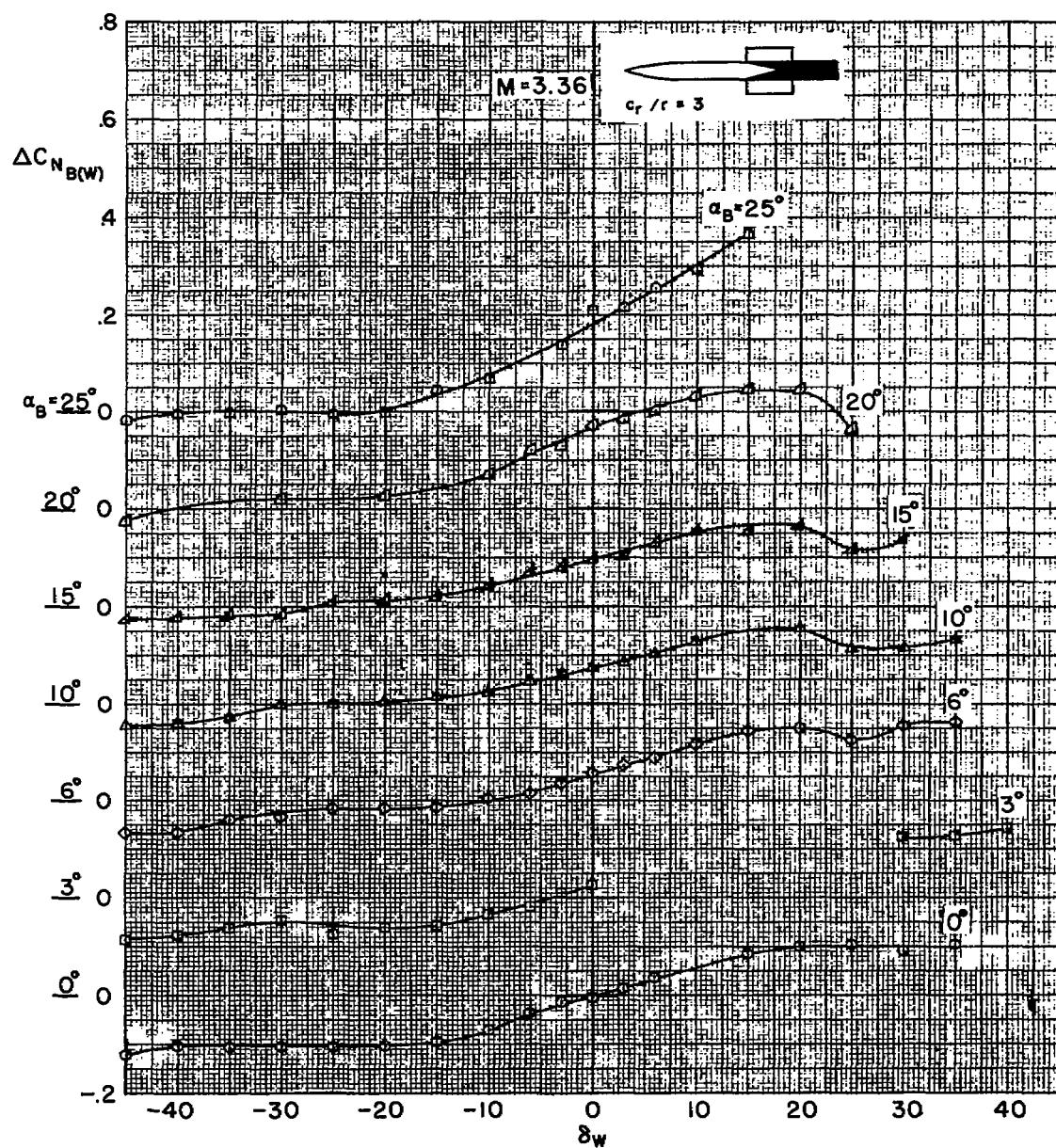
(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 8.- Concluded.

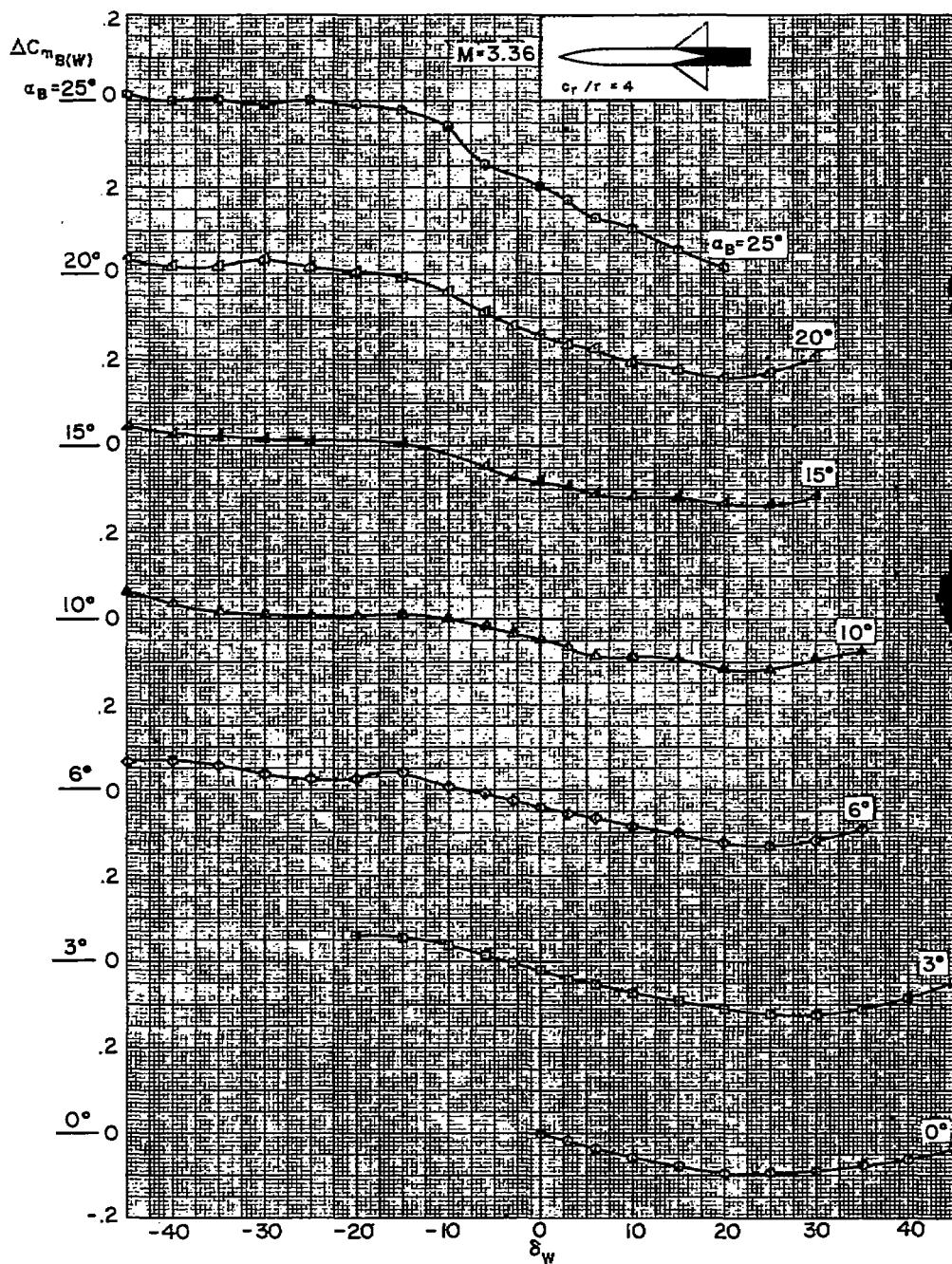
(a) $A = 4$ triangular wing, $r/s = 0.2$.

Figure 9.- Variation with deflection angle of interference pitching-moment coefficient for the body in the presence of the wings.

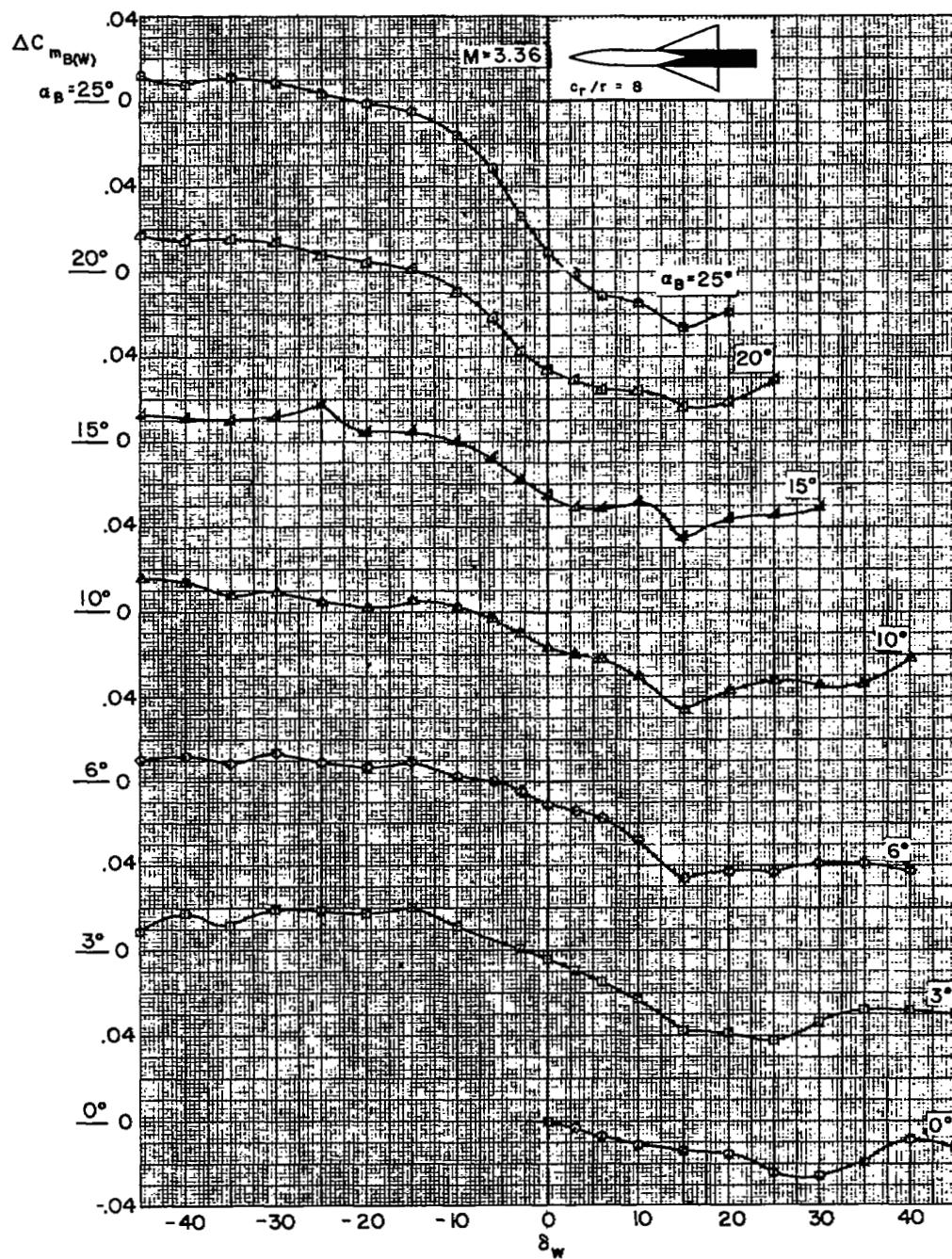
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 9.- Continued.

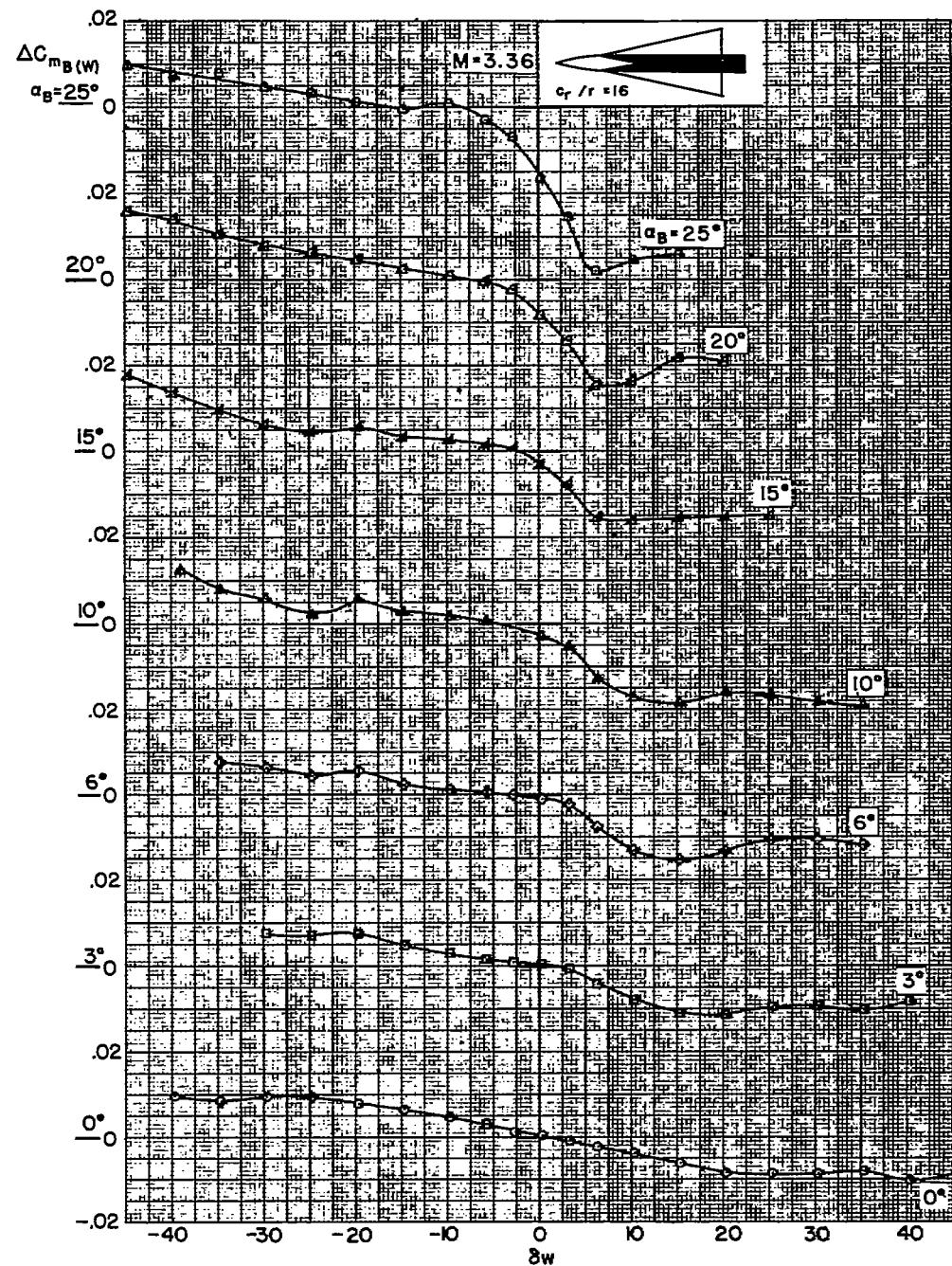
(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 9.- Continued.

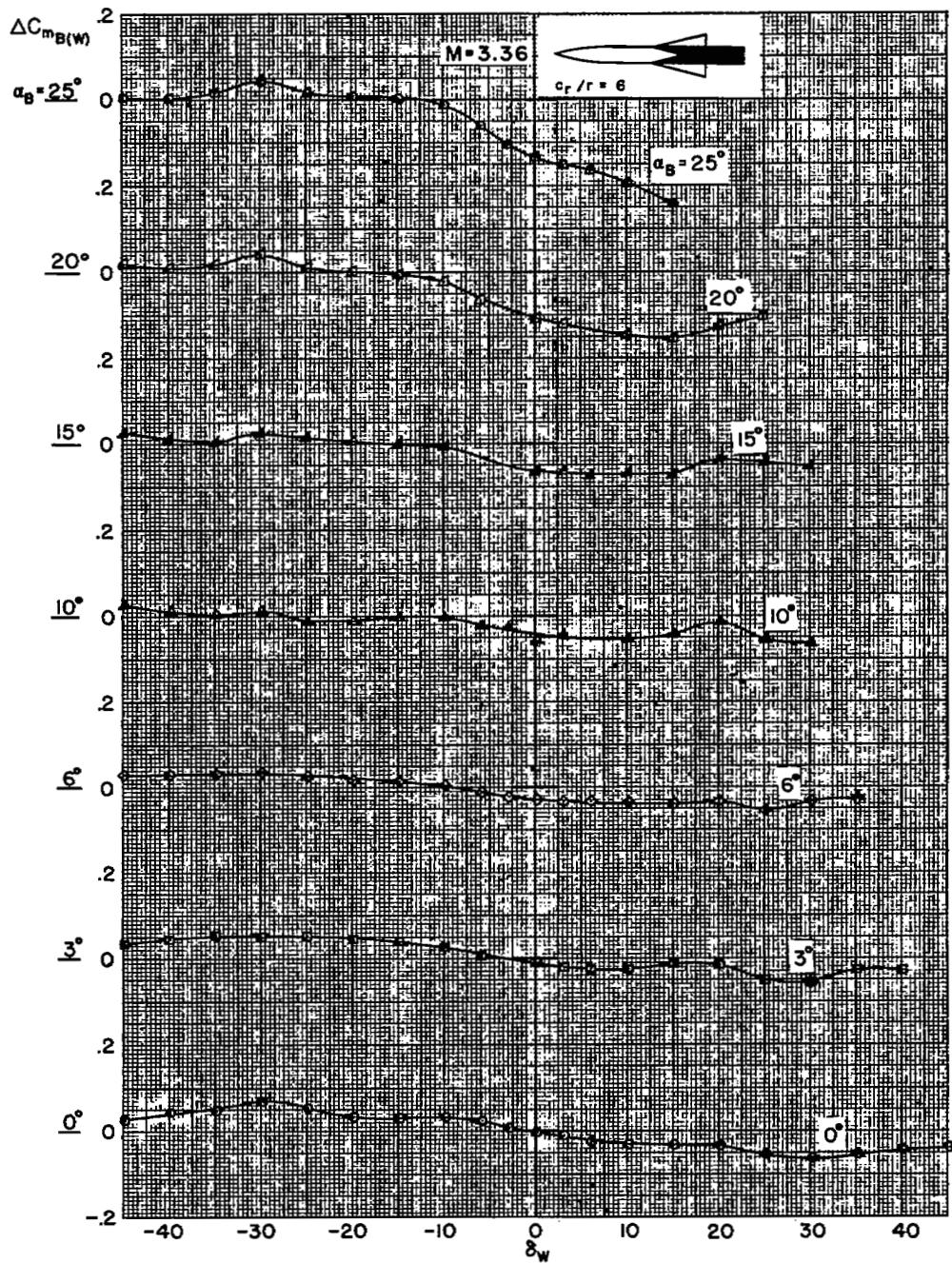
(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 9.- Continued.

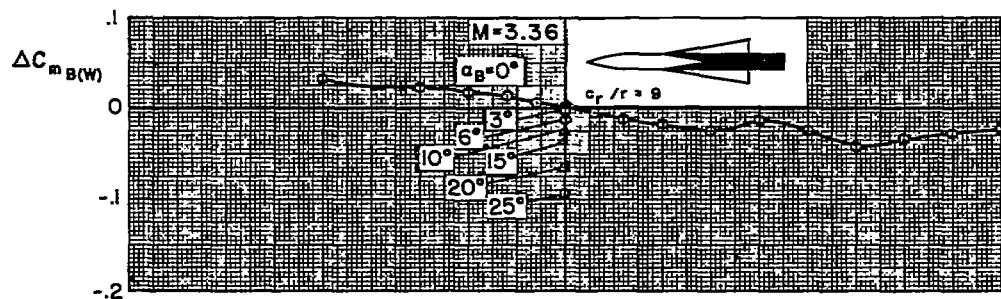
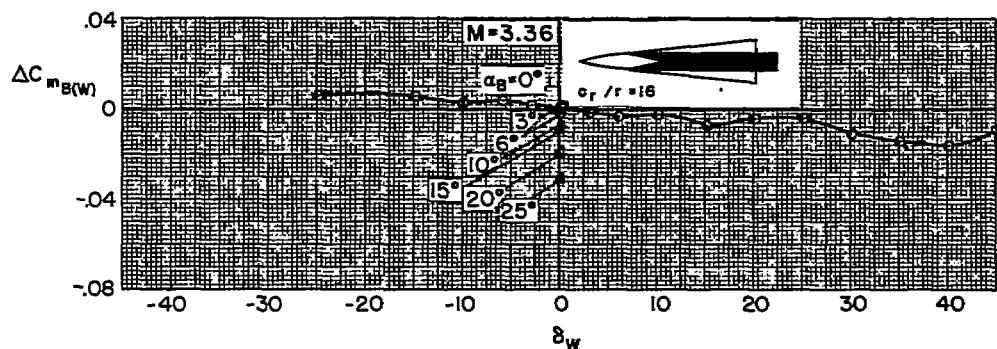
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 9.- Continued.

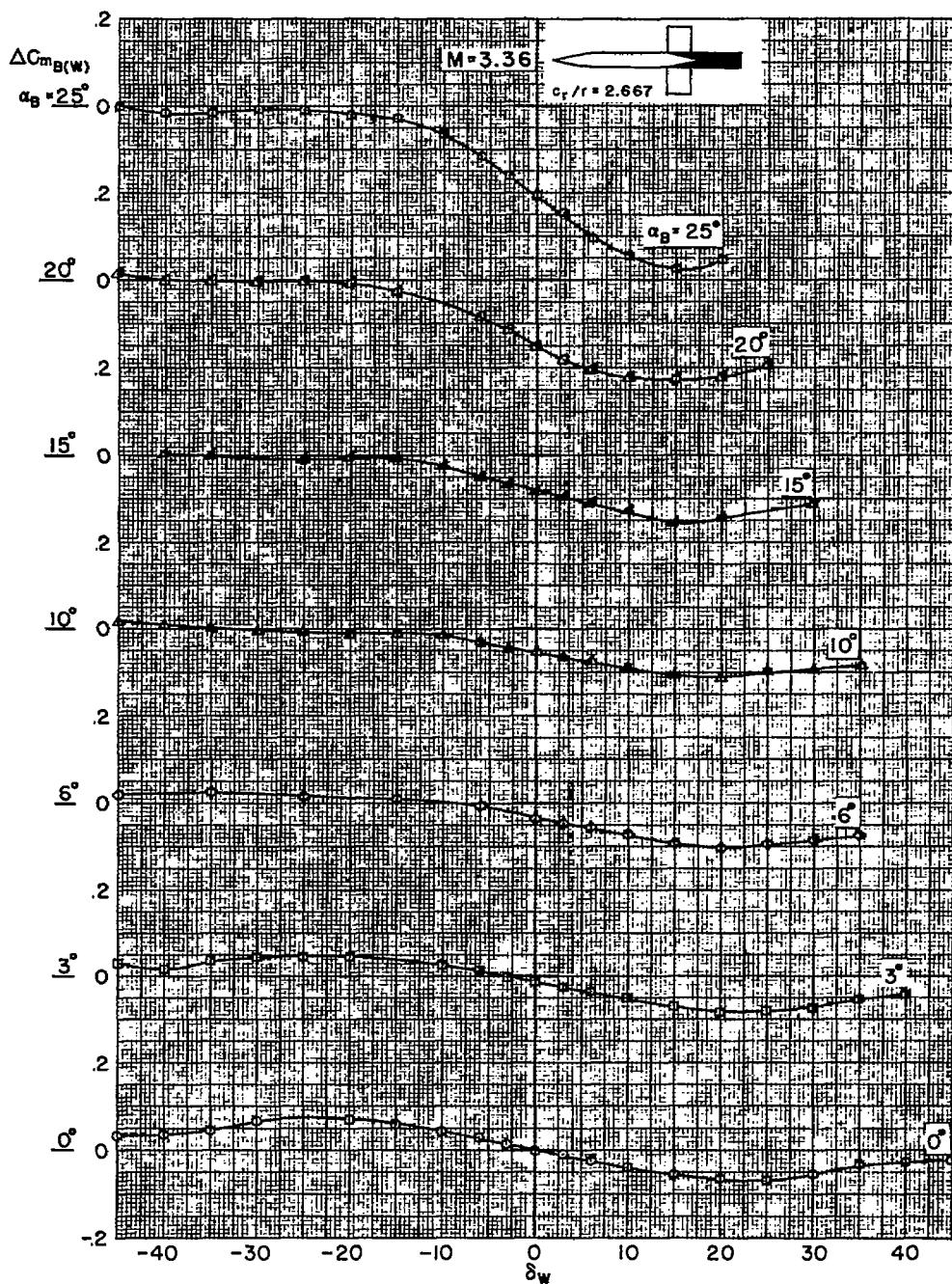
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 9.- Continued.

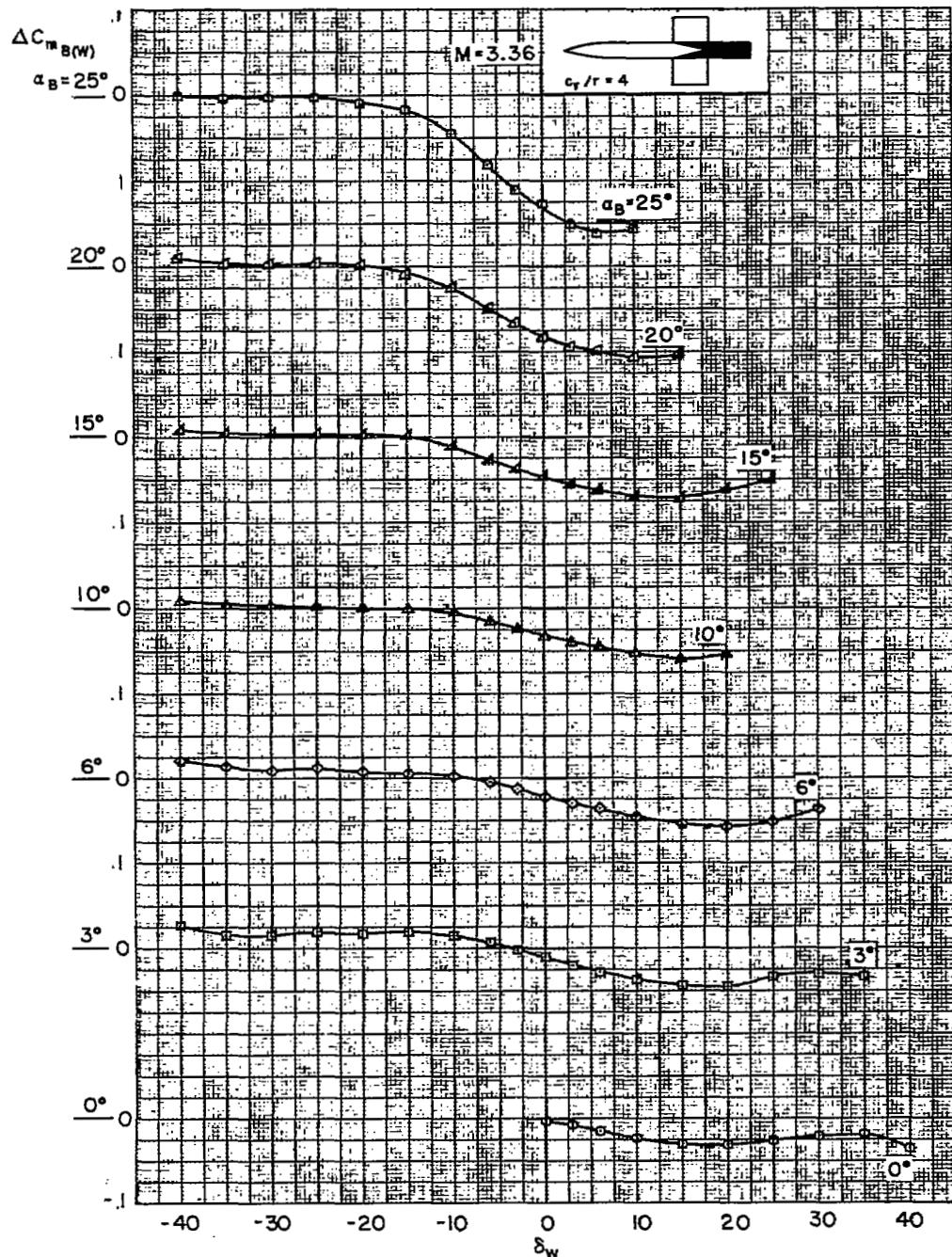
(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 9--Continued.

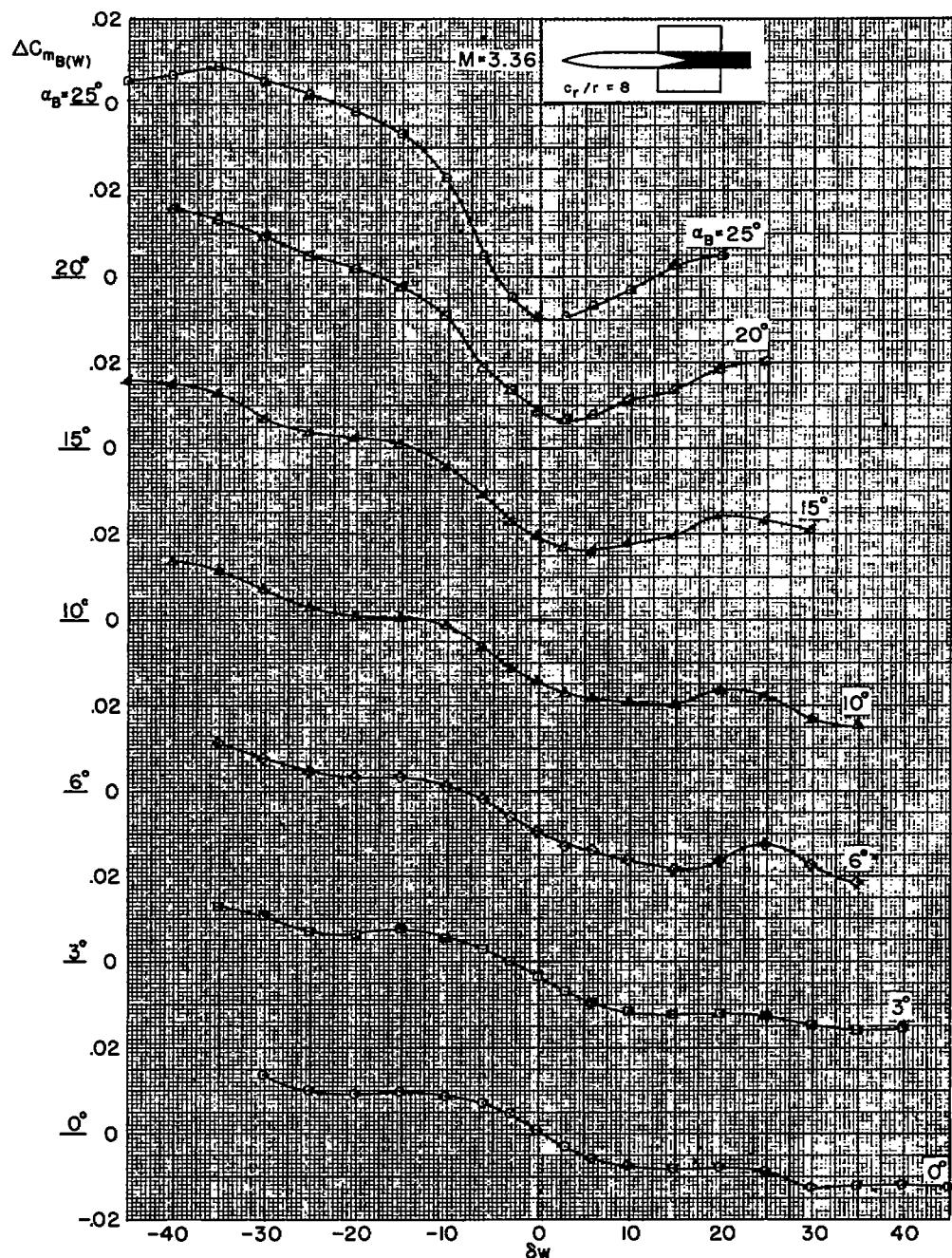
(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 9.- Continued.

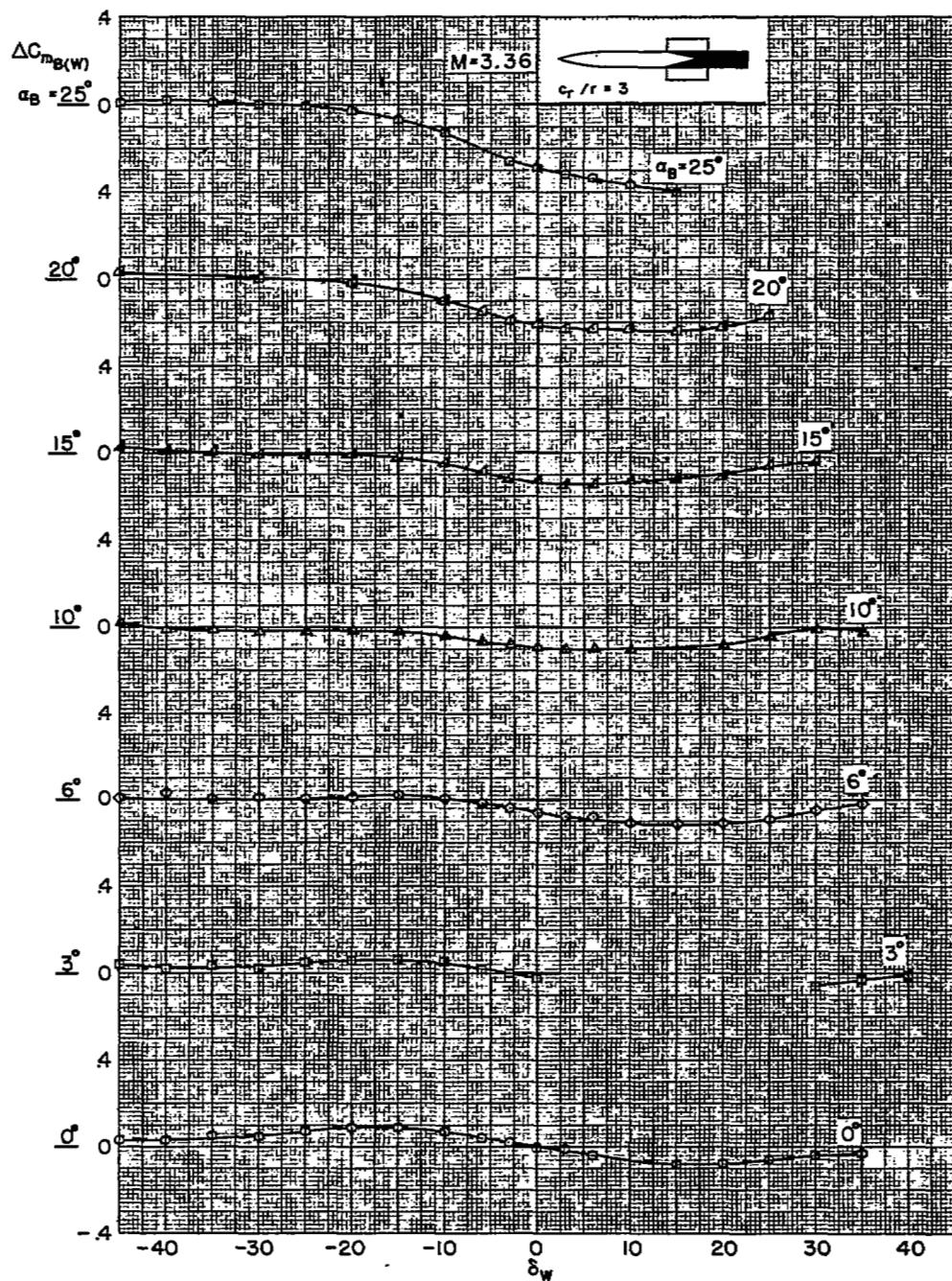
(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 9.- Concluded.

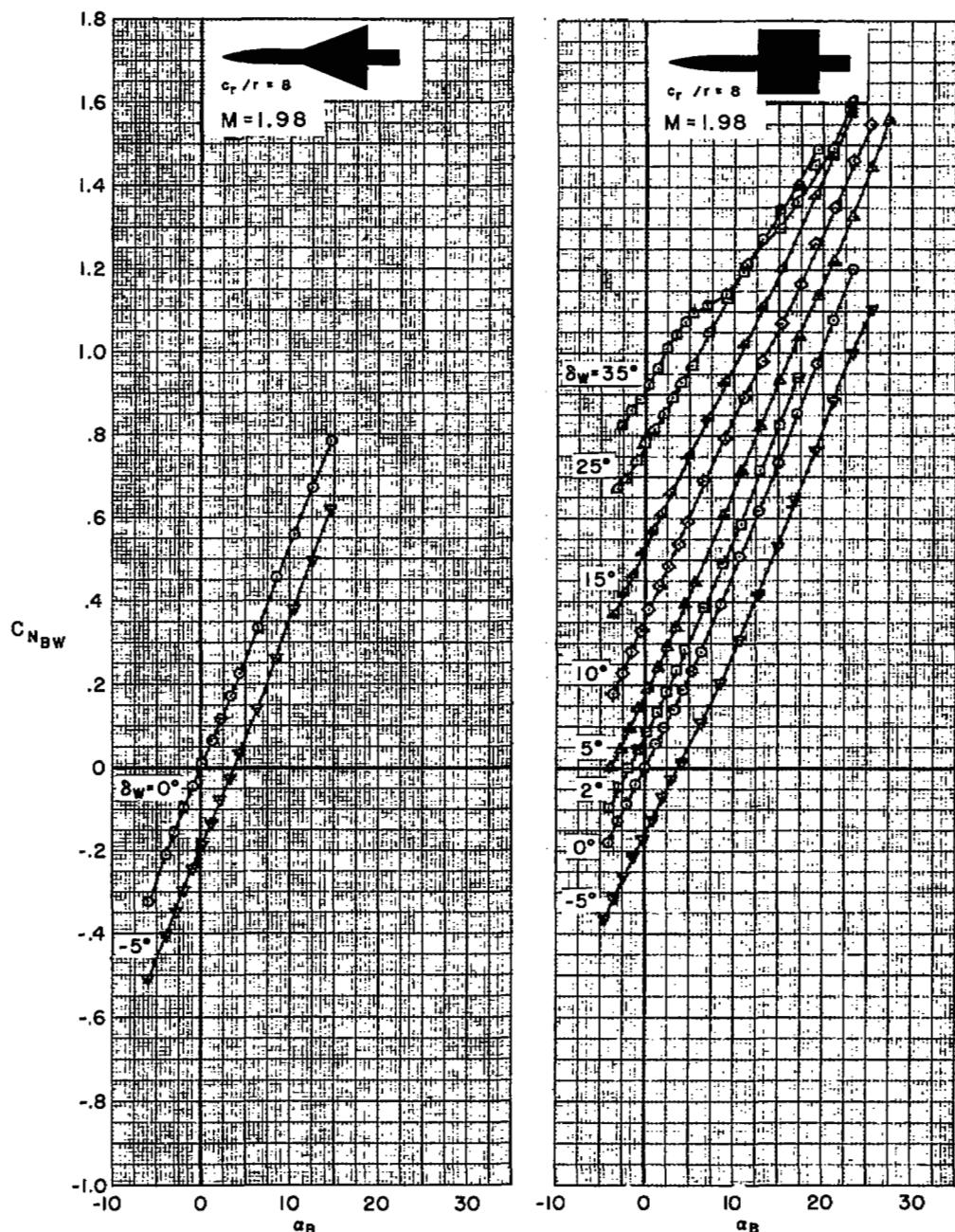
(a) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(b) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 10.- Variation with angle of attack of normal-force coefficient for the body-wing combinations.

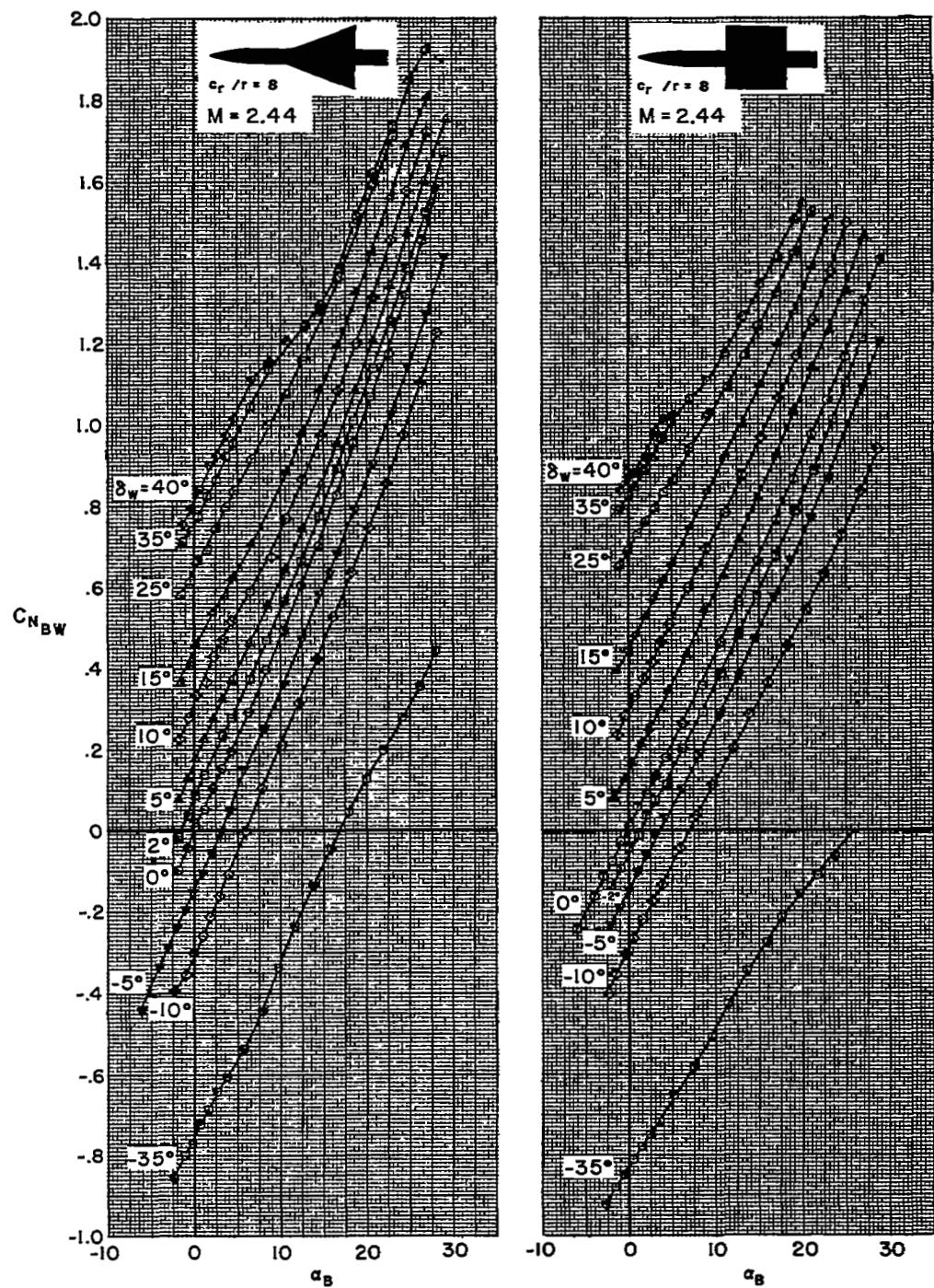
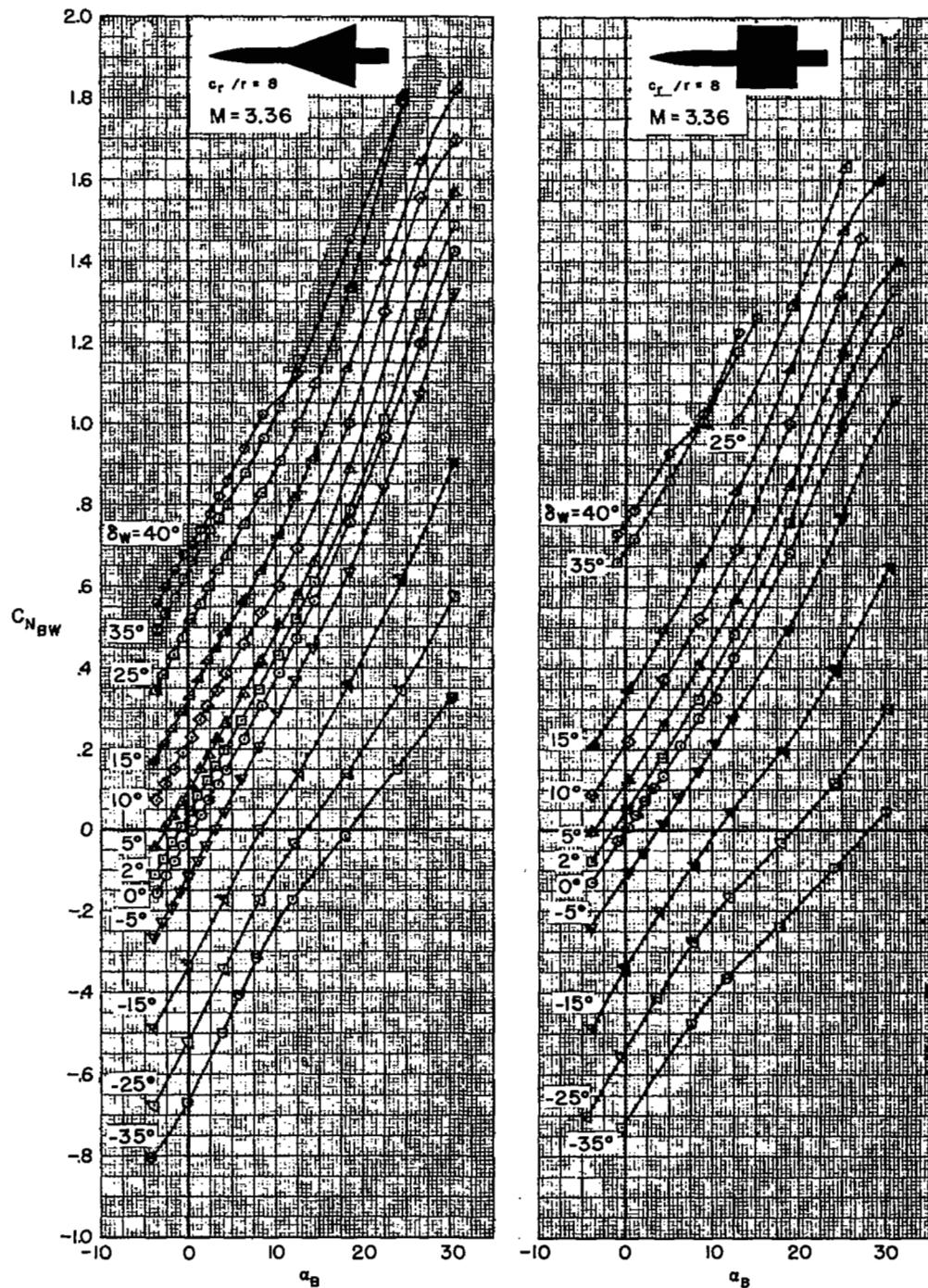
(c) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(d) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 10.- Continued.



- (e) $A = 2$ triangular wing and body combination, $r/s = 0.2$. (f) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 10.- Concluded.

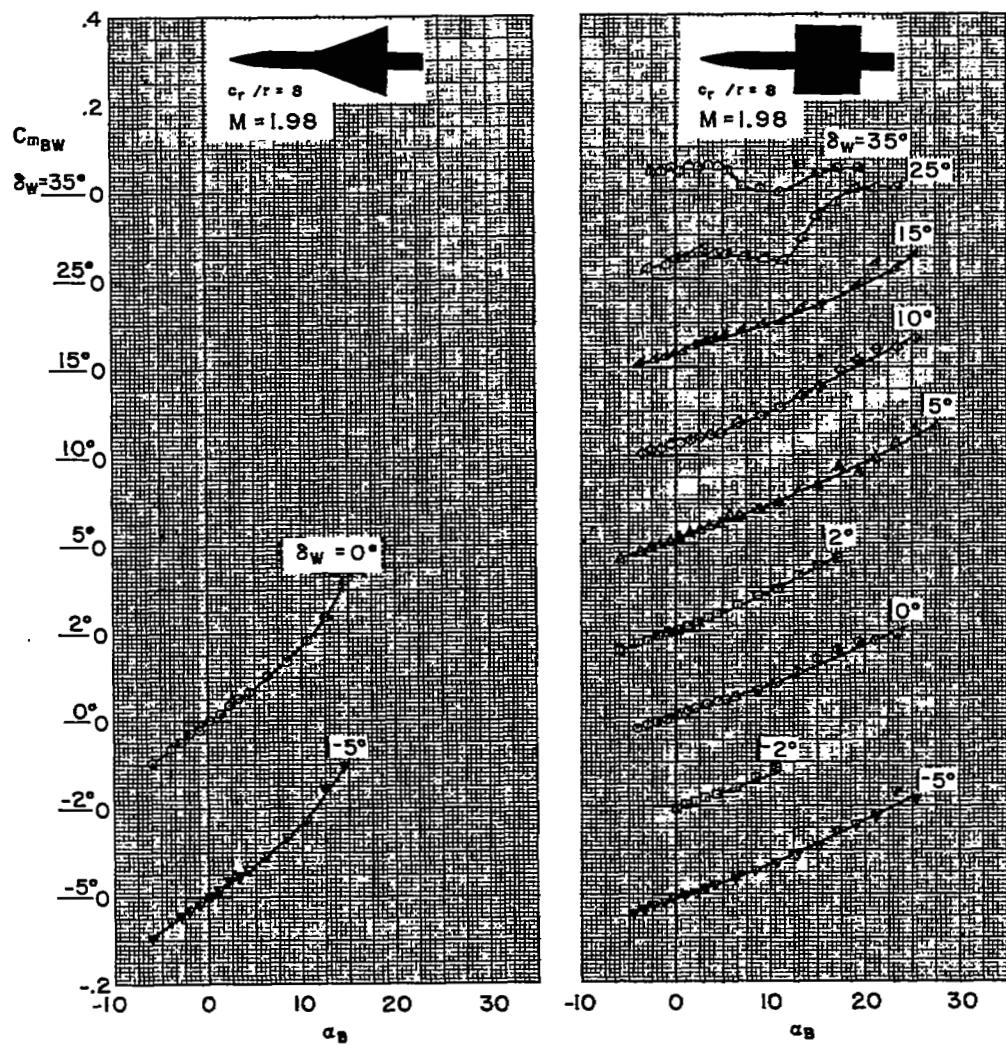
(a) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(b) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 11.- Variation with angle of attack of pitching-moment coefficient for body-wing combinations.

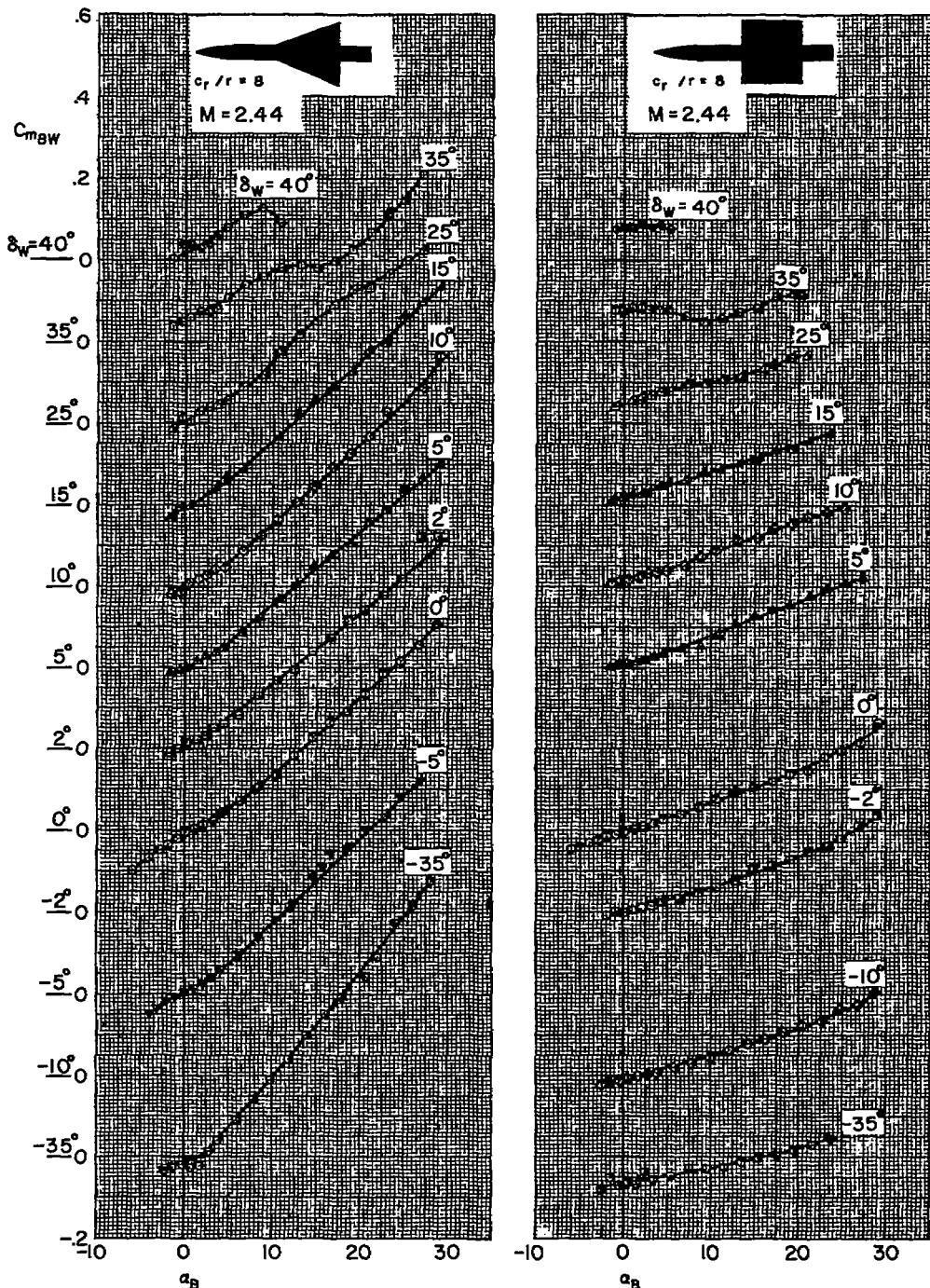
(c) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(d) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 11.- Continued.

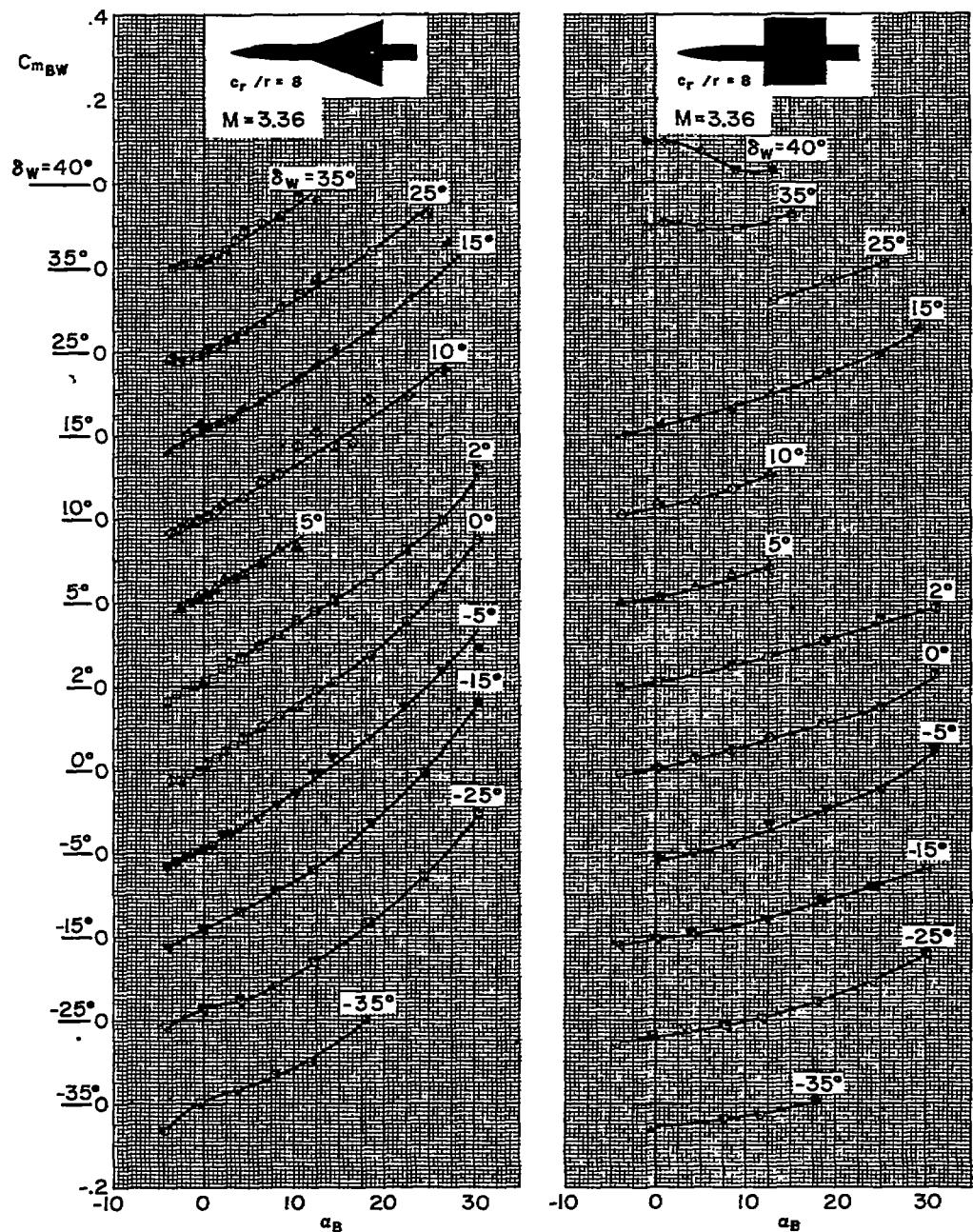
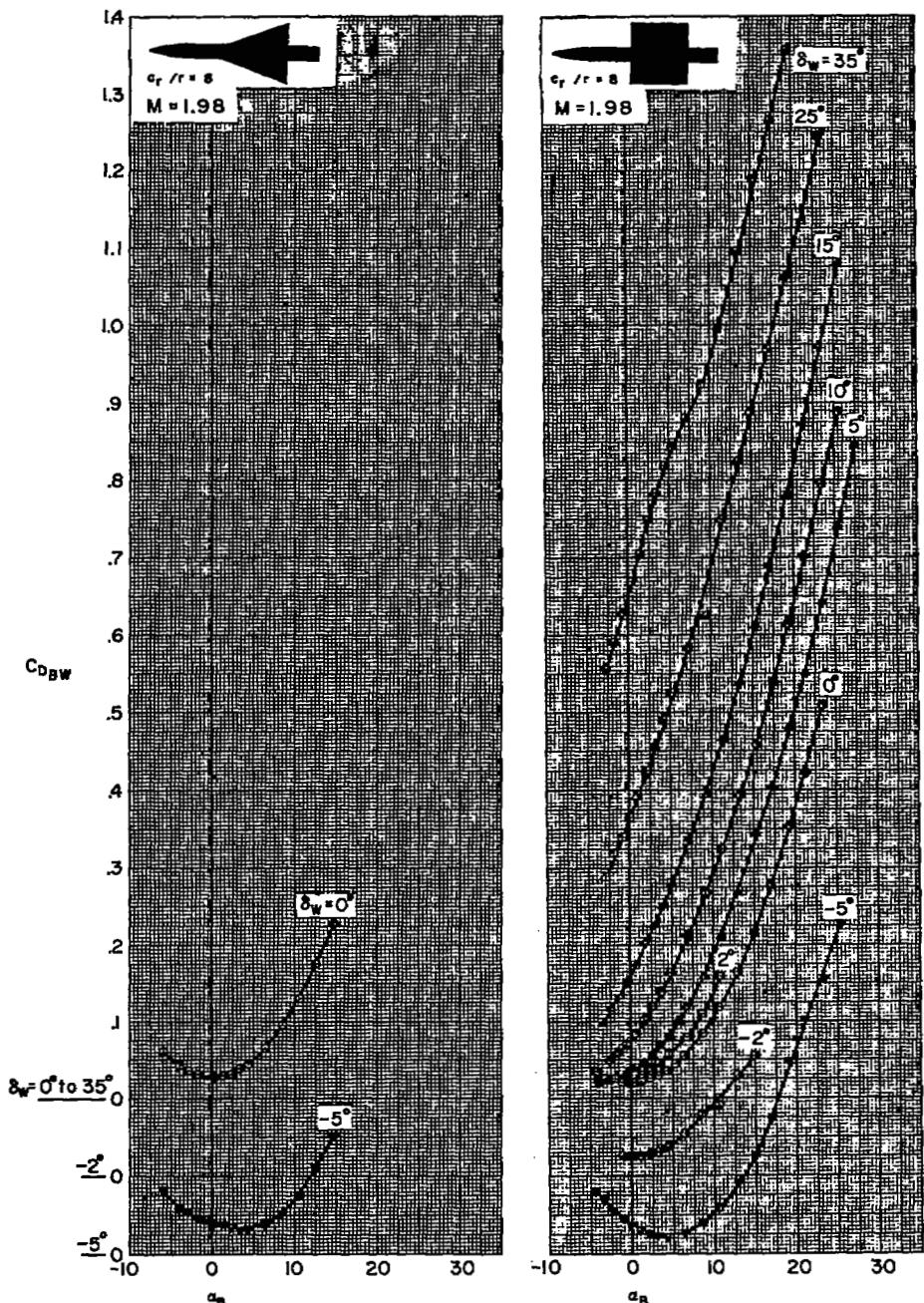
(e) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(f) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 11.- Concluded.



(a) $A = 2$ triangular wing and body combination, $r/s = 0.2$.

(b) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 12.- Variation with angle of attack of drag coefficient for the body-wing combinations.

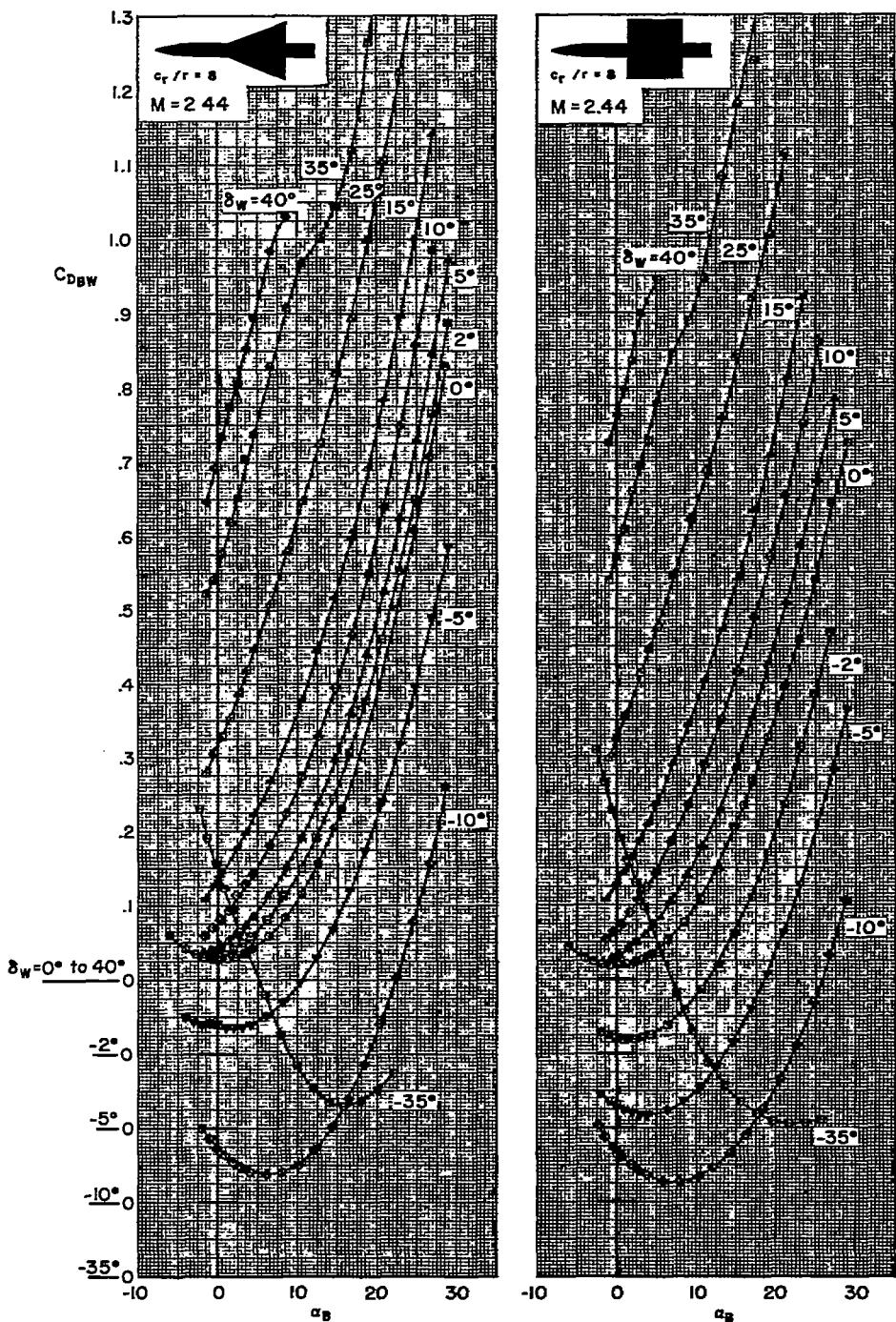


Figure 12.- Continued.

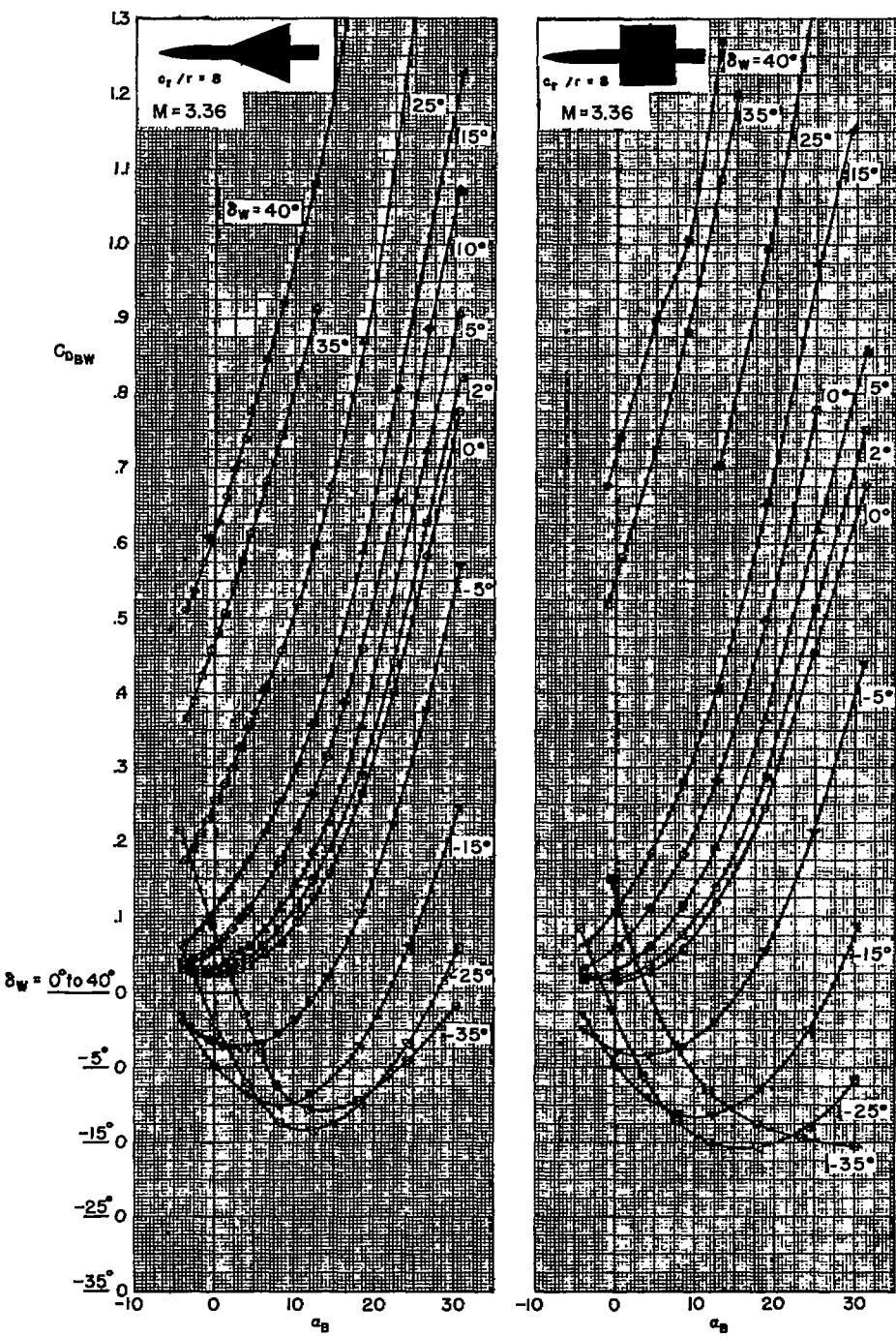
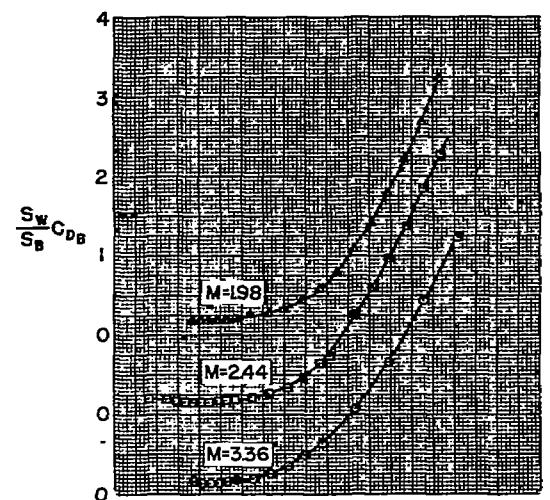
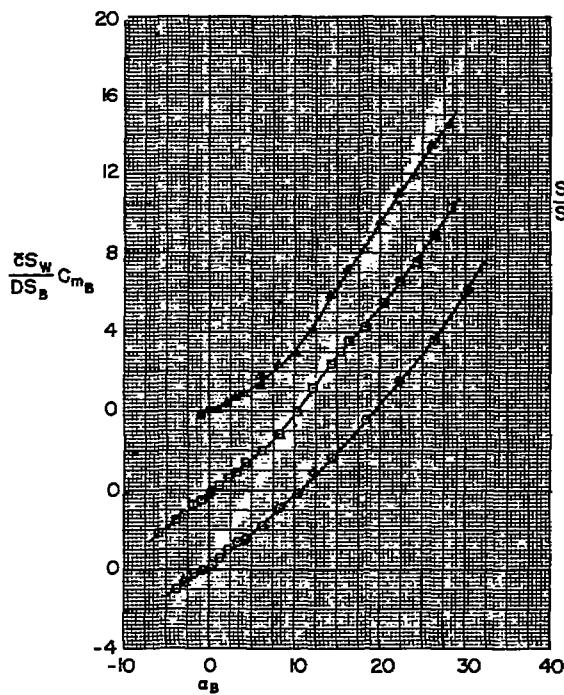
(e) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(f) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

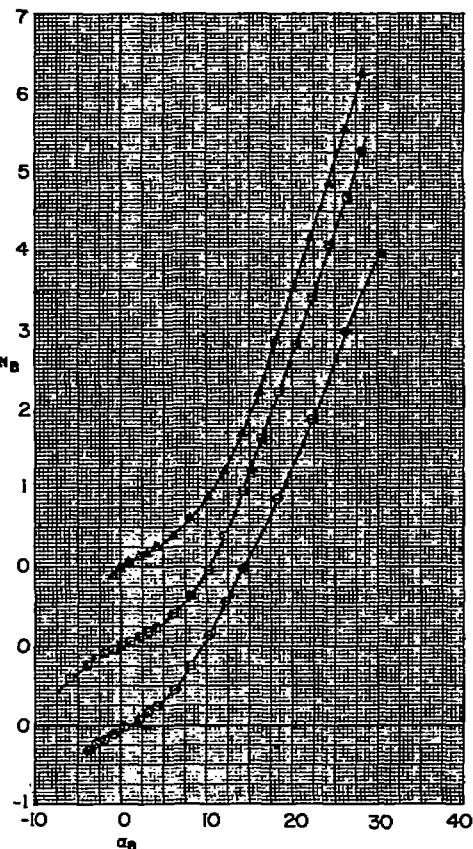
Figure 12.- Concluded.



(a) Drag.

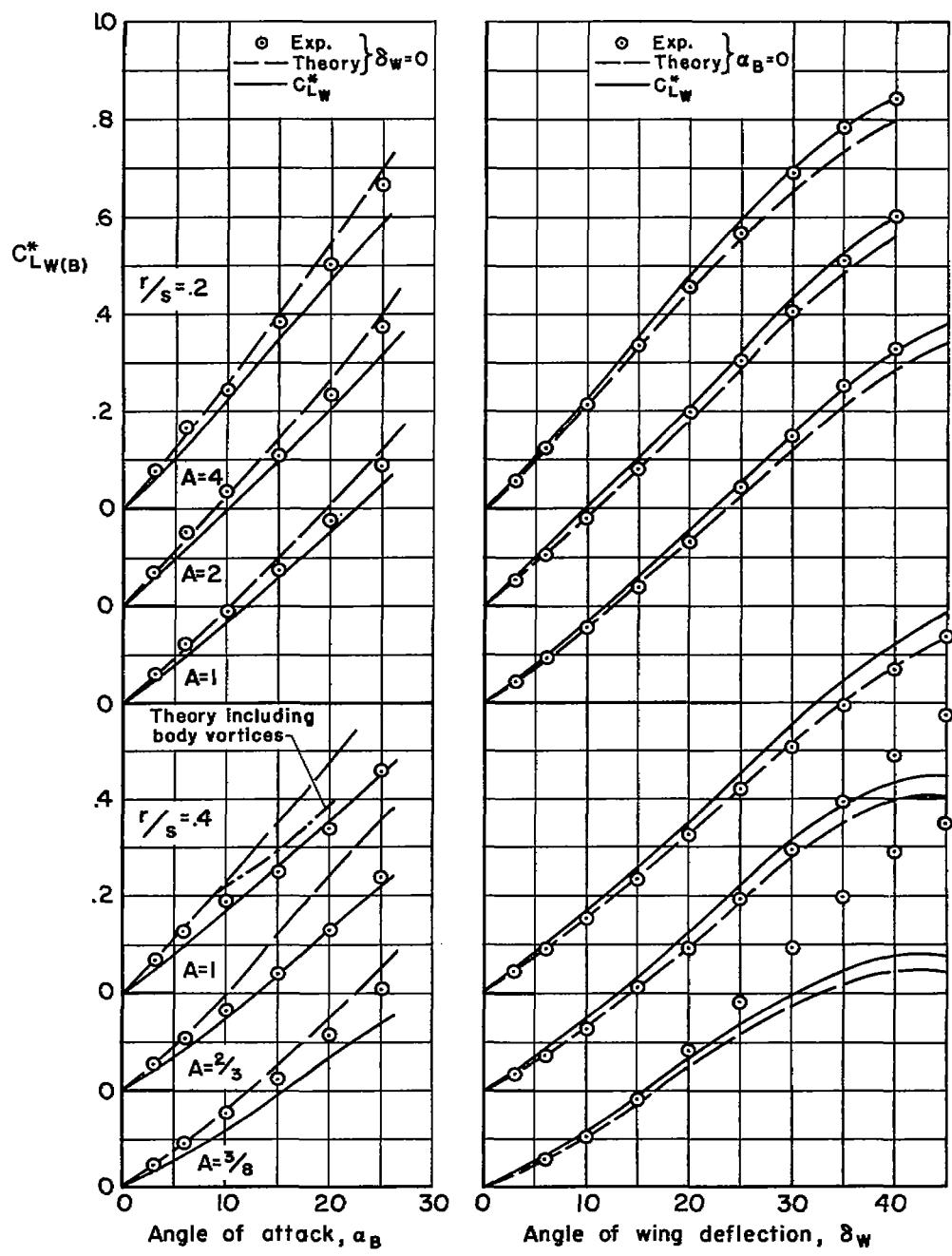


(b) Pitching moment.



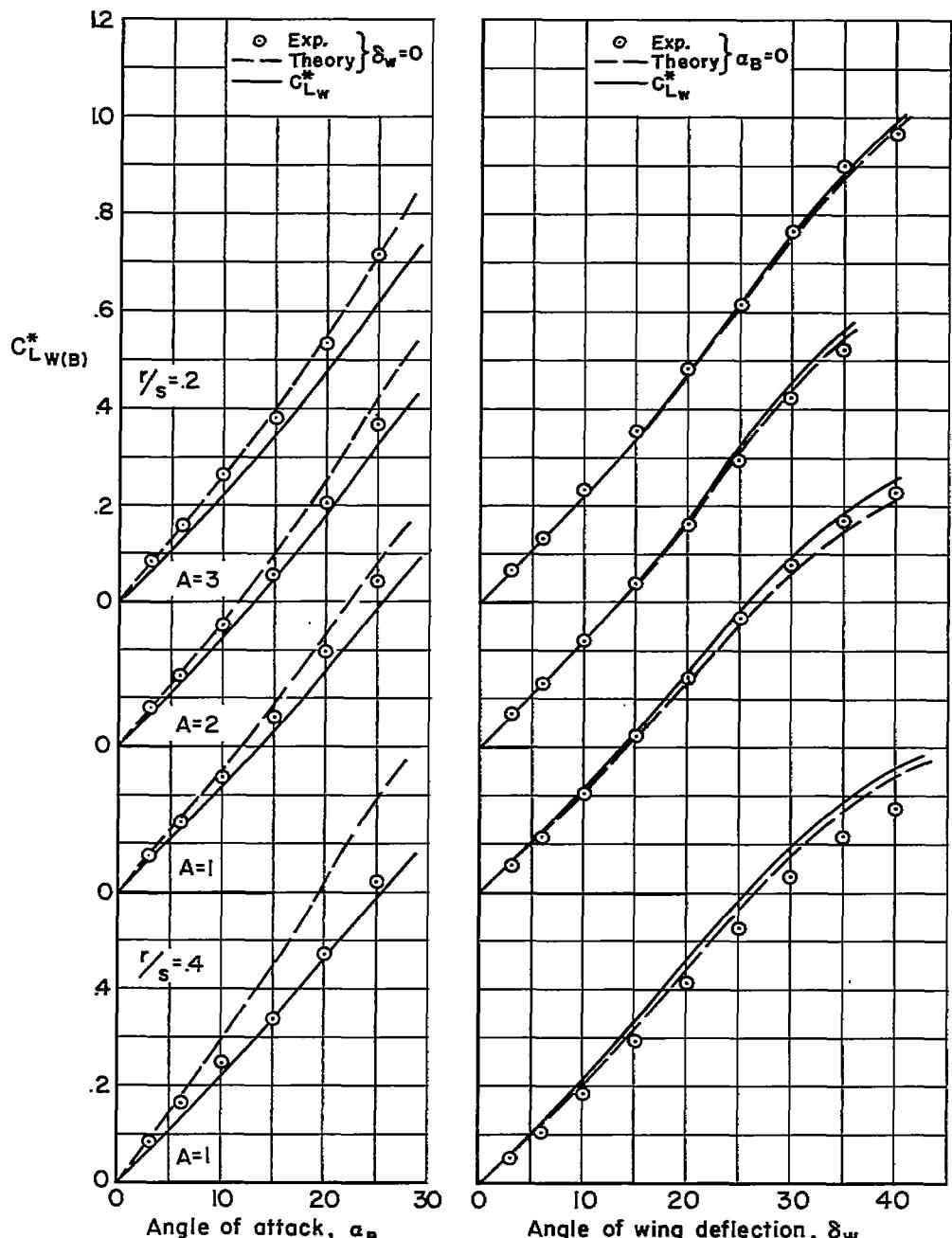
(c) Normal force.

Figure 13.- Variation with angle of attack of drag coefficient, pitching-moment coefficient and normal-force coefficient for the body alone.



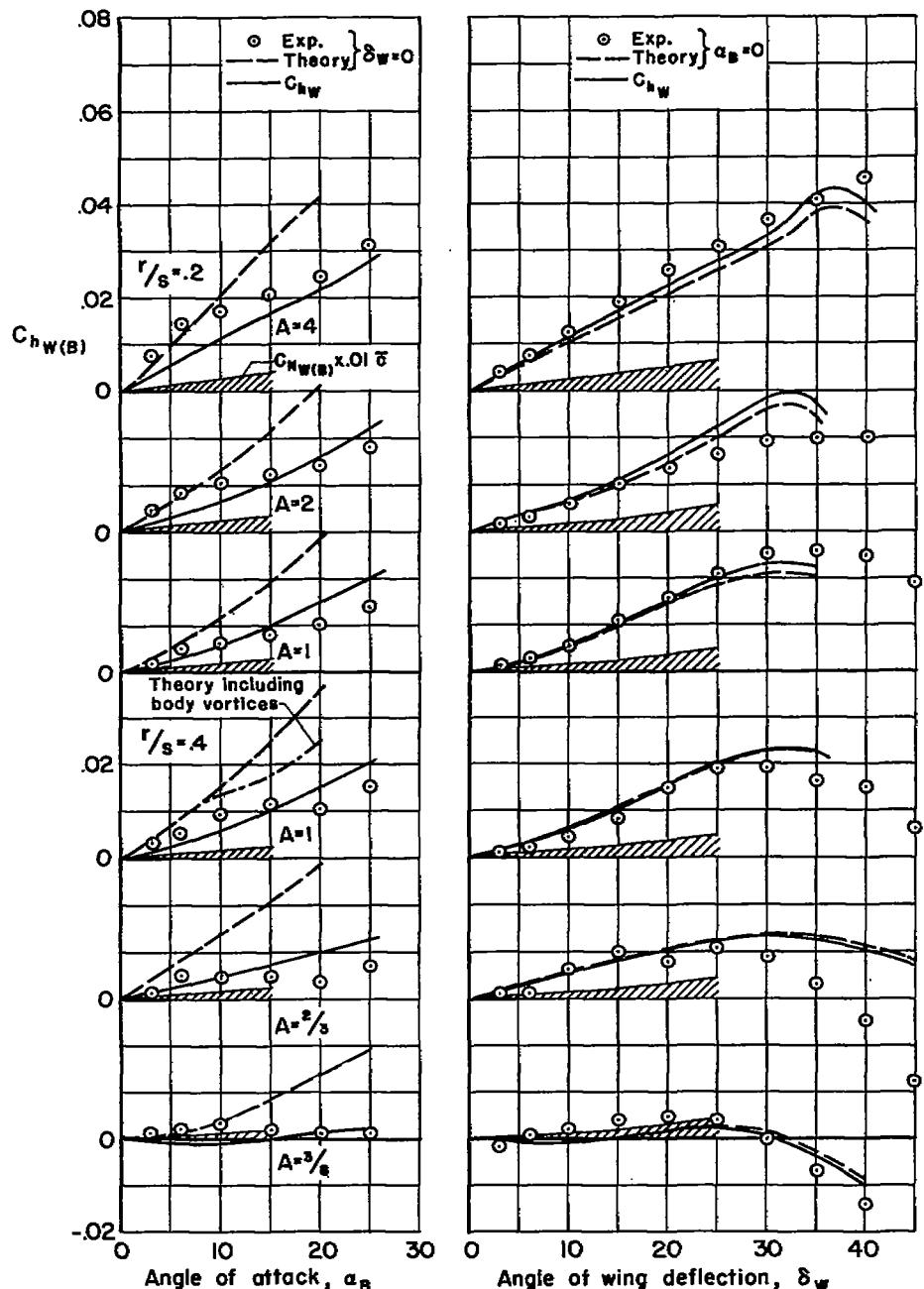
(a) Triangular.

Figure 14.- Comparison of theoretical and experimental lift coefficients for the wings in the presence of the body.



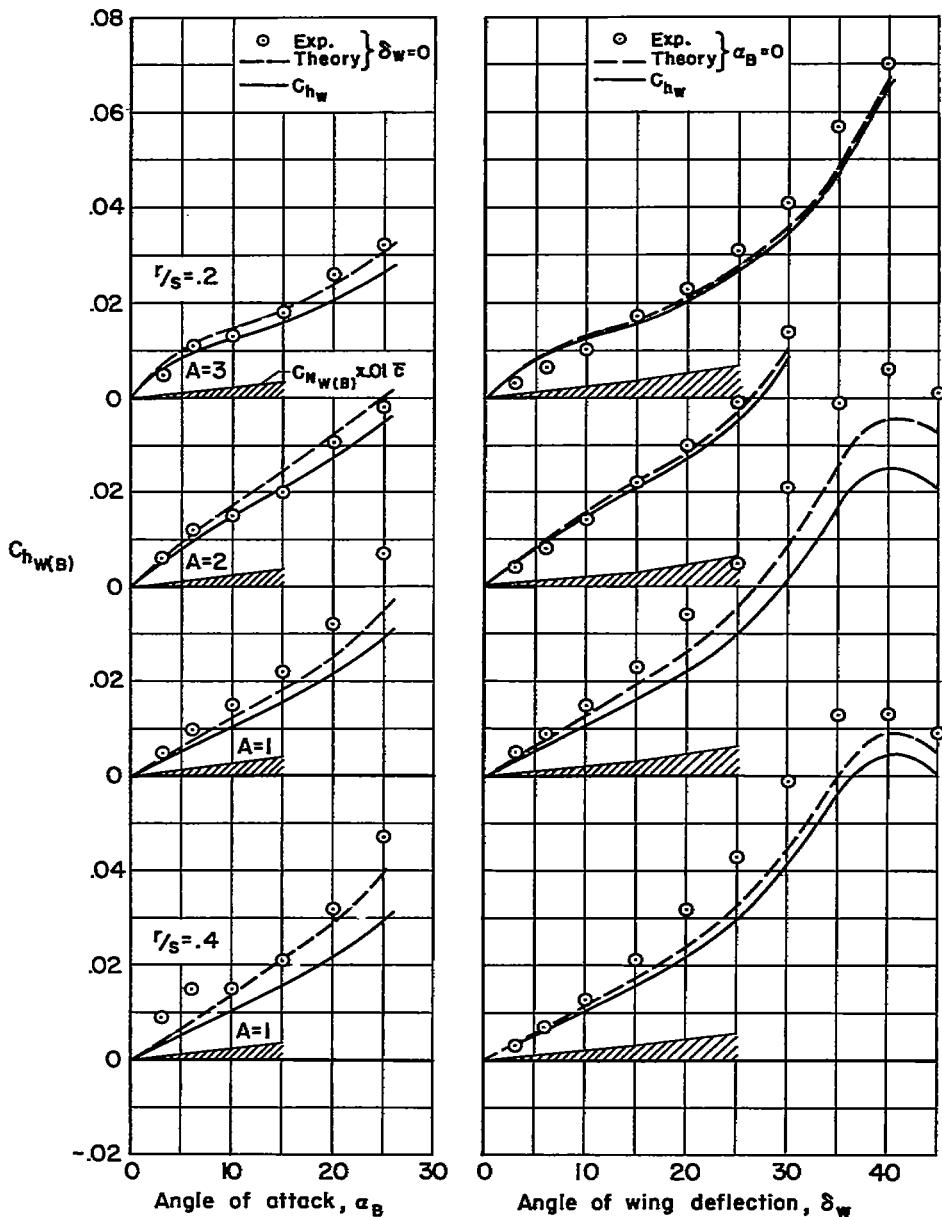
(b) Rectangular.

Figure 14.- Concluded.



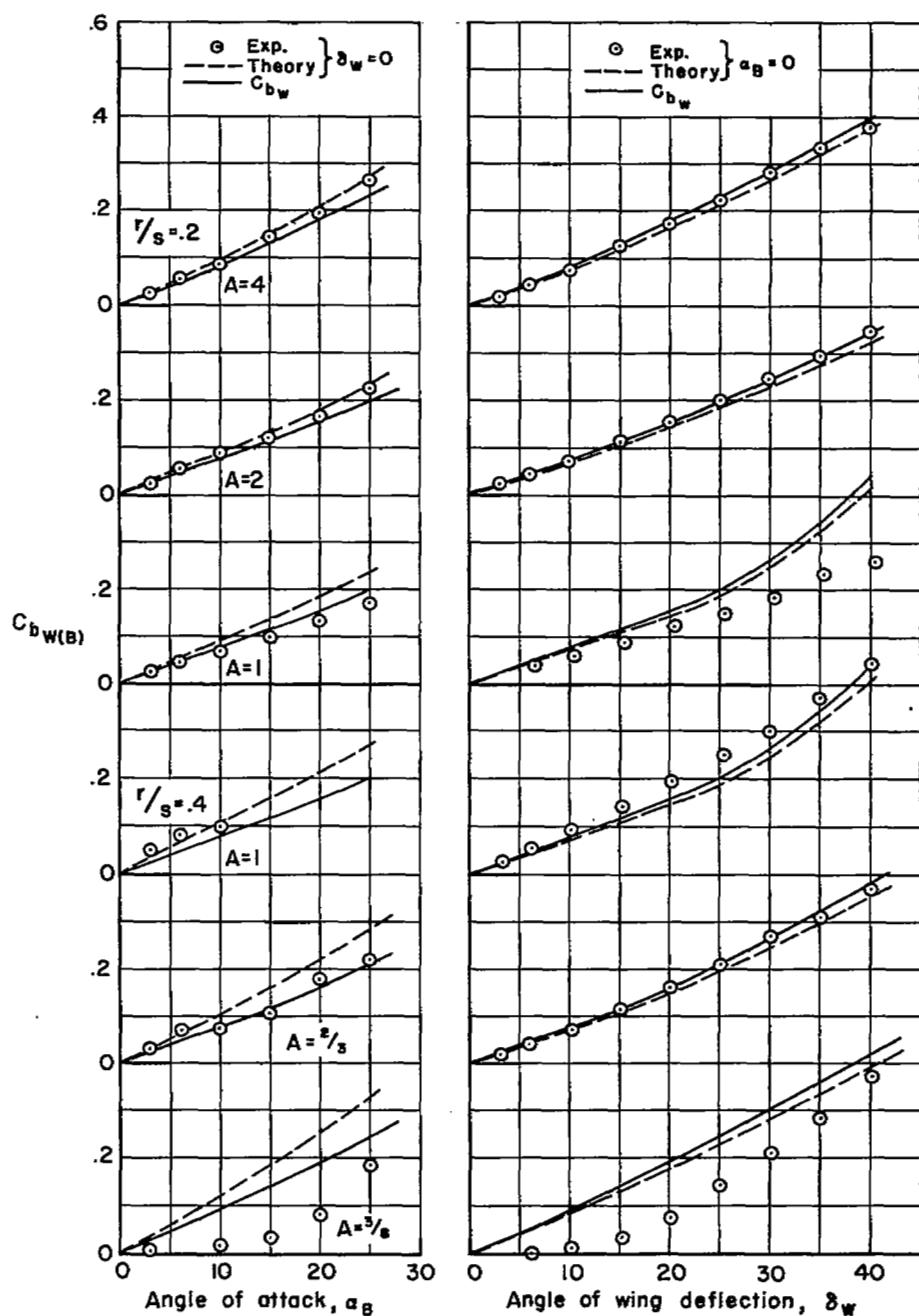
(a) Triangular.

Figure 15.- Comparison of theoretical and experimental hinge-moment coefficients for the wings in the presence of the body.



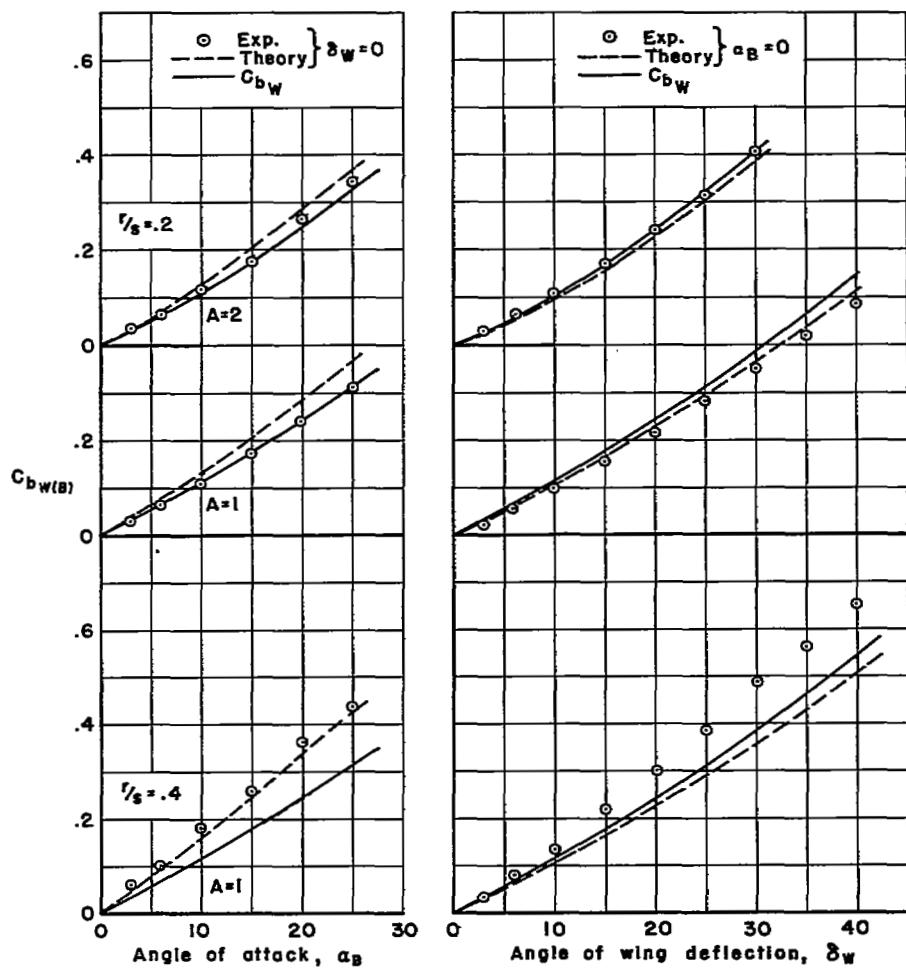
(b) Rectangular.

Figure 15.- Concluded.



(a) Triangular.

Figure 16.- Comparison of theoretical and experimental bending-moment coefficients for the wings in the presence of the body.



(b) Rectangular.

Figure 16.-- Concluded.

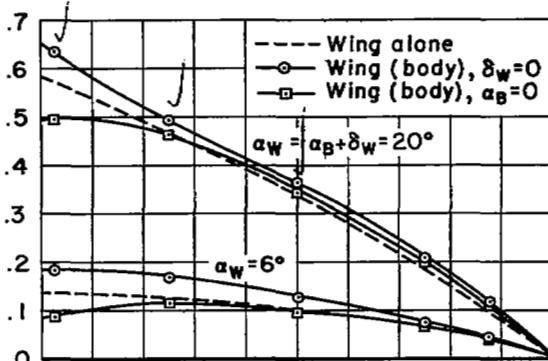
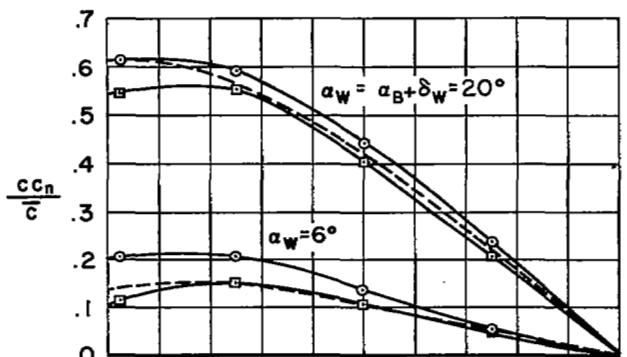
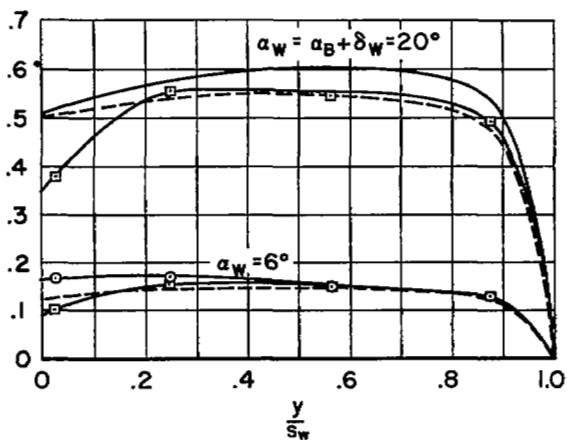
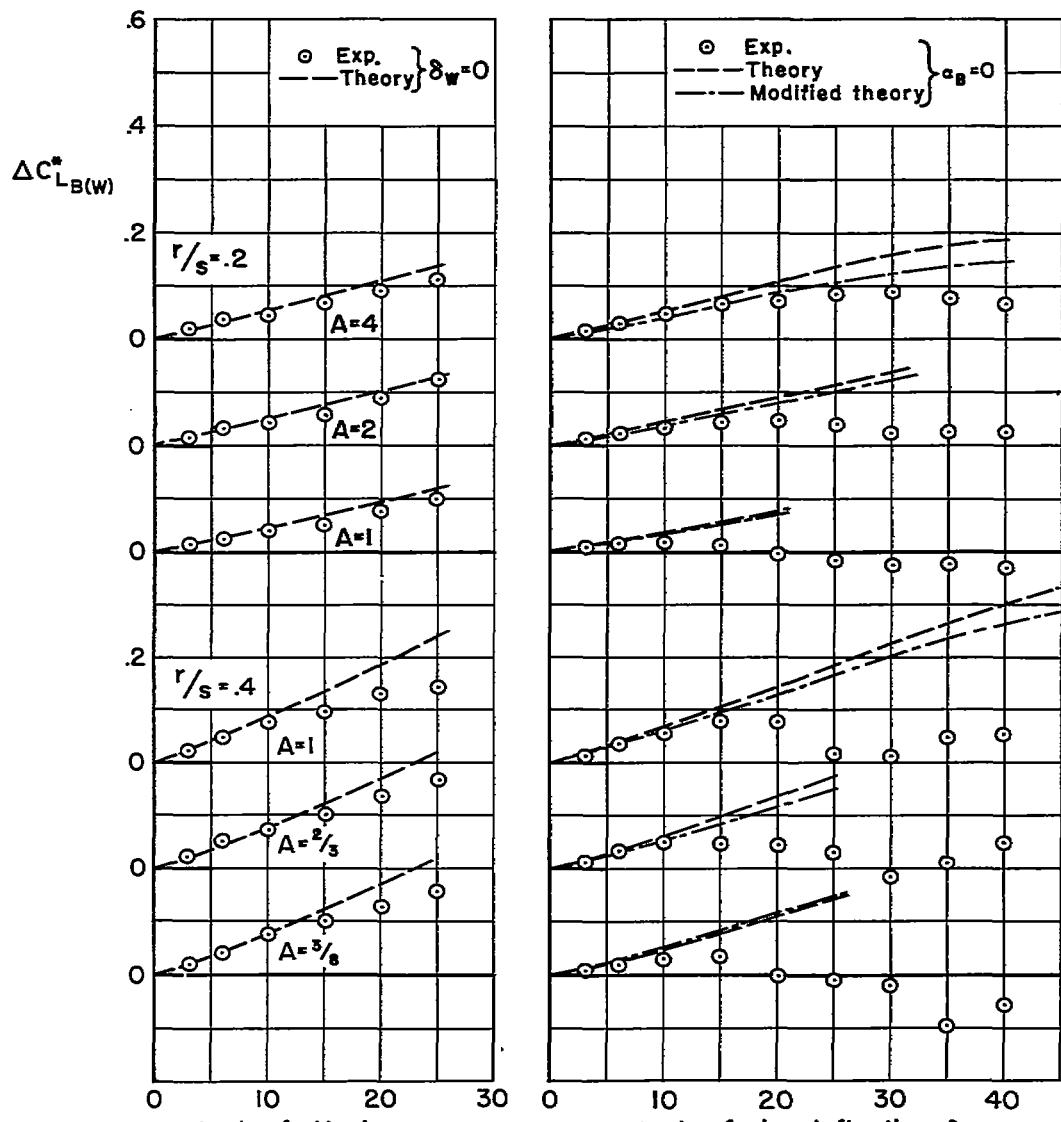
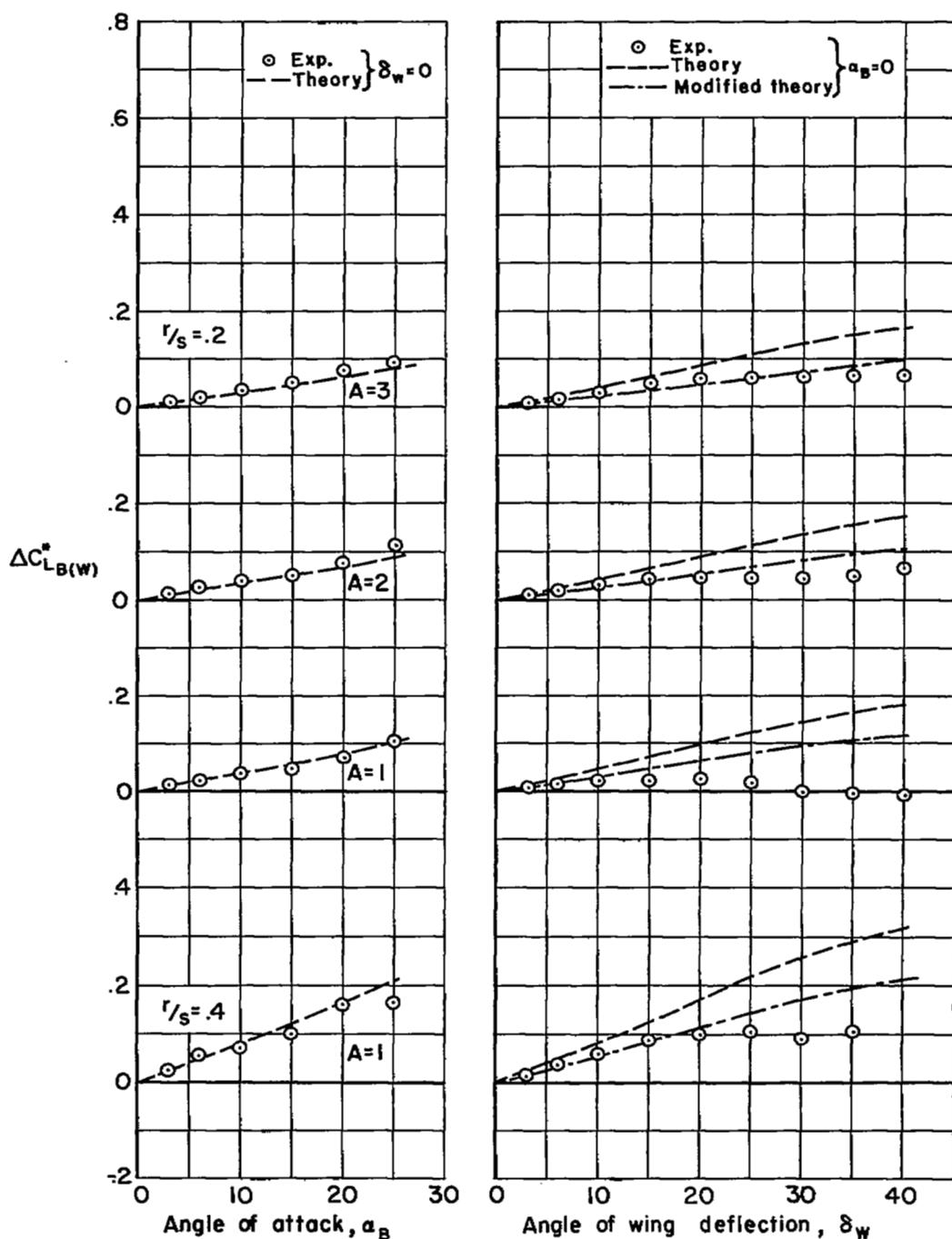
(a) $A = 2$ triangular wing, $r/s = 0.2$.(b) $A = 4$ triangular wing, $r/s = 0.2$.(c) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 17.- Comparison of span-loading coefficients for the wings in the presence of the body and for the wings alone.



(a) Triangular

Figure 18.- Comparison of theoretical and experimental interference lift coefficients for the body in the presence of the wings.



(b) Rectangular.

Figure 18.- Concluded.

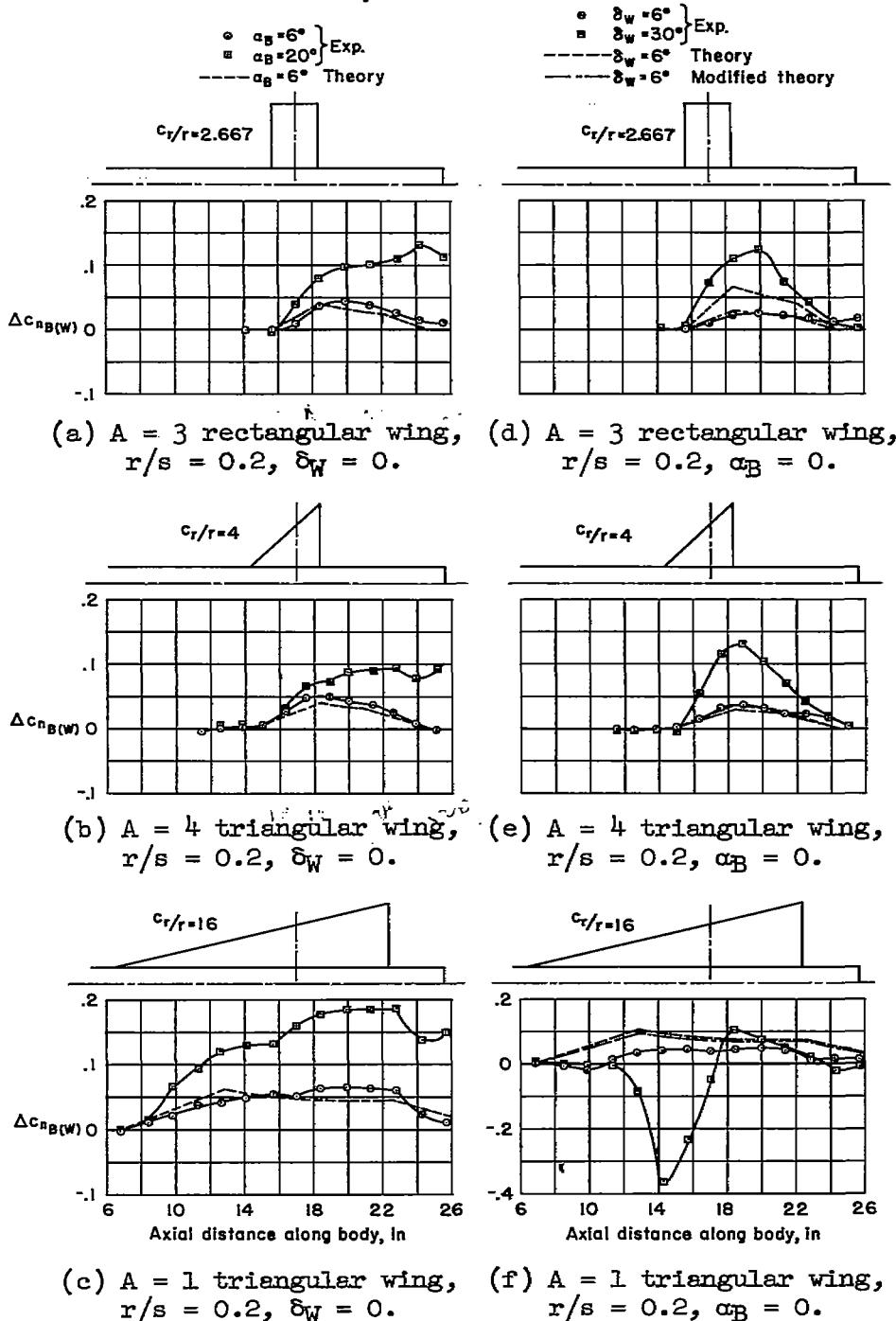
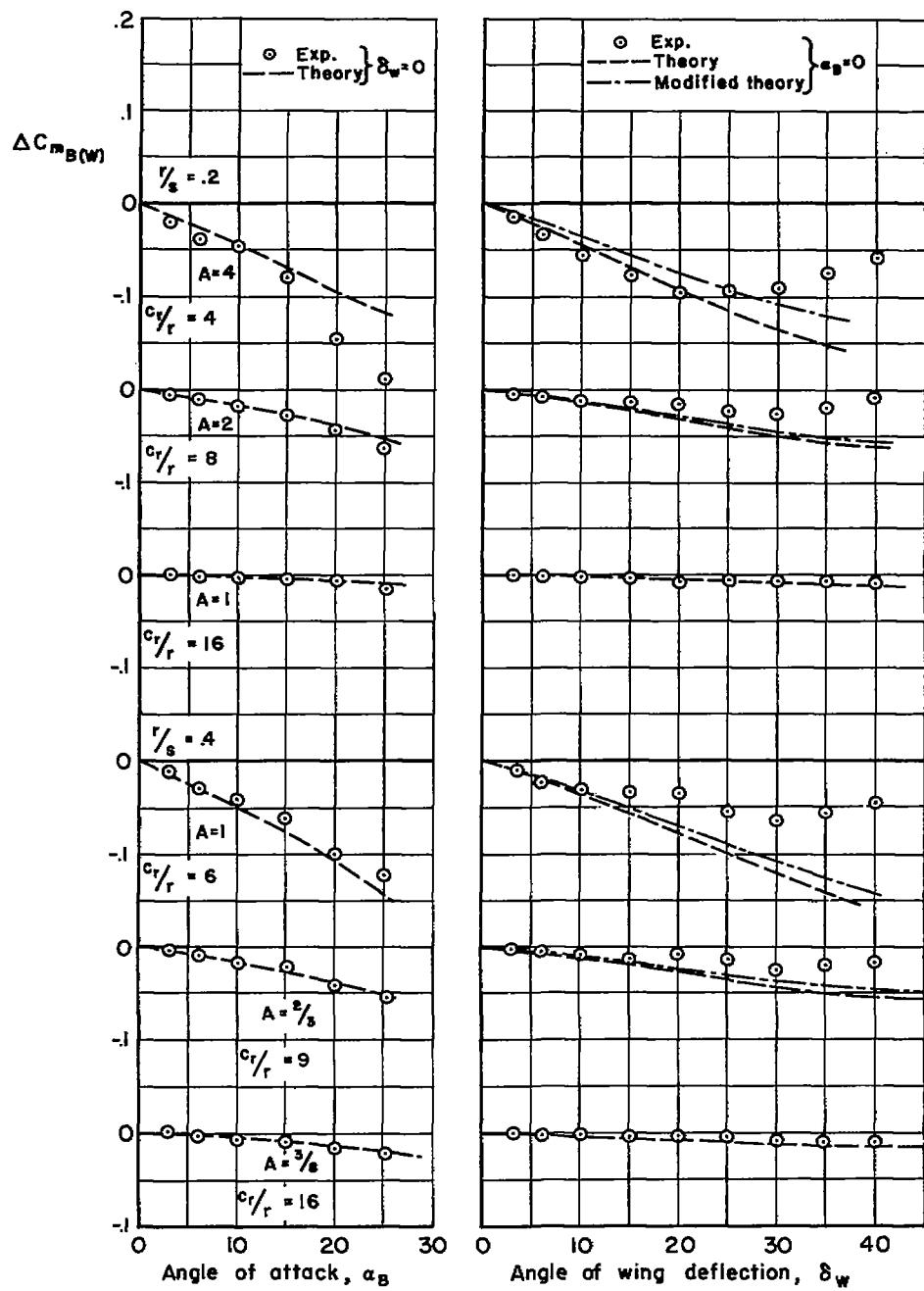
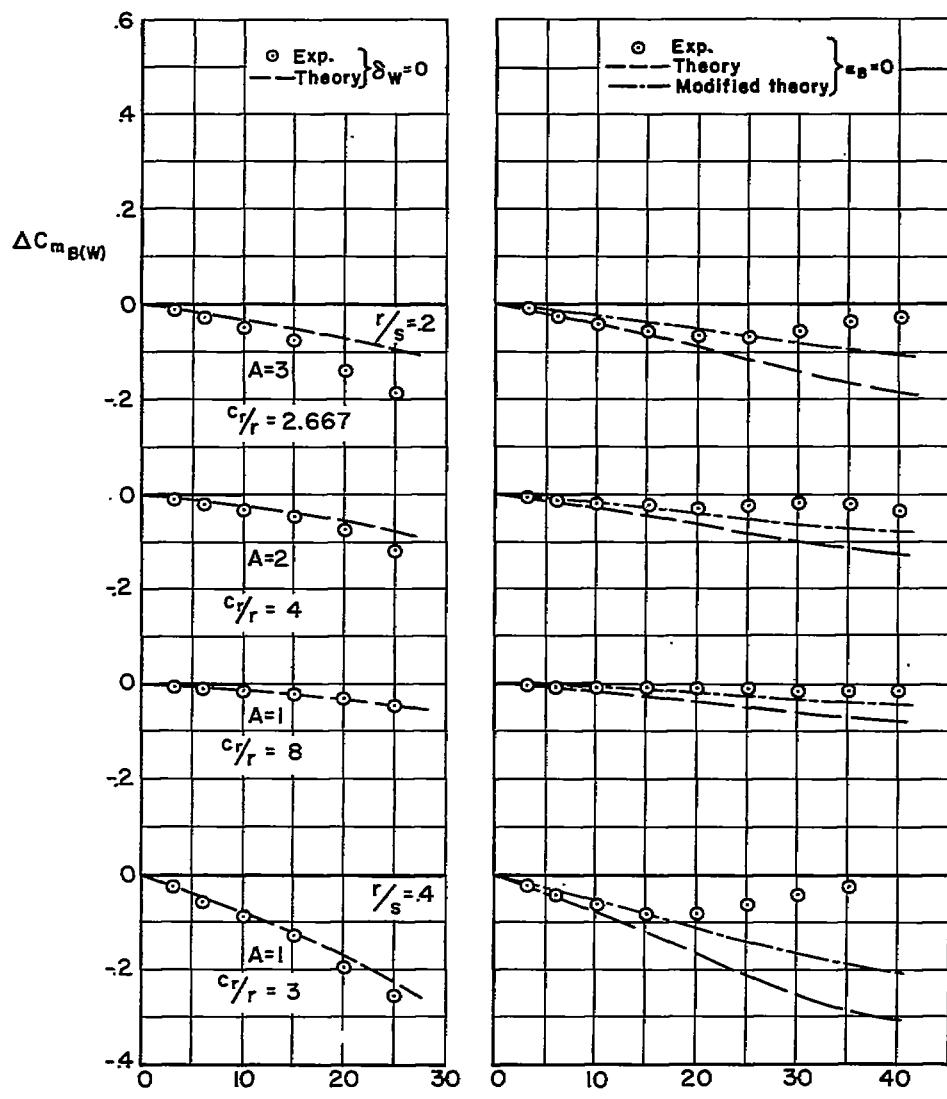


Figure 19.- Comparison of theoretical and experimental longitudinal interference loading coefficients of the body in the presence of the wings.



(a) Triangular.

Figure 20.- Comparison of theoretical and experimental interference pitching-moment coefficients for the body in the presence of the wings.



(b) Rectangular.

Figure 20.- Concluded.

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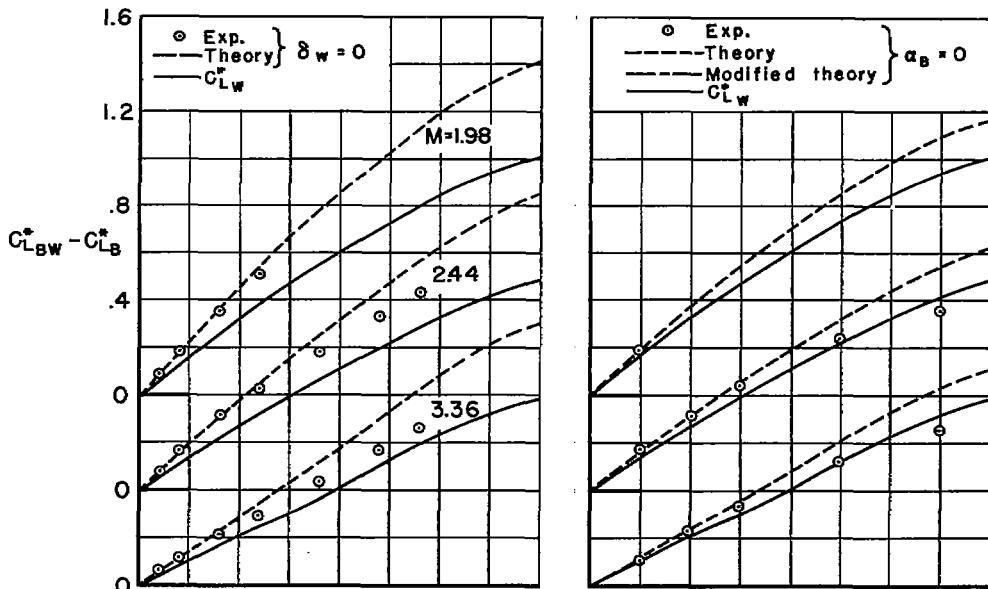
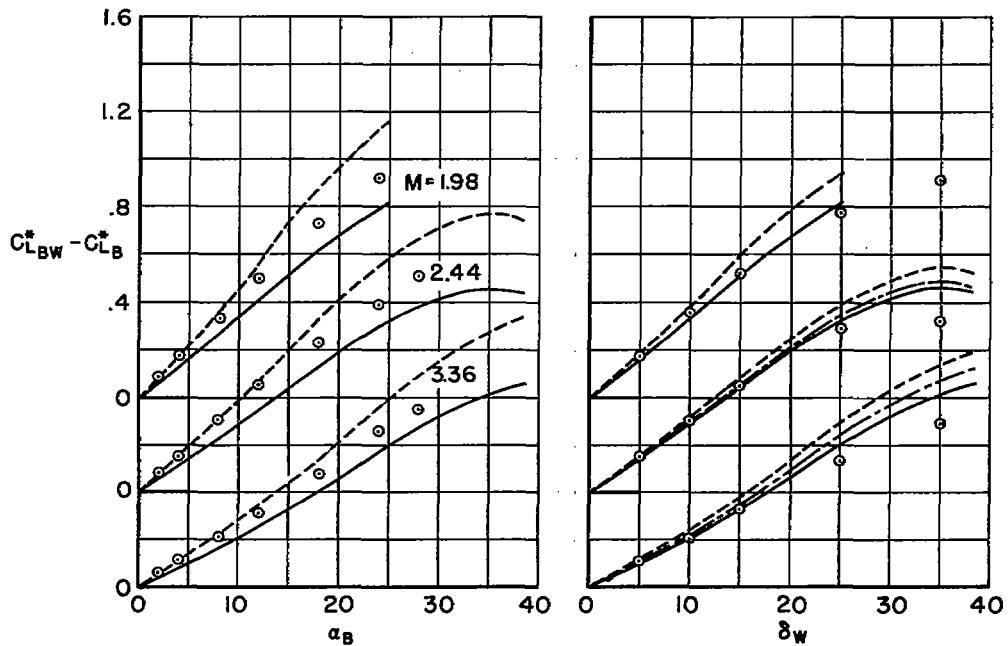
(a) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(b) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 21.- Comparison of theoretical and experimental combined lift coefficients of two body-wing combinations.

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